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COST EFFECTIVENESS STUDY OF WEATHER PROTECTION FOR SHIPBUILDING OPERATIONS

**VOLUME II** 

TODD SHIPYARDS CORPORATION

PREPARED FOR
MARITIME ADMINISTRATION

**APRIL 1974** 

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#### APPENDIX A

#### THE PRODUCTIVITY MODEL

#### DESCRIPTION OF THE PRODUCTIVITY MODEL

After a critical review of our notes from the shipyard interviews, the questionnaires, other data, and reports, we constructed Table A-1 which represents the productivity for the various crafts under selected weather categories and working locations. The effect of temperature on productivity in Table A-1 is based on Figure A-I, which is adapted from Figure C-1, Appendix C. Productivity values for some crafts varied from the norm according to the relative adverse effect of the weather category on that craft as indicated by the nature of the work. The values shown in Table A-1 assume no special Weather protection aside from normal clothing to fit the conditions. In-ship workers are assumed to be protected from wind and direct precipitation by ship structures. A special algorithm (Exhibit A) is applied to cover pass-out conditions for precipitation (or for relative humidity for painters and blasters). Exhibits B, C, and D provide explanations of our assumptions, special conditions, and penalties used to develop Table A-1.

Effective temperature (outside) is defined as the dry bulb temperature minus the wind speed in mph. This is a reasonable approximation of the wind chill factor over normal temperature ranges. Me applied the wind chill correction to dry bulb temperatures below 80°F. Above 80°F and within the ship, the effective temperature is the dry bulb temperature.

This model is applied to combinations of weather conditions with temperature by multiplying the probabilities of each other weather occurrence with its associated productivity. Under a set of combined weather conditions, the productivity in each temperature range Is the product of these separate productivities. The average annual productivity is the total of the separate productivities within each temperature range. with this model, We compute the average annual productivity for each craft and shift and for the entire standard shipyard for each shipyard location. The sample calculation which follows describes this procedure. A listing of the computer program to perform these calculations is given in

TABLE A-1. Estimated Productivity (%) of Shipyard Workers Under Various Weather Conditions

|           | EFFECTIVE TEMPERATURE (°F) |          |            |          |             |       |       |       | MIND | (MFH) |             | PRECI | II) ROITATIO | ICHES) |     |       |     |
|-----------|----------------------------|----------|------------|----------|-------------|-------|-------|-------|------|-------|-------------|-------|--------------|--------|-----|-------|-----|
|           | CRAFTS                     | <u> </u> | 5-19       | 20-29    | 30-39       | 40-79 | 80-89 | 90-99 | 100+ | <12   | 13-24       | 25+   | None         | Trace  | .01 | .0209 | .1• |
| õ         | TSIDE .                    |          |            |          |             |       |       |       |      |       |             |       |              |        |     |       |     |
|           | Painters                   | 30       | 56         | 75       | 92          | 100   | 84    | 48    | 15   | 100   | 70          | 0     | 100          | •      | 0   | •     | •   |
|           | Welders                    | 25       | 51         | 70       | 92          | 100   | 79    | 48    | 15   | 100   | 80          | 10    | 100          | 100    | 80  | 0     | C   |
|           | Riggers                    | 25       | 55         | 75       | 92          | 100   | 84    | 53    | 20   | 100   | 90          | 15    | 100          | 100    | 95  | 85    | 40  |
|           | Fitters                    | 25       | 51         | 70       | <b>92</b>   | 100   | 84    | 53    | 20   | 100   | 90          | 20    | 100          | 100    | 95  | 85    | 40  |
|           | Others                     | 30       | 56         | 75       | 92          | 100   | 84    | 53    | 20   | 100   | <b>9</b> \$ | 40    | 100          | 100    | 95  | 90    | 50  |
| <u> 1</u> | <u>n SHIP</u> (Effect      | tive Tem | perature 4 | Dry Bulb | Tempera tur | •)    |       |       |      |       |             |       |              |        |     |       |     |
| ,         | Painters .                 | 0        | 0          | 0        | 70          | 100   | 79    | 48    | 15   | 100   | 100         | 80    | 100          | •      | •   | •     | •   |
|           | Welders                    | 30       | 56         | 7\$      | 130         | 100   | 74    | 43    | 10   | 100   | 100         | 80    | 160          | 100    | 100 | 95    | 80  |
|           | Riggers                    | 30       | 56         | 75       | 92          | 100   | 79    | 48    | 15   | 100   | 100         | 60    | 100          | 100    | 100 | 95    | 80  |
|           | Fitters                    | 30 /     | 56         | 75       | 92          | 100   | 79    | 40    | 15   | 100   | 100         | 80    | 100          | 100    | 100 | 95    | 80  |
| •         | Others '                   | 30       | 55         | 75       | 92          | 100   | 79    | 48    | 15   | 100   | 100         | 80    | 100          | 100    | 100 | 95    | 60  |

<sup>.</sup> Relative humidity is assumed to be the dominant factor affecting the productivity of painters and blasters

F

TABLE A-1 (continued). Estimated Productivity (%) of Shipyard Workers Under Various Weather Conditions

|                | RELATIVE      | HUHIDITY               | FOG                | SHADE<br>CLOUD COYER INDEX<br>9 a.m 6 p.m. |               |  |
|----------------|---------------|------------------------|--------------------|--|---------------|--|
| CRAFTS         | <u>∢90</u>    | 90-100                 | Visibility         | <3<br>Temp.                                | 8-10<br>Temp. |  |
| OUTSIDE        |               |                        |                    | <80° F                                     | <80° F        |  |
| Painters       | 100           | •                      | **                 | 70   | 100           |  |
| Welders        | 100           | 100                    | **                 | 70   | 100           |  |
| Riggers        | 100           | 100                    | 50-Day             | 70   | 100           |  |
| Fitters        | 100           | 100                    | 30-Night<br>50-Day | 70   | 100           |  |
| Others         | 100           | 100                    | 30-Hight           | 70   | 100           |  |
| IN SHIP (Effec | tive Temperat | ure = Dry Bulb Tempore | iture)             |  |               |  |
| Painters       | 100           | 0                      | Same as            | 95   | 100           |  |
| Helders        | 100           | 100                    | for<br>outside     | 95   | 100           |  |
| Riggers        | 100           | 100                    | crofes             | \$5  | 100           |  |
| Fitters        | 100           | 100                    | •                  | 95   | 100           |  |
| Others         | 100           | 100                    | •                  | \$5  | 100           |  |

he Not Directly Applicable

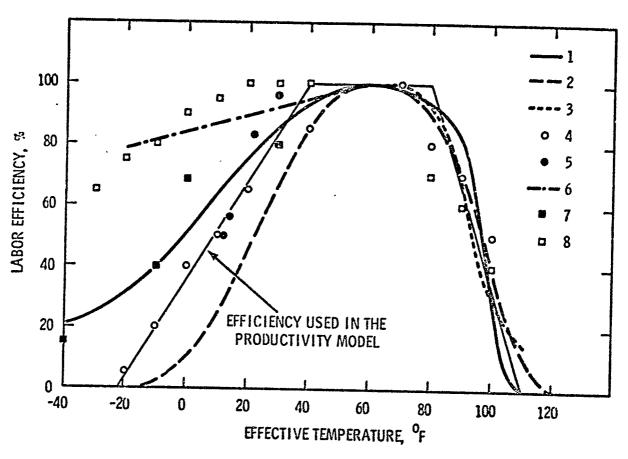


FIGURE A-1. Outdoor Worker Efficiency

#### LEGEND

- Doyle, "Controlling Climate Effects", Tool Engr., 1955 (efficiency curve prépared under condition of little or no wind.

- 2. General Dynamics, Quincy (DX Study).
  3. ASHVE Guide and Data Book (men at work 90,000 ft-Ib of work per hour).
  4. Constructor, May 1972 (welders, pipefitters, carpenters, electricians).
  5. Unidentified shippareture to effective temperature).
- 6. Bechtel construction project in Canada (winter) (converted from wind chill temperature and corrected to 100% efficienty at 60°F). ASHVE Guide and Data Book (Armstrong's data for line-maintenance job).
- Constructor, May 1972 (Laborers, ironworkers, operating engineers).

Appendix L. Improvements in the average productivity for the entire shipyard provide the basis for assessing the cost-effectiveness of various weather protective facilities.

#### Sample Calculation

Assume: A welder is working outside on day shift in 30 to 39°F effective temperature, (already corrected for the wind chill effect). The frequency of wind at this shipyard is 80% less than 12 mph, 15% between 13 to 24 mph, and 5% above 25mph. The frequency of precipitation is 85% none or trace, 10% at 0.01 in./hr, 3% from 0.02 to 0.09 in./hr, and 2% at 0.1+ in./hr. The welders average productivity in wind alone would be, using these frequencies and the productivity values in Table A-1:

$$0.80 \times 1.00 + 0.15 \times 0.80 + 0.5 \times 0. = 0.92 \text{ Or} 92\%$$

The welders average productivity affected by precipitation alone would be

$$0.85 \times 1.00 + 0.10 \times 0.80 + 0.03 \times 0. + 0.2 \times 0. = 0.93 \text{ or } 93\%$$

The welders average productivity for the 30 to 39°F effective temperature range would be the product of the productivities for temperature, wind, and precipitation, or

$$0.92 \times 0.92 \times 0.93 = 0.7870r 79\%$$

If the 30 to  $39^{\circ}F$  effective temperature occurred 10% of the time for the shipyard location, the average annual outside productivity of welders in this temperature range would be 0.10 x 0.79 or 0.079. The total annual productility would be the sum of the productivities for each effective temperature category. This type of calculation is repeated for each shift, each work location, and each craft.

The total shipyard productivity is the sum of craft, shift, and location productivities weighted by the number of craftsmen involved. The total shipyard productivity (when subtracted from unity and multiplied by the annual hours worked) indicates the total manhours of productivity lost because of adverse weather.

Since fog is not assumed to affect welders and since shade is assumed to be effective only at temperatures above 80°F, these conditions were not included in this calculation. Fog and shade, when included, are treated similarly to wind and precipitation.

#### ABSENTEEISM AND TURNOVER

Although the shipyards attributed some absenteeism and turnover to the weather, these were not believed to be major cost factors. Comments ran from "less than 5% of the absenteeism is caused by weather" to "its just as well they do not show up in bad weather, we would have to send them back home anyway."

On turnover, it was felt by some that poor working conditions caused by bad weather led employees to take other work when available. One shipyard foreman remarked that inside work was preferred by his crew even in good weather.

Since it was not possible to establish the rate or cost of either absenteeism or turnover to weather, these factors were omitted from our model.

#### An Assessment of Potential Bias in the Model

Our model is intended to provide a simplified approximation of the real situation. Since the real situation is too complex and too little understood to permit an economical exhaustive analysis, several simplifying assumptions were made and several factors were omitted from the model. These assumptions and omitted factors were examined in order to estimate, at least qualitatively their overall affect on our reported results. These factors are listed below according to whether they would tend to increase or decrease the benefits resulting from increased weather protection in the shipyards. On balance, we believe that the tendency toward increased benefits would far outweigh the tendency towards decreased benefits, and therefore, our results probably understated the potential benefits of increased weather protection.

#### Reasons Why Benefits May Exceed Those Calculated

- 1. We purposely tried to avoid overestimating productivity losses.
- 2. We did not include costs attributable to absenteeism and turnover.
- 3. He did not include potential benefits that might result from the ability to install more automated equipment through covering.
  - 4. We did not include benefits from improved lighting.
  - 5. He did not include benefits resulting from improved accident experience and the reduced potential for work stoppage for safety reasons under adverse conditions.
  - 6. We did not include savings immaterial losses.
  - 7. We did not include potential benefits from reduced maintenance on equipment, and lower capital costs of equipment purchased for inside use which does not have to be weathertight, hence, costs less, and is usually less expensive to install than outside in the weather.
  - 8. We did not include losses resulting from extreme or extended adverse weather conditions. These would tend to be ameliorated with better weather protection.
  - 9. The impact of snow and snow cover on lost production and time spent searching for and/or reproducing material lost in the snow was not included.
- 10. The savings in eliminating existing space heating and cooling costs were not included.
- 11. Higher and more consistent quality may result.
- 12. Smaller structures might be more cost-effective than a complete covering of an area, since more workers may be covered per unit area.
- 13. Hater and snow removal costs were not included.

#### Reasons Why Benefits May Be Less Than Those Calculated

- 1. Real conditions may not resemble the model shipyard. a worker distribution may be different
  - b) the work load may be too variable
  - c) fixed and variable expenses may be different

- 2. Covering may impede work more than estimated.
- 3. Workers may acclimatize to a greater extent than assumed; thus, productivity saving may be overstated.
- 4. Covering costs may be greater than estimated.
- 5. Other factors may have a much greater effect on productivity and overshadow the effects of weather.
- 6. Extreme weather tends to occur less frequently than more moderate weather. Within each weather class, weather occurrences tend to be biased toward the moderate. For instance, the temperature is more frequently between 35°F to 39°F than 30°F to 34°F. In estimating the productivity of a weather class at the midpoint, we may have introduced a slight bias toward lower productivity.

## The Effects of Meather on Productivity as Determined by the Modei

After applying the productivity model to the weather conditions near each shipyard location, the results were analyzed to determine the average annual productivity, both outside and in-ship, for each craft and shipyard location (Table A-2). The results were also analyzed to determine the effect of providing protection against specific weather conditions (Tables A-3 through A-7). The factors in these tables show the estimated productivity gain for each outside craft at each shipyard location of providing each type of weather protection. For example, referring to Table A-3, providing wind protection at San Diego would increase the productivity of outside painters by 1.034 or 3.4% (1.034 - 1.000). Tables A-4 through A-7 show the relative productivity increases for the other outside crafts. These factors should be generally applicable to productivity calculations for other weather protective devices, as described in the next section.

#### APPLICATION OF PRODUCTIVITY MODEL TO A SPECIFIC SHIPYARD

The productivity model may be applied to a specific weather protection facility and shipyard through the use of the factors shown in Tables A-3 through A-7. These factors represent the potential productivity increase

TABLE A-2. Average Annual Productivity by Craft and Work Location

|                  | Paint   |        | Weld    |        | Rig           | ger    | Fitt           |        | Oth     |        |
|------------------|---------|--------|---------|--------|---------------|--------|----------------|--------|---------|--------|
| Location         | Outside | Inship | Outside | Inship | <u>Outide</u> | Inship | <u>Outside</u> | Inship | Outside | Inship |
| Baltimore        | 0.581   | 0.733  | 0.721   | 0.923  | 0.786         | 0.908  | 0.775          | 0.912  | 0.812   | 0.916  |
| New Orleans      | 0.703   | 0.799  | 0.795   | 0.904  | 0.854         | 0.910  | 0.852          | 0.910  | 0.877   | 0.915  |
| Portland, Oregon | 0.706   | 0.802  | 0.805   | 0.967  | 0.875         | 0.953  | 0.869          | 0.955  | 0.895   | 0.960  |
| Norfolk, VA      | 0.656   | 0.800  | 0.759   | 0.934  | 0.812         | 0.911  | 0.805          | 0.913  | 0.850   | 0.932  |
| Portland, Maine  | 0.461   | 0.581  | 0.685   | 0.904  | 0.751         | 0.883  | 0.737          | 0.886  | 0.779   | 0.892  |
| New York         | 0.562   | 0.748  | 0.705   | 0.948  | 0.777         | 0.929  | 0.766          | 0.932  | 0.811   | 0.937  |
| Houston          | 0.620   | 0.772  | 0.732   | 0.887  | 0.800         | 0.894  | 0.798          | 0.895  | 0.833   | 0.899  |
| Seattle          | 0.590   | 0.737  | 0.749   | 0.970  | 0.823         | 0.949  | 0.814          | 0.951  | 0.857   | 0.961  |
| San Diego        | 0.930   | 0.963  | 0.956   | 0.989  | 0.970         | 0,986  | 0.970          | 0.986  | 0.980   | 0.991  |
| Mobile           | 0.653   | 0.770  | 0.779   | 0.913  | 0.837         | 0.915  | 0.835          | 0.916  | 0.862   | U.920  |
| Boston           | 0.499   | 0.711  | 0.637   | 0.924  | 0.717         | 0.906  | 0.706          | 0.909  | 0.759   | 0.914  |
| Los Angeles      | 0.881   | 0.941  | 0.928   | 0.986  | 0.951         | 0.982  | 0.952          | 0.982  | 0.967   | 0.987  |
| Philadelphia     | 0.610   | 0.746  | C.744   | 0.930  | 0.807         | 0.913  | 0.796          | 0.917  | 0.831   | 0.921  |
| Galveston        | 0.633   | 0.788  | J.745   | 0.898  | 0.814         | 0.910  | 0.812          | 0.910  | 0.844   | 0.913  |

NOTE: The above table covers only outside and in-ship locations. Crafts located in shops are unaffected by weather and are assumed to have a productivity of 1.0 (100%).

TABLE A-3. Estimated Productivity Gain for Painters Normally Assigned to Outsic When Protection Is Provided for Each Adverse Weather Condition

| Location         | Shade | Rain<br>Protection | Dehumidifiers | Wind<br>Protection | Cooling |
|------------------|-------|--------------------|---------------|--------------------|---------|
| San Diego        | 1.004 | 1.000              | 1.031         | 1.034              | 1.004   |
| Mobile           | 1.026 | 1.000              | 1.196         | 1.162              | 1.054   |
| Boston           | 1.006 | 1.000              | 1.135         | 1.439              | 1.016   |
| Los Angeles      | 1.003 | 1.000              | 1.054         | 1.067              | 1.003   |
| Philadelphia     | 1.010 | 1.000              | 1.117         | 1.223              | 1.025   |
| New Orleans      | 1.011 | 1.000              | 1.155         | 1.142              | 1.061   |
| Norfolk          | 1.014 | 1.000              | 1.120         | 1.216              | 1.032   |
| Portland, Maine  | 1.004 | 1.000              | 1.263         | 1.262              | 1.009   |
| New York         | 1.007 | 1.000              | 1.147         | 1.336              | 1.012   |
| Houston          | 1.029 | 1.000              | 1.169         | 1.242              | 1.071   |
| Seattle          | 1.002 | 1.000              | 1.262         | 1.255              | 1.003   |
| Portland, Oregon | 1.003 | 1.000              | 1.167         | 1.139              | 1.008   |
| Baltimore        | 1.015 | 1.000              | 1.137         | 1.262              | 1.033   |
| Galveston        | 1.036 | 1.000              | 1.163         | 1.236              | 1.057   |

NOTE: For painters, productivity gains for rain protection are included in the gains dehumidifiers. It was assumed that rain protection alone gave no productivity because relative humidity during rain was above 90%, a stop work condition for

TABLE A-4. Estimated Productivity Gain for Riggers Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

| Location         | Shade | Rain<br>Protection | Dehumidifiers | Wind<br>Protection | Cooling | Heating |
|------------------|-------|--------------------|---------------|--------------------|---------|---------|
| San Diego        | 1.003 | 1.005              | 1.000         | 1.012              | 1.004   | 1.007   |
| Mobile           | 1.024 | 1.021              | 1.000         | 1.021              | 1.078   | 1.032   |
| Boston           | 1.007 | 1.024              | 1.000         | 1.266              | 1.014   | 1.054   |
| Los Angeles      | 1.004 | 1.008              | 1.000         | 1.028              | 1.004   | 1.007   |
| Philadelphia     | 1.010 | 1.018              | 1.000         | 1.126              | 1.021   | 1.048   |
| New Orleans      | 1.011 | 1.021              | 1.000         | 1.062              | 1.056   | 1.012   |
| Norfolk          | 1.014 | 1.021              | 1.000         | 1.113              | 1.028   | 1.040   |
| Portland, Maine  | 1.004 | 1.024              | 1.000         | 1.169              | 1.007   | 1.100   |
| New York         | 1.006 | 1.021              | 1.000         | 1.198              | 1.025   | 1.020   |
| Houston          | 1.028 | 1.017              | 1.000         | 1.109              | 1.065   | 1.012   |
| Seattle          | 1.001 | 1.023              | 1.000         | 1.150              | 1.003   | 1.029   |
| Portland, Oregon | 1.002 | 1.026              | 1.000         | 1.081              | 1.007   | 1.021   |
| Baltimore        | 1.013 | 1.019              | 1.000         | 1.151              | 1.027   | 1.043   |
| Galveston        | 1.036 | 1.012              | 1.000         | 1.106              | 1.057   | 1.002   |

TABLE A-5. Estimated Productivity Gain for Fitters Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

| Location         | Shade | Rain<br>Protection | Dehumidifiers | Wind<br>Protection | Cooling | Heating |
|------------------|-------|--------------------|---------------|--------------------|---------|---------|
| San Diego        | 1.003 | 1.005              | 1.000         | 1.012              | 1.004   | 1.007   |
| Mobile           | 1.024 | 1.021              | 1.000         | 1.080              | 1.051   | 1.009   |
| Boston           | 1.006 | 1.025              | 1.000         | 1.278              | 1.013   | 1.061   |
| Los Angeles      | 1.003 | 1.008              | 1.000         | 1.027              | 1.003   | 1.009   |
| Philadelphia     | 1.010 | 1.019              | 1.000         | 1.137              | 1.021   | 1.051   |
| New Orleans      | 1.012 | 1.020              | 1.000         | 1.065              | 1.056   | 1.011   |
| Norfolk          | 1.014 | 1.021              | 1.000         | 1.120              | 1.029   | 1.041   |
| Portland, Maine  | 1.004 | 1.023              | 1.000         | 1.179              | 1.007   | 1.113   |
| New York         | 1.009 | 1.019              | 1.000         | 1.210              | 1.025   | 1.024   |
| Houston          | 1.029 | 1.017              | 1.000         | 1.112              | 1.066   | 1.010   |
| Seattle          | 1.001 | 1.023              | 1.000         | 1.162              | 1.003   | 1.029   |
| Portland, Oregon | 1.002 | 1.026              | 1.000         | 1.087              | 1.008   | 1.022   |
| Baltimore        | 1.013 | 1.019              | 1.000         | 1.193              | 1.027   | 1.047   |
| Galveston        | 1.036 | 1.013              | 1.000         | 1.107              | 1.057   | 1.003   |

TABLE A-6. Estimated Productivity Gain for Other Crafts Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

| Location         | Shade | Rain<br>Protection | Dehumidifiers | Wind<br>Protection | Cooling | Heating |
|------------------|-------|--------------------|---------------|--------------------|---------|---------|
| San Diego        | 1.004 | 1.004              | 1.000         | 1.008              | 1.005   | 1.000   |
| Mobile           | 1.024 | 1.018              | 1.000         | 1.055              | 1.051   | 1.004   |
| Boston           | 1.005 | 1.020              | 1.000         | 1.207              | 1.013   | 1.051   |
| Los Angeles      | 1.004 | 1.007              | 1.000         | 1.018              | 1.004   | 1.001   |
| Philadelphia     | 1.010 | 1.015              | 1.000         | 1.102              | 1.020   | 1.044   |
| New Orleans      | 1.011 | 1.017              | 1.000         | 1.042              | 1.056   | 1.008   |
| Norfolk          | 1.014 | 1.017              | 1.000         | 1.088              | 1.029   | 1.019   |
| Portland, Maine  | 1.004 | 1.019              | 1.000         | 1.140              | 1.006   | 1.094   |
| New York         | 1.007 | 1.017              | 1.000         | 1.157              | 1.022   | 1.018   |
| Houston          | 1.028 | 1.015              | 1.000         | 1.073              | 1.065   | 1.007   |
| Seattle          | 1.001 | 1.020              | 1.000         | 1.120              | 1.003   | 1.017   |
| Portland, Oregon | 1.002 | 1.022              | 1.000         | 1.066              | 1.008   | 1.037   |
| Baltimore        | 1.012 | 017                | 1.000         | 1.123              | 1.027   | 1.038   |
| Galveston        | 1.036 | 1.011              | 1.000         | 1.069              | 1.058   | 1.000   |
|                  |       |                    |               |                    |         |         |

TABLE A-7. Estimated Productivity Gain for Welders Normally Assigned to Outside Work When Protection Is Provided for Each Adverse Weather Condition

| Location         | Shade | Rain<br>Protection | Dehumidifiers | Wind -<br>Protection | Cooling | Heating |
|------------------|-------|--------------------|---------------|----------------------|---------|---------|
| San Diego        | 1.004 | 1.013              | 1.000         | 1.023                | 1.005   | 1.000   |
| Mobile           | 1.023 | 1.048              | 1.000         | 1.122                | 1.063   | 1.121   |
| Boston           | 1.005 | 1.067              | 1.000         | 1.364                | 1.016   | 1.056   |
| Los Angeles      | 1.003 | 1.019              | 1.000         | 1.047                | 1.005   | 1.002   |
| Philadelphia     | 1.009 | 1.052              | 1.000         | 1.179                | 1.027   | 1.046   |
| New Orleans      | 1.011 | 1.047              | 1.000         | 1.102                | 1.072   | 1.006   |
| Norfolk          | 1.013 | 1.052              | 1.000         | 1.169                | 1.036   | 1.021   |
| Portland, Maine  | 1.003 | 1.066              | 1.000         | 1.223                | 1.009   | 1.106   |
| New York         | 1.006 | 1.058              | 1.000         | 1.276                | 1.014   | 1.030   |
| Houston          | 1.027 | 1.040              | 1.000         | 1.173                | 1.082   | 1.008   |
| Seattle          | 1.001 | 1.076              | 1.000         | 1.212                | 1.004   | 1.018   |
| Portland, Oregon | 1.002 | 1.074              | 1.000         | 1.113                | 1.010   | 1.027   |
| Baltimore        | 1.012 | 1.052              | 1.000         | 1.209                | 1.033   | 1.043   |
| Galveston        | 1.035 | 1.030              | 1.000         | 1.170                | 1.076   | 1.000   |

attributablee to each weather condition for each craft, work location, and shipbuilding region. An individual shippard could estimate the productivity gain a weather protection facility at their shippard using the following formula.

$$P_a = P_a \times P_b \times P_c \cdots \times P_{n-1}$$

where

 $P_g$  = fraction productivity gain for each craft and location affected

Pa = fraction gain for that craft and location for a specific weather protection, e.g., wind

 $p_{b}$  = fraction gain for each craft, location, and second weather protection, e.g., shade

 $P_{\rm c}=$  fraction gain for each craft, location, and third weather protection, e.g., rain

 $P_n=$  continue for each additional weather protection category Then, taking the number of craft people protected by the facility Annual \$ saved each craft and location =  $P_g x$  effective annual wage expense for craft x number of craft people protected

Total \$ saved \{ \} \$ saved for each craft and location.

For illustration, assme the weather protection facility is a completely enclosed, unheated and uncooled, building for 35 welders in Baltimore. The building provides shade and complete protection from rain and wind. 'The estimated productivity gain (using factors for Baltimore from Table A-7) would be

$$P_g = {}^p \text{ shade } {}^{xp} P_{rain} \times Pwind -1$$
  
= 1.012 X 1.052 X 1.209-1  
= 0.287 (28.7%)

Assume the average annual expenditure per welder is \$20,000.

Then, the annual dollar savings for increased productivity for this facility would be (for 35 welders)

$$0.287 \times \$20,000 \times 35 = \$200,000$$

In other words, \$200,000 of additional work could be performed annually by these welders. A greater savings would result if overtime premiums were reduced, and an even greater savings would result if a greater shipbuilding capacity were achievable; i.e., to the extent that the welders were on the critical path. If other crafts were also protected from weather by this facility, the dollars saved would be added for each craft. The total dollars saved annually should be compared with the total annual dollar expenditure for each facility to determine the cost-effectiveness of the facility.

If this analysis appears cost-effective, the estimates of productivity which form the basis for the model (Table A-1) should be re-evaluated for the local situation and the analysis repeated, if lower productivity factors are indicated. Alternatively, new productivity estimates could be entered in the computer program data base, Appendix Land the program could be run to obtain new productivity factors.

#### EXHIBIT A

# ALGORITHM FOR PRECIPITATION COVERING PASS-OUT CORDITIONS AND TRANSFER OF WORKERS TO PROTECTED LOCATIONS

Workers will be passed out only for Precipitation rates greater than. .02"'/hr or, for painters and blasters only, for relative humidity occurrences greater than 90%. The occurrences of precipitation will be averaged over each shift in the following categories: .01"/hr; .02" - .09"/hr; .1" Or greater/hr.

- (1) All workers will work in .01"/hr precipitation at the reduced productivity rate. No pass-outs.
- (2) For the two precipitation categories of .02" and greater/hr, we will assume that 20% of the workers will be passed out sometime during the shift, and the remaining 80% will work the entire shift at the reduced productivity rate.
  - (a) We will assume that on the average the pass-outs will occur rather uniformly throughout the shift; that is:
    - (i) 1/4 of the time, the workers will be sent home at the beginning of the shift; work - 2 hours pay.
    - (ii) 1/4 of the time, the workers will be sent home after 2 hours; 2 hours work 4 hours pay.
    - (iii) I/4 of the time, the workers will be sent home after 4 hours; 4 hours work 4 hours pay.
    - (iv) I/4 of the time, the workers will be sent home with 6 hours work and 6 hours pay.

As shown in Table A-8 this can be sumarized as 7.2 hours (90%) are paid, on the average, for 7.0 hours (87.5%) work for these occurrences. The productivity during the work periods is, of course, reduced according to Table A-1.

- (b) In those cases where outside productivity would be zero, as for painters and welders, we will assume that 1 hour of each work day is lost transferring 80% of the workers to inside work. We will further assure the same 80% were transferred to inside work at the beginning of the shift in anticipation of precipitation. Table A-8 then becomes for these instances:
  - 7.2 hours pay
  - .6 hours outside work 100% productivity (average hours of outside work performed by the 20% of the workers before being passed out)
  - 5.6 hours inside work @ applicable productivity rate

 $\frac{\text{TABLEA-8}}{\text{Rate}}$ . Assumed Paid Time and Hours Worked When Precipitation Rate >.02"/Hr

| Fraction of Time | Fraction of Workers | Hours Pay | Weighted<br>Hours Pay | Hours<br><u>Work</u> | Weighted<br>Hours Work |
|------------------|---------------------|-----------|-----------------------|----------------------|------------------------|
| 1/4              | .2                  | 2         | .1                    | <b>0</b>             | 0                      |
|                  | .8                  | 8         | 1.6                   | 8                    | 1.6                    |
| 1/4              | .2                  | <b>4</b>  | .2                    | 2                    | .1                     |
|                  | .8                  | 8         | . 1.6                 | 8                    | 1.6                    |
| 1/4              | .2                  | 4         | .2                    | <b>4</b>             | .2                     |
|                  | .8                  | 8         | 1.6                   | 8                    | 1.6                    |
| 1/4              | .2<br>.8            | 6<br>8    | .3<br>1.6             | 6<br>8               | 1.6                    |
|                  |                     |           | 7.2                   |                      | 7.0                    |

#### EXHIBIT B

# EXPLANATIONS OF SPECIAL CONDITIONS AND PENALITIES MHICH APPLY TO THE PRODUCTIVITY TABLE A-1

(Comparisons are to all other crafts)

- (1) Painters will work outside only when actual temperature is 35°F or above.
- (2) Painters' productivity was penalized additional 5% for temperatures over 90°F because some paints cannot be applied in this temperature range.
- (3) Painters' productivity in wind is penalized additionally because of high paint losses; i.e., more spraying is required to achieve same coating thickness.
- (4) Painter will work outside only when the relative humidity is less than 90%. The effect of fog and other precipitation is included in the relative humidity affect.
- (5) Welders and fitters are penalized 5% when effective temperature is below 29°F caused by more preheating time and the effect of cold steel on the welders comfort.
- (6) Welders are penalized 5% when effective temperature exceeds 80" F for additional fatigues caused by heat radiation from hot steel.
- (7) Riggers are penalized 5% at temperatures <5°F because of reduced service availability of cranes.
- (8) Welders are penalized in wind because of greater difficulty in positioning parts, higher reject rates, and difficulty in maintaining gas shields for MIG and TIG welding.
- (9) Riggers and fitters are penalized in high wind reflecting difficulty in positioning structures, crane operations. Some operations must stop in winds in excess of 20 mph. Nearly all operations stop with winds in excess of 40 mph.
- (10) Extra penalties for welders for precipitation are brought about by extra time for drying joints, interrupted work, or rework. Penalties for other crafts reflect more difficult working conditions.
- (11) Fog directly affects only the crane operations and the riggers and fitters who work more closely with the crane operators.
- (12) The absence of shade tends to increase the effective outside temperature about 10°F causing an additional 30% loss of productivity in the sun when the temperature is above 80°F. We will assume that outside workers are in the shade half of the time.

#### EXHIBIT C

# ASSUMPTIONS OF PRODUCTIVITY FOR WORKERS PROTECTED BY THE SHIP'S STRUCTURE

Workers are generally protected from wind and rain. The effective temperature is the dry bulb temperature. These productivities assume no-additional heating, cooling, or dehumidifying, but assume minimum ventilation to remove fumes from painting and welding.

- (1) At temperatures above 80°F, a 5% penalty is assessed for buildup of heat from men and equipment. Heat from welding is assumed to cause an additional 5% penalty.
- (2) Heat provided by welding increases productivity to 100% in the temperature range of 30-39°F.
- (3) Painters' 70% productivity in 30-39°F temperature range reflects loss of productivity below freezing point, time waiting for temperature to rise, drying surfaces, etc.
- (4) Loss of productivity in high wind and rain is caused by increased difficulty and delays in supplying needed parts, tools, and materials; drafts, dust, leaks, and noise interfering with work and causing uncomfortable or more hazardous working conditions; hesitancy of workers to transfer between work stations involving exposure to the elements; extra work to secure parts and equipment; and general interdependency on some outside work.
- (5) Without drying equipment, relative humidity within ship is assumed to be the same as outside. In many instances, it is worse, particularly below the water line during outfilling.
- (6) Lack of shade is assumed to increase temperature within the ship, reducing productivity further

#### EXHIBIT D

#### ASSUMPTIONS TO BE USED IN THE CALCULATIONS

- (1) The annual hourly occurrences of effective temperature and dry bulb temperature will be used for the Productivity measurements for each' shift.
- (2) The percentage occurrence of wind will be averaged for each shift.
- (3) The percentage occurrence of precipitation and >90% relative humidity will be averaged for each full shift.
- (4) The annual % frequency of fog will be applied to each shift.
- (5) The correction for lack of shade will De made to that portion of the shift affected. We will assume shade and cloud cover are beneficial from 9 a.m. through 6 p.m. when the dry bulb temperature exceeds 80°F.

\_\_...

### APPENDIX B

#### WEATHER DATA FOR U. S. SHIPYARD LOCATIONS

A summary of annual weather observations near each shipbuilding location is presented in Exhibit A. These tables were taken from a "Summary of Hourly Observation" from the <u>Decennial Census of United States Climate, 1951-1960</u>, U. S. Department of Commerce. Exhibit A also contains precipitation data for Seattle and Mobile covering a five-year period and precipitation data for Newark, New Jersey, which was substituted for the missing precipitation data for New York International.

The tables in Exhibit A are reproduced from the best available copies. These data are not used directly in the computer model. For use in the computer model, these annual data were disaggregated into frequencies of occurrence for the three standard work shifts (Exhibit B). These data (Exhibit B) were input to our computer model and are the same data a shipyard would use.

# APPENDIX B, EXHIBIT A

ANNUAL SUMMARIES OF HOURLY WEATHER OBSERVATIONS

# A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

| WIND  |                   |  | 0-4 /                                      | uph,                                       |   |  |   |  | 5-14 /  | MPH   |                                       |  |                |   | 15-74    | MP.H. |  |  | Γ                | 25 M  | P.H.  | AND            | OVE                                       |   |  |
|---|-------------------|--|--|--|---|--|---|--|---|---|---------------------------------------|--|----------------|---|----------|-------|--|--|------------------|---|---|----------------|---|---|--|
| EEL<br>HAMMER   | 8                 | 8  |  | 2  |   |  | ¥   | 2  | 7   | 2   | 7                                     | 3  | E              | g.  | 2        | 2     | 2  | 8  | 2                |   | ,   |                | 2   | 6   | \$ 0 p   |
| Nasp<br>Cli   | ¥#                | À  | 3  | 76.791                                     | ŝ   | 8  | Šx  | *  | a de  | 78.70                                       | ŧ                                     | 8  | 3 x            | ¥   | i        | r e   | ğ  | 8  | 3×               | ¥   | Ĭ   | Ř              | i   | \$  | TOTAL  |
| 99/ 95 94/ 90 89/ 85 84/ 80 79/ 79 74/ 70 69/ 65 64/ 60 59/ 55 54/ 50 49/ 43 29/ 29 24/ 20 19/ 10 -01/-05 -05/-10 -11/-12 10TAL | + + + + + + + + \ | ++12400000000000000000000000000000000000 | + 25 9 1 1 1 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 | 13<br>18<br>18<br>18<br>13<br>17<br>4<br>2 | 27<br>25<br>27<br>27<br>27<br>21<br>15<br>14<br>12<br>5 | 112<br>115<br>99<br>88<br>79<br>82<br>53 | 4.0.4.2.2.1.1.1.4.4.1.4.4.4.4.4.4.4.4.4.4.4 | 8227-659-623-623-623-623-623-623-623-623-623-623 | 3 2 3 2 5 6 5 1 0 9 6 6 9 2 6 6 6 9 2 6 6 6 9 2 6 6 6 9 2 6 6 6 6 | 67<br>7 68<br>6 69<br>8 8 4 8 5 5 6 7 3 2 + | 8999<br>999<br>709<br>434<br>18<br>52 | 128<br>191<br>201<br>197<br>168<br>179<br>181<br>166 | 43442111+1++++ | + 3<br>4 1<br>11<br>19<br>20<br>26<br>24<br>22<br>24<br>18<br>20<br>18<br>5<br>17<br>11 | 23<br>30 |       | 9<br>10<br>14<br>16<br>15<br>16<br>42<br>1 | 29<br>41<br>46<br>47<br>51<br>49<br>17<br>13 | ÷<br>+<br>+<br>+ | + 1<br>1<br>1<br>1<br>1<br>1<br>2<br>2<br>2<br>2<br>2<br>1<br>1<br>1<br>1 | + + + + 1 1 1 1 1 1 1 2 4 4 4 3 1 1 + + 2 7 | 11111221111111 | * + 1 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 11<br>33<br>94<br>10<br>11<br>12<br>77<br>74<br>22<br>+ | 1<br>14<br>149<br>275<br>407<br>780<br>808<br>760<br>772<br>839<br>829<br>408<br>299<br>408<br>299<br>190<br>299<br>155<br>197<br>2767 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole number, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

#### OCCURRENCES OF PRECIPITATION AMOUNTS:

C

|                  |      |     |    |          |      | FRE        | JUEN | CY   | OF C | xccu | RRE | NCE  | FOR | EAC | Н Н | OUR | OF  | THE | DAY | ,     |     |    |    |     | Γ   |
|------------------|------|-----|----|----------|------|------------|------|------|------|------|-----|------|-----|-----|-----|-----|-----|-----|-----|-------|-----|----|----|-----|-----|
| INTENSITIES      |      |     |    |          | H F  | <b>SUC</b> | EKDI | NG A | τ.   |      |     |      |     |     |     |     | 4 H | OUR | CHD | NG A  | Ť   |    |    |     | 1 : |
|                  | •    | 2   | •  | 4        | 3    | 8          | ,    |      | •    | 10   | 111 | 40UW | •   | 2   | 3   | 4   | ,   | 6   | 7   |       | 5   | 10 | ** | 8-2 | G   |
| FMCE             | 31   | 2.6 | 27 | 25       | 31   | 34         | 34   | 33   | 33   | 35   | 33  | 31   | 32  | 33  | 36  | 37  | 37  | 34  | 33  | 35    | 34  | 34 | 30 | 31  | 9   |
| OI A             | 10   | 12  | 14 | i 14     | 11   | 10         | 10   | 10   | 9    | 8    | 8   | 7    | 7   | 7   | 2   | 8   |     | 12  |     |       | - 1 | 77 | 11 | 1.0 | 1 ; |
| 03 10 00 M       | 19   | 18  | 20 | 20       | 21   | 21         | 18   | 19   | 19   | 18   | 17  | 17   | 16  | 16  | 13  |     | 18  |     |     |       | ,   | 16 | 18 | 19  | 1 : |
| 16 TO 24 M       | 4    | 4   | 4  | ļ 6      | 5    | 6          | 5    | 5    | 5    | 4    |     | 4    | -5  | 5   |     | - 2 | 2   | -3  | - 2 | 1 ~ . | 4   | ** | 10 | 1.7 | 1   |
| 25 10 49 PI      | 1    | 1   | 1  | <b>,</b> | 1    | 1          | ,    | 1    |      | ,    |     |      |     | 1   | •   | ,   | -   | 1   |     | 1 7   |     | •  | 3  | -   | 3   |
| 10 TO 10 M       | 1 4  |     | 1  | ہ ا      | 1    |            |      |      |      | 1    | 1   |      | •   | ,   |     | •   |     | •   |     |       | •   |    | 1  | j 3 | 3   |
| 100 TO 100 M     |      | Ĭ   | Ī  | Ť        | '    | 1          | ' '  | '    | '    | •    | •   | 1 1  |     | 1   |     |     | 1   |     | •   | •     | l i |    | •  | 1   | 2   |
| BAND CHA IN OO S | 1 1  |     | 1  |          | Ī    | 1.         |      | l    | 1    | l    |     | 1 1  | 1   | •   | •   | •   | 1   | 7   |     |       |     |    |    | , ! | 1   |
| TOTAL            | 65   | 63  | 65 | 65       | 66   | 7,         | 6.6  | 48   | 46   |      | ١,, | 60   |     | 4.5 |     |     |     |     |     |       |     |    |    |     |     |
| 10176            | 1 22 | -33 |    |          | . 93 |            | 00   | 30   | 102  | 00   | 60  | LON  | 91  | 04  | 04  | 00  | 07  | 67  | 66  | 65    | 6.5 | 67 | 64 | 65  | 10  |

# PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|             |     |          |          |            | CEATN        | C (FEE       | )            |               |          |      |
|-------------|-----|----------|----------|------------|--------------|--------------|--------------|---------------|----------|------|
| (ARES)      | °   | ##<br>## | 38<br>48 | 250<br>100 | 1025<br>1436 | 2004<br>7700 | 3953<br>4600 | 3490.<br>1780 | OVE FIGE | 101. |
| 0 10 1/8    | 1.0 | .9       | +        | +          |              | •            |              | -             |          | 1.5  |
| 3/16 TO 3/8 | -3  | - 5      | - 1      | +          | +            |              |              |               | .1       | 1.0  |
| 1/2 TO 3/4  | +   | - 9      | . 5      | .2         | +            |              |              |               |          | 1.6  |
| 1 70 21/2   | +   | • 9      | 2.5      | 2.0        | •6           | -2           | •2           | . 3           |          | 7.4  |
| 3 10 6      | ĺ   | • 1      | • 9      | 2.7        | 1.5          | - ?          | •6           | 1.2           | 3.9      |      |
| 7 10 15     |     |          | •1       | 1.0        |              |              | 5.1          | 0.3           | 36.4     | 76.4 |
| 29 10 30    | 1 1 | . 1      | - 1      |            |              |              |              |               | 7 7 7    |      |
| 35 CR MORE  | , , | 1        |          |            |              |              |              |               | 1        |      |
| TOTAL       | 1.3 | 2.6      | 4.0      | 5.5        | 4.5          | 3. 7         | 6.2          | 10.6          | 51.5     | 300  |

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

|         | <del></del> |       | HOUR   | Y OBS   | RVATIC<br>M MAES I | NS OF   | WIND    | SPEED    |            |       |        |
|---------|-------------|-------|--------|---------|--------------------|---------|---------|----------|------------|-------|--------|
| BESCHOR | • :         | 4.7   | 0 - 12 | 13 19   | 10 - 34            | 25 - 21 | 37 - 36 | 70 - 44  | DVSE<br>LI | 1014  | 5480   |
| N       | .4          | 2.5   | 3.3    | 2.1     | •4                 | •1      | +       | +        |            | 8.9   | 10.5   |
| NNE     | -2          | 1.1   | 1.6    | 1.6     | . 4                | • 1     | +       | +        |            | 5.1   | 11.9   |
| NE      | • 1         | . 8   | 1.0    | 5       | .2                 | - 1     | +       |          | i          | 2.7   | 10.3   |
| ENE     | -1          | • 7   | 1.0    | 7       | • 2                | •1      | +       | +        | i .        | 2.8   | 11.6   |
| E       | •2          | . 9   | 1.5    | 1.0     | 2                  | •1      | +       | +        | +          | 3.9   | 11.1   |
| ESE     | -1          | • 7   | 1.0    | 3 .6    | į •1               | +       | +       | ŀ        | +          | 2.6   | 10.1   |
| SE      | .1          | • 7   | .6     | 4       | • 1                | +       | •       | j +      |            | 2.0   | 9.5    |
| SSE     | •2          | .8    | 1.5    | . 1.1   | ! •1               | -1      | +       | +        | i +        | 1 3.9 | : 11•2 |
| S       | -3          | 1.7   | 3.1    | 2.8     | •5                 | ' - 1   | +       | +        | :          | 8.5   |        |
| SSW     | .3          | 2.2   | 2.7    | 7, 1.4  | . +2               |         | ļ       | 1        | 1          | 6.9   | 9.5    |
| SW      | .4          | 2 . 5 | 2.5    | 1.0     | -1                 | +       | +       | 1        | į          | 6.6   | ,      |
| WSW     | .5          | 2.9   | 2.8    | 1.7     | .4                 | • 1     | +       | 1        | 1          | 8.4   |        |
| W       | •7          | 3.6   | 2.7    | r 1.5   | -4                 | -1      | +       | 1        |            | 9.1   | 9.2    |
| WNW     | -6          | 3.3   | 2.6    | 1 2 - 5 | • 3                | 1       | +       | 1        | 1          | 8.5   |        |
| NW      | .6          | 3.0   | 2.5    | 1.6     |                    |         | . +     | +        | 1          | 8.0   | 9.3    |
| HNW     | 63          | 2.2   | 2.4    | 1.6     | -3                 | +       | +       | l        | 1          | 7.2   | 10.2   |
| CALM    | 4.0         | 1     | 1      | 1       | !                  | 1       | l       | 1        |            | 4.6   | 4      |
| TOTAL   | 10.1        | 29.8  | 32.5   | 21.     | 4.3                | 1.2     | <u></u> | <u> </u> | ┸*-        | 100   | 9.6    |

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PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                   |          | OUG<br>LE O |          |          | IND      |           | 0                | RE       | ATIV      | E H       | DIML      | ITY (     | %)         |
|-------------------|----------|-------------|----------|----------|----------|-----------|------------------|----------|-----------|-----------|-----------|-----------|------------|
| HOUR<br>OF<br>DAY | 0.<br>3  | 47          | g.<br>10 | g.<br>3  | 4.<br>12 | 13.<br>24 | 25-<br>&<br>OVER | 0-<br>27 | 20-<br>49 | 50-<br>69 | 70-<br>79 | 80-<br>89 | 90-<br>100 |
| 00<br>01          | 42<br>42 | 10<br>10    | 47<br>48 | 15<br>16 | 70<br>65 | 14<br>15  | i.               | •        | 2         | 15<br>15  | 14        | 22        | 47<br>50   |
| 02                | 42       | 10          | 48       | 16       | 69       | 14        | ١i               | 1        | li        | 13        | 14        | 21        | 52         |
| 03                | 40       | 11          | 49       | 15       | 70       | 14        | l.i              |          | Ιi        | 12        | 13        | 21        | 53         |
| 04                | 37       | 12          | 50       | 15       | 69       | 15        | l'i              | 1        | Ιī        | lii       | 113       | 20        | 154        |
| 05                | 36       | 13          | 52       | 16       | 68       | 15        | 1                | l        | li        | 11        | 13        | 21        | 53         |
| 06                | 36       | 12          | 53       | 15       | 68       | 16        | 1                | +        | 1         | 14        | 16        | 23        | 46         |
| 07                | 35       | 12          | 53       | 12       | 67       | 19        | 1                | +        | 3         | 20        | 18        | 21        | 37         |
| 08                | 34       | 12          | 53       | 10       | 63       | 26        | 1                | +        | 8         | 32        | 18        | 16        | 26         |
| 09                | 3>       | 12          | 53       | 7        | 60       | 31        | 2                | 1:       | 16        | 37        | 14        | 12        | 20         |
| 10                | 34       | 13<br>16    | 53       | 5        | 57       | 36        | 2 2              | 1 2      | 23        | 38        | 12        | 10        | 1          |
| 11<br>12          | 30       | 17          | 52       | 3        | 50       | 44        | 3                | Ž        | 29        | 36        | 10        | 9         | 14         |
| 13                | 130      | 17          | 52       | Ž        | 46       | 47        | 1 3              | 3        | 131       | 135       | lio       | ĺś        | 11:        |
| 14                | 31       | 18          | 51       | 2        | 48       | 48        | 2                | 3        | 29        | 35        | 111       | 9         | 1          |
| 15                | 31       | 18          | 51       | 2        | 51       | 45        | 2                | 3        | 26        | 36        | 12        | 10        | 14         |
| 16                | 33       | 16          | 51       | 4        | 57       | 38        | 2                | 2        | 150       | 37        | 13        | 11        | 110        |
| 17                | 35       | 14          | 51       | 5        | 64       | 30        | 1                | 1        | 14        | 35        | 17        | 14        | 11         |
| 18                | 35       | 14          | 51       | 8        | 67       | 23        | 1                | 1        | 10        | 31        | 19        | 18        | 23         |
| 19                | 37       | 12          | 50       | 10       | 68       | 120       | 1                | ! *      | 1.2       | 27        | 19        |           | 2          |
| 20                | 40       | 11          | 49       | 12       | 64       | 18        |                  | ‡        |           | 24        | 17        | 21        | 134        |
| 21<br>22          | 41       |             | 48       | 14       | 65       | 17        |                  | 1 *      | 3         | 119       | 16        | 21        | 31         |
| 23                | 43       | lio         | 47       | 16       | 68       | 15        |                  | ١.       | ĺź        | 17        |           |           | 14         |
| ĀVG               |          | 13          | 51       | lio      | 163      | 26        |                  | Ιì       | 1,5       | 25        | 14        | 17        | 13         |

PORTLAND, MAINE Municipal Airport

B-3

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# A TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

| 104/100  | WWO  |                     |             | 64  | MPM   |   |   |                |                       | 5-14   | MPH  |  |  |                     |  | 15 24   | MPH                               |  |  | Π         | 25 M   | PH.  | AND         | OVI       | ,                    |   |
|--|--|---------------------|-------------|---|---|---|---|----------------|-----------------------|--|--|--|--|---------------------|--|---|-----------------------------------|--|--|-----------|--|--|-------------|-----------|----------------------|---|
| 99/ 95<br>94/ 90<br>89/ 85<br>84/ 80<br>4 1 2 4<br>79/ 75 4 2 4 4 2<br>69/ 65 4 2 8 11 14 25 8 52 139 100 121 121 13 45 64 23 22 22 25 5 3 2 3 4 8 59/ 55 4 2 6 8 13 23 10 55 121 79 97 127 12 49 60 28 29 34 2 6 4 1 6 8 7 7 7 12 5 55 130 73 87 75 61 8 53 78 30 36 44 2 10 8 2 3 11 7 12 12 4 55 141 77 63 79 5 63 115 37 41 61 13 13 3 6 21 8 32/ 27/ 25 14 7 3 2 2 4 4 7 3 6 7 7 10 3 55 138 49 38 59 50 70 94 24 21 38 2 14 13 2 3 19 6 94 70 10 10 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | cri  |                     | Ş           | 1   | Ę   | §   | 8   | 3.8            | ş                     | ş  | E  | eg .   | \$   | *<br>3×             | Ş  | Ş   | F                                 | £ 8  | 6.15   | \$ R      | Ę  | ٤  | Ę           | £         | 8 15                 | 101AL 085   |
| -11/-15<br>TOTAL 3 34 100 80 100 137 81 7741643 843 865 838 112 796 991 312 299 330 27126 94 30 40107187   | 99/ 95<br>94/ 90<br>84/ 80<br>79/ 75<br>74/ 70<br>69/ 65<br>64/ 60<br>59/ 35<br>34/ 30<br>39/ 35<br>34/ 30<br>19/ 10<br>14/ 10<br>09/ 05<br>04/-05<br>-01/-05<br>-06/-10 | * * * * * * * * * * | 22222334431 | 9<br>5<br>6<br>12<br>10<br>11<br>9<br>7<br>3<br>2 | 11<br>10<br>8<br>6<br>7<br>9<br>7<br>6<br>3 | 14<br>13<br>10<br>7<br>8<br>11<br>7<br>24 + | 21<br>23<br>15<br>12<br>11<br>12<br>10<br>2 | 8065343442+ ++ | 386862255259553221412 | 24<br>70<br>122<br>153<br>139<br>121<br>130<br>137<br>141<br>138<br>48<br>20<br>9<br>4 | 12<br>58<br>101<br>100<br>79<br>72<br>73<br>87<br>74<br>49<br>29<br>41 | 31<br>94<br>129<br>121<br>97<br>821<br>75<br>61<br>38<br>19<br>10<br>4<br>21 | 50<br>111<br>121<br>127<br>109<br>90<br>61<br>79<br>52<br>112<br>+ | 681083129855554421+ | 39<br>44<br>45<br>45<br>45<br>53<br>57<br>64<br>70<br>64<br>7<br>20<br>10<br>12<br>+ | 40<br>50<br>55<br>64<br>607<br>78<br>105<br>77<br>56<br>29<br>15<br>10<br>1 | 56 26 21 23 25 23 24 25 5 4 1 + + | 22<br>23<br>22<br>29<br>37<br>36<br>39<br>41<br>21<br>117<br>4 | 14<br>22<br>34<br>46<br>44<br>52<br>61<br>38<br>8<br>2 | 222222412 | 7<br>10<br>11<br>13<br>14<br>19<br>10<br>10<br>1 | 3<br>4<br>5<br>8<br>13<br>13<br>12<br>7<br>3 | 142632322++ | 634634211 | 14<br>20<br>21<br>19 | 757<br>828<br>848<br>674<br>429<br>256<br>151<br>74<br>35<br>4<br>9 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

#### C OCCURRENCES OF FRECIPITATION AMOUNTS:

|                |     |     |    |    | - 1 | FREC | UEN  | CY ( | OF C | xcu | RRE | NCE  | FOR | EAC | H H: | OUR | OF  | THE  | DAY        | ,    |     |    |    |     | Γ         |
|----------------|-----|-----|----|----|-----|------|------|------|------|-----|-----|------|-----|-----|------|-----|-----|------|------------|------|-----|----|----|-----|-----------|
| INTERSITIES    |     |     |    |    | MH  | OLR  | ENDI | IG A | r    |     |     |      |     |     |      | P   | M H | OUR  | ÉND        | NG A | ŧ-  |    |    |     | 80<br>(27 |
|                |     | 2   | ,  | 4  | 3   | •    | 7    | •    | •    | 10  | 115 | *CO* |     | 2   | 1    | 4   | ,   | •    | <b>_</b> , | •    | •   | 10 |    | **  | DAYS      |
| TRA-L          | 34  | 38  | 39 | 39 | 39  | 41   | 38   | 41   | 40   | 39  | 41  | 37   | 35  | 35  | 37   | 36  | 33  | 35   | 35         | 34   | 38  | 37 | 34 | 34  | 62        |
| O #4           | 10  | 10  | 12 | 12 | 13  | 10   | 11   | 11   | 10   | 10  | 10  | 9    | 10  | 10  | 9    | 11  | 12  | 11   |            |      |     |    |    | 12  | 16        |
| 67 10 07 M     | 17  | 15  | 16 | 17 | 15  | 17   | 20   | 16   | 16   | 17  | 15  | 16   |     | _   |      | 16  | 17  |      |            |      |     |    | :  | 17  | 38        |
| 10 24 M        | 6   | 7   | 7  | 5  | 6   | 5    | - 4  | 5    | 6    | 5   | 5   | 5    | 5   | 5   | 6    | 6   | 5   |      | -          | - 3  | - 4 |    | 5  | 6   |           |
| 23 TO 49 PM    | 1 1 | 2   | 1  | 1  | ī   | 1    | 2    | 1    | ī    | i   | ĺi  | 1    | 1   | ī   | ī    | 1   | ī   | 1    | 1          | 1    | 1   | 1  | 1  | ĭ   | 57        |
| 30 TO 99 M     | 1 + | -   | +  | 1  | 4   |      | +    | •    | +    | 4   | Ī   | 4    | +   |     | 1    | 4   |     | 4    |            |      | 1   | •  | 1  | • • | 31        |
| 100 10 195 44  | 1 1 | - 1 |    | -  | 1   |      | 1    |      |      | +   |     | 4    | -   |     | 1    |     | 1   | 1    |            |      | ľ   |    | 1  | . 1 | 2.        |
| 2 00 M AND CHE | 1 1 | - 1 |    |    |     |      |      |      |      |     |     |      | - 1 | - 1 |      | 1   |     | i 'i | •          |      |     |    |    |     |           |
| TOTAL          | 68  | 72  | 74 | 73 | 73  | 74   | 75   | 75   | 74   | 71  | 72  | 68   | 33  | 67  | 67   | 70  | 83  | 71   | 70         | 67   | Λo  | 60 | 60 | 40  | 106       |

PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|                      |      |            |     |             | THE.          | is Gif        | 0   |               |              |      |
|----------------------|------|------------|-----|-------------|---------------|---------------|-----|---------------|--------------|------|
| VISIBALTY<br>(MILES) | ۰    | 10A<br>200 | 83÷ | 538-<br>968 | 1300-<br>1600 | 5296.<br>1939 | =   | 2980-<br>0270 | Ovt3<br>9388 | 101. |
| 0 10 VS              | •    | +          | +   | •           | •             |               |     |               | -            |      |
| 3/14 TO 3/8          |      | +          | •   |             |               |               |     |               |              | ,    |
| 1/2 TO 3/4           | +    | +          | +   |             |               |               |     | •             | اء           | - 1  |
| 1 10 21/2            | 1 1  |            | 1   | 2           | 1             |               | اه  | •             | •            |      |
| 3 1O é               |      | +          | 1   | 3           | 2             | 1             | 1   | •             |              | 1    |
| 7 TO 15              | 1    | +          | +   | 2           | 3             | 3             | 5   | £             | 36           | 7    |
| 20 10 28             |      |            |     | _           |               |               |     |               | •            | - '; |
| 25 OR MORE           |      |            |     |             |               |               |     |               | 6            |      |
| TOTAL                | i +l | 3          | 2   | 6           | 6             | 3             | اما | 10            | 65           | 10   |

BOSTON, MASS. Logan Int. Airport

#### URRENCES:

|               |                     | 25 A                  | PH.                | NID I                                   | OVE  |                                | 4  |
|---------------|---------------------|-----------------------|--------------------|---|--|--------------------------------|--|
|               | S III               | ma                    | R.M.               | 33.75                                   | ##   | # · #                          | 101AL OBS  |
| 264246421882+ | ** NORRENEES **** * | +12343555670113490051 | +12123345833327331 | + 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 | 1423 0 5 4 6 5 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 124<br>104<br>201<br>2198<br>+ | + 10<br>39<br>39<br>127<br>245<br>433<br>676<br>819<br>766<br>757<br>768<br>828<br>848<br>674<br>429<br>256<br>479<br>151<br>74<br>35<br>49<br>9 |
| O             | 27                  | 128                   | 94                 | 30                                      | 40   | 107                            | 6767   |

Hivided by 10).
sums exactly
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| _   |    |    |          |           |      |
|-----|----|----|----------|-----------|------|
| ī Ā | ,  |    |          | —-j       | *2   |
|     | •  | 10 |          | <b>PC</b> | BATS |
| 34  | 38 | 37 | 36<br>11 | 34        | 62   |
| 18  | 15 | 15 | 16       | 17        | 38   |
| 3   | 1  | 1  | 5        | 1         | 24   |
| 4   | +  |    | +        |           | 21   |
| •   |    |    |          |           | 11   |
| 67  | 69 | 69 | 69       | 69        | 196  |

BOSTON, MASS. Logan Int. Airport

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

В

E

| į          | !     |     | HUHITI | CHICAGO<br>Marie | VAI: | N's (3) | WINE | 41111 |   |     | •     |
|------------|-------|-----|--------|------------------|------|---------|------|-------|---|-----|-------|
| Desiration |       |     | • "    | te (8 8          |      | · ·     | 47 # |       |   |     | ***** |
| M -        |       | 1   | 2!     | 2 :              | +    | • ;     | • '  | •     | • | 5   | 17.0  |
| NNE        | +     | 1   | 1      | 1:               | + .  |         |      | • • • | • | 3   | .13.3 |
| NE         | +     | 1   | 1      | 1 .              | 1 :  |         | • 1  | •     | • |     | 14.2  |
| ENE        | +     | 1   | 1      | 1                | 1    | +       | +    | , • i | • | 4   | 14.1  |
| E          |       | 1   | 2      | 2!               | +!   | •       | •    | + ;   | • | i 5 | 12.9  |
| 'ESE       | +     | 1   | 2      | 2 '              | •    | 4 1     | •    |       |   | 15  | 12.0  |
| SE.        | i + 1 | 1   | 2 :    | 1 :              | ٠.   | • !     | • 1  |       | • | 4   | 10.8  |
| SSE        | . +   | 1   | 1:     | 1.               | ٠.   | • ;     | . +  | + 1   | + | 3   | 110.4 |
| S          | +     | 1   | ' 2 '  | 1 '              | • i  |         | . •  | •     | • | 4   | 11.0  |
| SSW        | ٠.    | 1   | 3 !    | 2                | 1    | + 1     |      | . +   | • | 7   | 113-0 |
| SW         | : +   | l i | 4 '    | 5                | 1!   | •       | •    | +     |   | 12  | :13.3 |
| RSR        | . +   | 1   | . 3 '  | 3                | 1    | . •     | •    | •     |   | ' 7 | 13-0  |
| [W         |       | 1   | . 2    | 3                | 1 !  | +       | •    | +     |   |     | 14.2  |
| MNM        | . +   | 1   | 3 .    | 4 .              | 2 .  | 1       |      | • 1   |   | 11  | 14.6  |
| NW         |       | 1   | 3 :    | 4                | 2    | 1       | •    |       | • | 11  | 15.2  |
| NNW        | +     | 1   | 2:     | 3                | 1    |         | •    | i +   |   | 7   | 13.6  |
| CALM       | l 1   | 1   | - 1    | - 1              |      |         |      | 1     |   | 1 1 | 1     |
| TOTAL      | 3     | 12  | 33 :   | 35 ;             | 12   | 4       | 1    | •     | • | 100 | 13.3  |

## PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                   |         | נעט<br>פעט |           | W       | CiAt<br>Mi |           | D                | RE       | LATIN     | E M       | JAHO<br>- | 5TY ( | *          |
|-------------------|---------|------------|-----------|---------|------------|-----------|------------------|----------|-----------|-----------|-----------|-------|------------|
| HOUE<br>OF<br>DAY | Q.<br>3 | 4.<br>7    | \$-<br>10 | g.<br>3 | 4.<br>12   | 12-<br>24 | 25-<br>&<br>OYIR | 0-<br>29 | 30-<br>49 | 50-<br>49 | 76-<br>79 | 80-   | 90-<br>100 |
| 00                | 43      | - 8        | 49        |         | 53         | 39        | ~-<br>3          | •        | 10        | 34        | 18        | 19    | 20         |
| 01                | 42      | 9          |           | 4       | 54         | 38        | 3                | +        |           |           |           |       | 21         |
| 02                | 43      | 9          | 49        | 4       | 55         | 37        |                  |          | 6         |           |           |       | 23         |
| 03                | 42      | 9          | 50        | 4       | 56         | 36        | 4                |          |           | 31        | 18        | , 21  |            |
| 04                | 40      | 9          | 51        | 5       | 55         |           |                  |          | 7         | 29        | 19        | . 21  | 24         |
| 05                | 38      | 9          |           |         | 56         |           |                  |          |           |           | : 20      | 21    | 24         |
| 06                | 37      | 10         |           | 4       | 54         |           |                  |          |           |           |           | . 20  | 22         |
| 07                | 36      |            | 54        | 4       |            |           | 4                | +        |           |           |           | . 18  |            |
| 08                | 36      |            | 53        | 4       | 46         |           |                  | +        |           |           |           | , 14  | ; 15       |
| 09                | 36      | 11         | 53        | 3       | 43         |           |                  |          | 24        |           |           |       |            |
| 10                | 34      | 12         | 53        | j       | 40         |           | 7                |          | 30        |           | 11        |       |            |
| 11                | 32      | 15         | 53        | 2       | 38         |           |                  |          |           |           |           |       | 11         |
| 12                | 31      | 17         | 52        | 2       |            | 55        |                  |          | 36        | 30        |           |       |            |
| 13                | 30      |            | 53        | 1       | 32         |           |                  |          | 36        |           | 10        | -     |            |
| 14                | 31      | 17         | 52        | 1       | 31         | 60        |                  |          |           |           | 9         |       |            |
| 15<br>16          | 33      | 17         | 52        | 1       | 32         |           | 6                |          | 34        | 28        |           |       |            |
| 17                | 35      | 14         | 53        | 1       | 35<br>39   |           | 7                |          | 32        | 29        | , 11      | 10    |            |
| is                | 37      | 12         | 51<br>51  | 2       | 39         | 54        |                  | 5        | 29        |           |           |       |            |
| 19                | 38      | 12         | 50        | 3       | 47         |           |                  |          |           |           | 1.2       | 12    | 14         |
| 20                | 40      | 11         | 49        | 3       | 40         | •         | 4                |          | 21<br>17  |           |           |       |            |
| 21                | 40      | ii         | 60        | 4       | 49         | 43        |                  |          | 15        | 35        |           |       |            |
| 22                | 41      | 10         | 49        |         | 50         |           |                  |          |           | 35        |           | 18    |            |
| 23                | 42      | 9          | 69        |         | 52         |           | ;                | ¥        | lii       |           |           | 119   | ! ::       |
| ĀVG               | 37      | 12         | 51        | 3       | 46         | : 4£      | 5                |          |           |           | 114       | 15    |            |

#### TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

| wwo  |   |                | 041  | MPH .                                |   |                                  |                                   |  | 3 14  | WFH  |  |  |  |  | 15 74  | MPII   |  |   |  | 25 M  | PH .          | AHE: | CVIE                              |                              | 2  |
|--|---|----------------|--|--------------------------------------|---|----------------------------------|-----------------------------------|--|---|--|--|--|--|--|--|--|--|---|--|---|---------------|------|-----------------------------------|------------------------------|--|
| N  | ş,                                      | 6 11           | Ş  | **                                   | -   | -                                | ž,                                | ş  | ww  | 412  | BAR  | K IKS  | S X  | ş  | Ş  | 24   | K.M.   | ç,  | e<br>S m                               | Ş   | Ken           | £    | £ 22                              | ř.                           | 10°A: 013  |
| 04/100<br>99/ 95<br>94/ 90<br>89/ 85<br>84/ 80<br>79/ 75<br>74/ 70<br>59/ 65<br>64/ 60<br>59/ 55<br>54/ 40<br>39/ 35<br>14/ 30<br>19/ 25<br>14/ 10<br>19/ 05<br>14/ 10 | *************************************** | 13766555455623 | 20<br>15<br>16<br>17<br>18<br>16<br>23<br>19 | 14<br>16<br>14<br>15<br>10<br>4<br>2 | 31<br>24<br>21<br>18<br>19<br>17<br>16<br>6 | 43<br>40<br>30<br>28<br>23<br>27 | 89<br>64<br>4<br>2<br>1<br>2<br>1 | 23328<br>477761<br>7615554<br>464328<br>72744<br>72777 | 84<br>122<br>148<br>152<br>125<br>114<br>126<br>128<br>155<br>185 | 86<br>105<br>105<br>89<br>77<br>78<br>91<br>85<br>49<br>16 | 74<br>141<br>129<br>101<br>84<br>76<br>77<br>82<br>78<br>39<br>9 | 26<br>133<br>130<br>102<br>105<br>97<br>104<br>102 | 7<br>8<br>6<br>3<br>3<br>2<br>1<br>2<br>3<br>2 | 38<br>47<br>50<br>44<br>43<br>40<br>27<br>1<br>7 | 548<br>466<br>577<br>59<br>80<br>98<br>108<br>99<br>79<br>40<br>40 | 12<br>32<br>32<br>20<br>22<br>24<br>23<br>28<br>32<br>30 | 28<br>25<br>26<br>27<br>28<br>27<br>12<br>57 | 23<br>28<br>30<br>41<br>50<br>47<br>49<br>27<br>3 | 11 11 11 11 11 11 11 11 11 11 11 11 11 | + + + 1 1 1 2 2 2 3 3 3 3 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | 15<br>11<br>7 | •    | + 2 3 2 2 5 3 4 4 4 1 1 1 1 + 3 0 | + 3 6 4 6 11 14 9 10 6 22 72 | + 5<br>28<br>96<br>263<br>604<br>926<br>877<br>754<br>745<br>722<br>796<br>858<br>603<br>330<br>188<br>603 |

In Table A, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

OCCURRENCES OF PRECIPITATION AMOUNTS:

C

DATA NOT AVAILABLE

PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

| Ď   | •                     |    | CEL   | LINC |            | isib         |               | Y:           |              |              |     |
|-----|-----------------------|----|-------|------|------------|--------------|---------------|--------------|--------------|--------------|-----|
| Г   |                       |    |       |      |            | CERT         | े व्यक्त      | )            |              |              |     |
|     | VISIBILITY<br>(AMLES) | •  | 18 TO | ##   | 23±<br>103 | 1500<br>1900 | 3038-<br>3030 | 1030<br>4030 | 1980<br>1980 | £162<br>7160 | 101 |
| ۲   | 0 10 1/8              | +  | +     | +    | •          |              |               | +            | +            | +            | 1   |
| - 1 | 3/16/10/2/8           | +  |       |      | *          | •            | •             |              |              | +            | 2   |
|     | 1/2 10 2/4            |    | +     | +    |            |              | +             |              | •            | 4            | 1   |
| - 1 | 1 10 2 VZ             | li | +     | 1    | 1          | 1            | - 4           | +            | •            | 3            | 6   |
| -1  | 3 10 4                | +  | +     | 1    | 3          | 2            | 1             | 1            | 2            | 12           | 21  |
|     | 7 10 IS<br>20 10 39   | •  | *     | +    | 1          | 3            | 2             | 5            | 7            | 52           | 70  |
| L   | 35 GE MOSE<br>TOTAL   |    | _1    | 2    | 9          | و            | 3             | 7            | Q            | 67           | 100 |

| /#        |                                | 2   |
|-----------|--------------------------------|---|
| 4         | N . N                          | 10'A. CBS   |
| 232253444 | 11<br>14<br>9<br>10<br>22<br>2 | 5<br>28<br>94<br>243<br>604<br>926<br>877<br>754<br>745<br>722<br>796<br>838<br>858<br>503<br>330<br>188<br>22<br>26<br>10<br>13767 |

| В            |      |         |      |        |       | req<br>on |     |                  |    | ):                     |
|--------------|------|---------|------|--------|-------|-----------|-----|------------------|----|------------------------|
| . Leak James |      |         | IKR# | Y COES |       | 72, LH    |     | ware             |    |                        |
| ,            | • •  | • •     | •    | ** **  | 17 .4 | · ^ #     |     | , <del>-</del> ' | 4" | , e-44 , <b>V</b> 44** |
| N            | •    | 1       | 3    | . 5    | 1     | •         | ٠   |                  | ,  | 7 11.5                 |
| NHE          | •    | 1 1     | . 2  | . Z    | . 1   |           | •   | . •              |    | 6 11 6                 |
| iNE          | •    | 1 3 1   | Z    | . 1    |       | •         | •   | •                | •  | 5 .11.3                |
| ENE          |      | 1 1     | . 1  | 1      | •     | +         | •   | •                |    | . 4.30.4               |
| E            |      | 1       | 1    | 1      | +     | +         |     | +                |    | 3 10.7                 |
| ESE          | +    | 1 1     | 1    | 1      | •     | . +       | •   |                  |    | 3 10.5                 |
| S€           | •    | 1 1     | î    | 3      | +     | •         | •   |                  |    | 3 .11.2                |
| :SSE         | +    | 1 1     | 2    | 2      | 1     | . +!      |     | 1                |    | 6 12-5                 |
| SSE          |      | 2       | 4    | 3      | . 1   |           |     |                  |    | 10 12-2                |
| SSW          |      | 2       | 4    | . 3    | . ī   | •         | •   |                  |    | 9.11.4                 |
| SW           |      | 2       | 3    | 1 2    | ` ;   |           |     | 1 :              |    | 8 10-6                 |
| WSW          |      | 1 7     | 1    | ٠ - 5  |       |           |     |                  |    | 8 12.4                 |
| 'W           |      |         | 2    | 2      | : ;   |           |     | •                |    | 1 6 14.0               |
| WNW          | ! I  | ;       | 2    |        |       |           |     |                  | •  |                        |
| INW          |      | 1 : 1   |      |        | : :   | I         |     | , T              | ļ. | 8 14.5                 |
|              | i I  | 1 :     | 2    | 3      | · :   |           | •   |                  |    | 8 14-1                 |
| NNW          | : :  | i * I   | ~    | 2      | 1 1   | *         | •   | •                | l  | 7 :12 - 7              |
| CALM         | 2    | ا ۔ ۔ ا |      |        | ١     | ١ ـ       |     | 1 .              |    | 2 !                    |
| ITOTAL       | L_6. | iI 7i   | 35   | L 2.8  | 170   | l 3 .     | L . | l. <b>-</b> +.   | ٠  | 100.112.0              |

PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND E RELATIVE HUMIDITY:

|           |         | re o |          | W       | IND<br>IAL |           | D                | RE       | LATH      | E H       | UMID      | ITY (     | (%)        |
|-----------|---------|------|----------|---------|------------|-----------|------------------|----------|-----------|-----------|-----------|-----------|------------|
| OF<br>EAY | g.<br>3 | 4-7  | 8-<br>10 | o 3     | 4 12       | 13-<br>24 | 25-<br>&<br>0771 | 0-<br>29 | 39.<br>47 | 50-<br>69 | 70-<br>79 | 50-<br>69 | 50.<br>100 |
| 00        | 46      | 11   | 42       | 9       | 61         | 28        |                  | +        |           |           | 17        | 21        | 24         |
| 01        | 46      | 10   | 44       | 9       | 62         | 27        | 2                | +        |           |           | 17        | 21        |            |
| 02        | 45      | 11   | 44       | 10      | 61         | 27        | 2 2              | <b>+</b> | 5         | 29        | 17        |           | 27         |
| 03        | 46      | 10   | 44       | 11      | 61         | 27        |                  | †        | ! 5       | 28        | 17        |           | 28         |
| 05        | 40      | 12   | 46       |         | 61         | 26<br>25  | 2                | •        | 5         | 27        | 17        | 22        | 30         |
| 06        | 37      | 13   |          |         |            |           |                  | l        | 1         | 27<br>29  | 18        |           | 30         |
| 07        | 35      | 14   | 51       | 9       | 56         | 32        | 5                | +        |           |           | 18        | 20<br>20  | 28         |
| 08        | 35      | 13   | 52       | 7       | 52         |           |                  | +        | 11        |           | 16        |           | 22         |
| 09        | 35      | 14   |          | 6       | 50         |           |                  | 1        | 16        | 40        | 15        | 13        |            |
| 10        | 35      | 16   | 50       | 4       | 48         | 44        |                  | i        | 25        | 38        | 14        |           | 12         |
| 11        | 33      | 16   |          | 3       | 45         |           |                  | 2        | 30        | 36        | 12        |           | 11         |
| 12        | 32      |      | 50       | 2       | 43         | 50        |                  | 3        | 33        | 34        | ii        | 9         | 10         |
| 13        | 32      | 18   | 50       | Z       | 40         | 53        | 5                | 3        | 34        |           | ii        |           |            |
| 14        | 31      | 19   | 50       | 2 2 2 2 | 37         | 56        |                  | 5        | 32        | 34        | 11        | 9         | Í          |
| 15        | 32      | 18   | 50       | 2       | 30         |           |                  | 5        |           |           |           | 20        | 9          |
| 16        | 32      | 16   |          |         |            |           |                  | 4        | 26        |           |           |           | 10         |
| 17        | 33      | 17   | 49       | 2 2 3   | 45         | 49        |                  | 3        | 22        | 35        |           |           | 11         |
| 18        | 35      | 24   | 48       | 3       | 49         | 45        | 4                | 2        | -19       | 34        | 17        |           | 14         |
| 19        | 38      | 15   | 47       | 5       | 53         | 39        |                  | 1        | 15        |           |           | 17        | 16         |
| 20        | 41      | 14   | 45       | 6       | 54         | 37        | 3                | 1        | 13        |           |           | 19        | 18         |
| 21        | 44      | 13   | 43       | 7       | 57         | 34        |                  | 1        | 12        |           | 19        | 19        | 20         |
| 22        | 45      | 13   | 42       | 7       | 59         | 32        |                  | +        | 11        | 30        | 19        | 20        | 20         |
| 23        | 45      | 12   | 43       | 8       | 60         | 30        |                  | +        | 9         | 30        | 17        | 21        | 22         |
| AVG       | 98      | 14   | 47       | 6       | 52         | 38        | 3                | 1        | 16        | 33        | 16        | 16        | 10         |

NEW YORK, NEW YORK Int. Airport (Idlewil

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# TEMPERATURE AND WIND SPEED-RELATIVE HUMIDITY OCCURRENCES:

| No.   No. | MO  |                             |  | 0-4 A   | APH  |  |   |                |  | 514 -  | APH   |  |  |              |  | 15-24   | MPH   |   |  |           | 25 M                  | PH.                       | AHD                                     | CYCE    |  | *   |
|---|---|-----------------------------|--|---|--|--|---|----------------|--|--|---|--|--|--------------|--|---|---|---|--|-----------|-----------------------|---------------------------|---|---------|--|---|
| 7 95       1       1       1       1       10       1       1       2       1       2       1       7       4       6       1       1       1       1       1       1       1       1       1       1       7       7       4       2       2       1 <th>-</th> <th>\$</th> <th>£</th> <th>Ş</th> <th>Ę</th> <th>£</th> <th></th> <th>S R</th> <th>Š</th> <th><b>C</b></th> <th>PP-44</th> <th>wa</th> <th>4</th> <th>REPOR</th> <th>ų,</th> <th>Ş</th> <th>É</th> <th>É</th> <th><u>{</u></th> <th>1<br/>12</th> <th>ş</th> <th>ş</th> <th>Ę</th> <th>£</th> <th>4</th> <th>  0  </th>  | -   | \$                          | £  | Ş   | Ę  | £  |   | S R            | Š  | <b>C</b>   | PP-44   | wa   | 4  | REPOR        | ų,   | Ş   | É   | É   | <u>{</u>                                     | 1<br>12   | ş                     | ş                         | Ę                                       | £       | 4  | 0   |
| ITAL 14 152 351 292 384 408 018092 875 875 815 849 53 474 493 126 140, 191 3 31 23 7 10 178767  | 95/850/850/850/850/850/850/850/850/850/85 | 1 + 1 2 2 2 2 2 1 1 + 1 1 + | 15<br>16<br>15<br>10<br>10<br>11<br>10<br>10<br>10<br>11<br>10 | 25<br>28<br>29<br>22<br>23<br>27<br>29<br>23<br>35<br>18<br>7<br>21 | 26<br>27<br>30<br>27<br>20<br>25<br>32<br>27<br>13<br>27<br>13<br>27 | 45<br>45<br>45<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43<br>43 | 60<br>67<br>46<br>41<br>34<br>35<br>34<br>29<br>64<br>1 | 14118533122114 | 37<br>69<br>102<br>105<br>94<br>80<br>77<br>70<br>61<br>70<br>52<br>31<br>17 | 138<br>146<br>148<br>128<br>118<br>113<br>126<br>140<br>159<br>164<br>100<br>102 | 86<br>96<br>93<br>82<br>70<br>61<br>71<br>73<br>88<br>63<br>26<br>10<br>7 | 84<br>121<br>104<br>84<br>78<br>67<br>64<br>60<br>74<br>45<br>16<br>63 | 120<br>118<br>99<br>97<br>87<br>77<br>81<br>75<br>49<br>61 | 765544322222 | 36<br>35<br>46<br>47<br>48<br>42<br>29<br>18 | 28<br>225<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27 | 13<br>10<br>13<br>14<br>12<br>15<br>62<br>4 | 13<br>15<br>15<br>15<br>17<br>16<br>6<br>4<br>3 | 12<br>17<br>19<br>23<br>23<br>31<br>31<br>15 | 1 1 1 1 1 | 1 1 2 2 4 4 5 4 3 1 1 | + + + 1 1 1 2 3 2 2 2 2 4 | 111111111111111111111111111111111111111 | 1 1 1 + | + 21<br>11<br>12<br>11<br>13<br>22<br>31<br>1+ | 74<br>225<br>420<br>655<br>864<br>808<br>735<br>710<br>663<br>701<br>758<br>818<br>654<br>335<br>169<br>100<br>32 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

#### OCCURRENCES OF PRECIPITATION AMOUNTS:

C

| INTENSITIES       | -    |    |    |    | M H | OUR | ENCK | NG AT | _  |     |    |       |    |    |    |    | м н | CUR | ENDH       | G AT | ,  |    |    |     | ×   |
|-------------------|------|----|----|----|-----|-----|------|-------|----|-----|----|-------|----|----|----|----|-----|-----|------------|------|----|----|----|-----|-----|
|                   | -    | 7  | ,  | 4  | •   | •   | 7    | •     | •  | 10  | 11 | 40712 | •  | 1  | 1  | 4  | •   | •   | ,          | •    | •  | 10 | 11 | •0  | 12. |
| TRALE             | 24   | 25 | 26 | 27 | 26  | 27  | 30   | 30    | 33 | 32  | 31 | 26    | 29 | 29 | 28 | 26 | 27  | 25  | 26         | 27   | 27 | 25 | 26 | 25  |     |
| • •               | 8    | 7  | 7  | 7  | 8   | 7   | 8    | 8     | 6  | 7   | 6  | 8     | 7  | 5  | 6  | 6  | 6   | 7   | C          | 7    | 9  | 7  | 8  | 7   | ] 1 |
| e2 10 <b>60</b> m | 13   | 16 | 15 | 14 | 13  | 16  | 14   | 14    | 13 | 13  | 13 | 13    | 12 | 13 | 13 | 14 | 14  | 13  | 13         | 13   | 12 | 14 | 15 | 14  | 1 3 |
| 10 24 m           | 5    | 5  | 9  | 5  | 6   | 5   | 5    | 3     | 3  | 27  | 3  | 3     | 3  | 3  | 3  | 4  | 3   | 3   | 4          | 4    | 3  | 4  | 4  | 4   | 4 3 |
| 15 10 es m        | 1    | 1  | 1  | 1  | 2   | z   | 1    | 2     | 1  | 2   | +  |       | 1  | •  | 1  | 1  | 1   | 1   | 1          | 2    | 1  | 1  | 1  | 1   | L   |
| 10 99 44          | 4    |    | +  | +  | +   | +   |      | +     | +  | +   | +  |       | +  | +  | +  |    | +   | +   | 1          | 1    | •  | +  | •  | +   | 1   |
| 40 'O 199 PI      | 1    |    | *  |    |     |     |      |       |    | 1 1 |    | •     |    |    | *  | *  | -   | +   | +          | •    |    |    | !  |     | 1   |
| 00 M MG THER      |      |    |    |    |     |     | ŀ    |       |    | 1 1 |    |       |    |    |    |    |     |     |            |      |    |    |    | +   | 1   |
| OTAL              | 1 51 | 53 | 54 | 54 | 54  | 56  | 58   | 57    | 57 | 55  | 54 | 50    | 52 | 52 | 51 | 53 | 51  | 50  | <u>5</u> 2 | 53   | 52 | 51 | 54 | _52 | 1   |

# PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|                  |   |       |           |     | CERA       | o ver         |               |              |              |     |
|------------------|---|-------|-----------|-----|------------|---------------|---------------|--------------|--------------|-----|
| WEELTY<br>WEELTY | • | 10.20 | 386<br>45 | 159 | 188<br>188 | 2333-<br>2700 | )595-<br>(160 | 2006<br>9100 | 0+58<br>7340 | 101 |
| e 10 1/8         | • | •     | +         | •   | *          |               | •             | •            | •            |     |
| 3/14 TO 3/2      |   | +     | •         |     | •          | •             | •             | •            | +            | •   |
| 1/2 TO 2/4       | • | +     | •         |     | +          |               | +             | +            | +            | 1   |
| 1 10 21/2        | l | +     | 3         | 2   | 2          | •             | +             | •            | 3            |     |
| 3 10 4           |   |       |           | 3   | 3          |               | ?.            | 3            | 16           | 2   |
| 7 10 15          |   |       | +         | 1   | 2          | Z             | 5             | 7            | 46           | 6   |
| 30 TO 38         | 1 |       |           | i : | 1          | +             |               | •            | +            |     |
| 35 OR MORE       | • |       |           | i   |            |               |               | ļ.           |              |     |
| POTAL            |   | 1     | 2         | . 6 | . 6        |               | 1_7           | 10           | 66           | 10  |

PHILADELPHIA, PENNA. Int. Airport

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#### CURRENCES:

|   |   | 25 M               | PH .         | AND                                    | CVER   |         | 4   |
|---|---|--------------------|--------------|--|--|---------|---|
| \$<br>\$  | i                                       | ž                  | Ę            | £                                      | <b>BM</b>                                      | 88.16F6 | 101AI 01S   |
| 3<br>10<br>12<br>17<br>19<br>23<br>23<br>33<br>31<br>15<br>42 | + + 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | ++++11122445543111 | +++1+112324+ | 11 11 11 11 11 11 11 11 11 11 11 11 11 | +<br>1<br>+<br>2<br>1<br>1<br>2<br>1<br>1<br>+ | +22     | 17<br>74<br>225<br>420<br>654<br>868<br>735<br>710<br>663<br>701<br>818<br>654<br>335<br>169<br>100<br>32 |
| 191   | 5                                       | 31                 | 23           | 7                                      | 10   | 17      | B767  |

1 divided by 10). ir sums exactly n 0.5.

| 1    |    |    | • • |    |          |
|------|----|----|-----|----|----------|
| HG A |    |    |     |    | 8        |
| 27   | 27 | 25 | 26  | 25 | 59       |
| 1 7  | 9  | 7  | 20  | 7  | 10       |
| 1 13 | 12 | 14 | 15  |    |          |
| 1 4  | 3  | 4  | 4   | 4  | 25<br>19 |
| 2    | 4  |    | +   | +  | 20       |
| 1    |    |    |     |    | 8        |
| 4 53 | 52 | 51 | 54  | 52 | 175      |

PHILADELPHIA, PENNA. Int. Airport

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# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

В

E

| BERCHON |            |     |      | Y 08% |       |      |     |    |             |          | _    | , 44   |
|---------|------------|-----|------|-------|-------|------|-----|----|-------------|----------|------|--------|
|         | 10.1       | .,  | • 17 | 13 4  | 19 34 | 25 4 | 111 | 26 | » 4         | , UV10   | 1014 | 7/10   |
| ٧       | +          | -2  | 7    | 7     |       | 1    | 7   | +" | <del></del> | ŧ        | t    | 9.     |
| INF.    | +          | 1   | 2    | . 1   | . +   | ! +  | 1   | •  |             | 1        | ! 6  | 10.    |
| YE.     |            | 1   | 1    | 1     | , +   |      | i   | +  | i           | !        | 3    | 11.    |
| ENE     | i +        | 1   | ' 2  | ! 2   | ۱ 💠   | +    | ī   | +  | !           | ļ        | 6    | 12.    |
| Ē       | +          | 1 1 | 2    | 1     |       | : .  | i   | ÷  | ł           | <u>!</u> | . 4  | ii 0 . |
| ESE     |            | 1   | 1    |       | . +   | 1 +  |     | ٠  | !           | :        | 9    |        |
| E       | +          | 1   | 1    |       |       |      | į   | •  | •           | +        | ; 3  | . 8.   |
| SSE     | 1 +        | 1   | : 1  |       | : •   | . +  |     | •  | •           | :        | : 3  | 7.     |
| 5       | . +        | 2   | 1    | . 1   |       |      | •   |    |             | ٠ ٠      |      | . 8.   |
| SSW     | . +        | 2   | . 2  | ĺ     | . +   | ! .  | ı   |    | +           | •        | ' 6  | 10.    |
| SW      | · +        | ! ž | . 4  | Ž     |       |      | !   | +  | i           |          |      | . 9.   |
| rsw     | : •        | . 3 | 5    | · ž   | ٠ +   | : .  |     | +  | •           |          | 11   | . 9.   |
| i       |            | : 2 | ιž   | 1     | +     |      | •   | •  | ;           | :        |      | . 9.   |
| INV     | ; <b>+</b> | , 2 | 3    | 2     | , I   |      | 1   | •  | . +         |          | 1 8  | 111    |
| 44      | 4          | 2   | ز ا  | : 2   | 1     | ٠ ٠  | !   |    |             | 4        | . 7  | :ii.   |
| WAY     | +          | Ž   | , 2  | 1 2   | ĭ     | ! +  | 1   | ٠  | +           | l        | 7    | 11.    |
| CALH    | i 7        | -   | -    |       | :     | i    | 1   |    |             | 1        | 7    | 1      |
| TOTAL   | 111        | 27  | 35   | . 21  | . 5   | . 1  | 1   | •  | •           |          | 100  | ' 9.   |

## PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                  |            | LE O | -10      |         | HCD<br>CM 9 |       | D                | RE       | LATIN     | /E H      | UMID | itY      | (%)<br> |
|------------------|------------|------|----------|---------|-------------|-------|------------------|----------|-----------|-----------|------|----------|---------|
| OUR<br>OF<br>DAY | <b>a</b> 3 | 4-7  | 8.<br>10 | Q.<br>3 | 4-<br>12    |       | 25-<br>E<br>CYLE | G-<br>29 | 30-<br>49 | 50-<br>69 | 1    |          | 98-     |
| 00               | 46         | 9    |          | 15      | 67          | 18    | 1                | L        | 6         | 27        |      |          | 22      |
| 01               | 44         | 10   | 45       | 16      | 67          | 17    | +                | ı        | . 6       |           | 19   |          | :25     |
| 02               | 44         | 11   | 45       | 18      | 65          | 17    |                  | ı        | 5         | 125       | 18   | 124      | .28     |
| )3               | 43         | 10   | 46       | 19      | 64          | 16    | 1                | l        | 4         | 23        | j 18 | 124      | 131     |
| 74               | 41         | 11   | 48       | 18      | 65          | 17    | +                |          | 4         | 123       | 18   | 23       | 133     |
| 05               | 37         | 13   | 50       | 19      | 83          | 188   | *                | +        | 1 3       | '22       | 18   | '23      | 34      |
| 06               | 34         | 14   | 52       | 19      | 62          | 19    | 1                | i +      |           |           | 19   |          | 131     |
| 37               | 33         | 14   | 53       | 15      | 63          | 21    | 1                | +        | 5         | 29        |      | 22       | 125     |
| 08               | 33         | 14   | 53       | 12      | 60          | 27    | 1                | +        | 10        |           | , 18 | 19       | :17     |
| 09               | 33         | 16   | 51       | 11      | 57          | 31    | 1                | +        | 19        | 39        | .15  | 14       | 13      |
| 10               | 32         | 17   |          | 8       | 57          | f · _ | 2                | 1        | 28        | • -       | 12   | 10       | ļIO     |
| 11               | 30         |      | 50       | 7       | 54          | 37    | 2                | 3        |           | 36        |      |          | . 8     |
| 12               | 29         |      | 51       | 5       | 54          | 38    | 2                | •        | 42        |           | 9    | j •      | ; 7     |
| 13               | 27         | 20   | 53       |         | 52          | 41    | 2                | !        | 45        |           |      |          | 7       |
| 14               | 27         | 23   | 51       |         | 52          | 41    | 2                | 7        | 140       | 28        |      | 6        | 6       |
| 15               | 27         | 22   | 51       | 5       | 51          | 41    | 2                | 7        | 47        |           |      | 6        | 1 7     |
| 16               | 29         | 20   | 50       | 5       | 55          |       | 2                |          |           | 30        | •    | 7        | 1 7     |
| 17               | 33         |      | 48       |         | 61          | 32    | 1                | 1 2      | 36        |           | ; 8  | . 7      | !       |
| 18               | 36         |      | 48       |         | 66          |       | 1                | 2        | 28        |           | 111  | ! .9     | ! 9     |
| 19               | 38         |      | 47       | 6       |             |       | 1                | ] }      | 1 7 7     | 42        | 115  | 111      | 110     |
| 20               | 42         |      | 45       | 9       | 9           | 20    | ! ;              | 1        | 113       | 41        | ,19  | :::      | :32     |
| 21<br>22         | 44         | 12   | 44       | 10      | 70          |       | 1                | 1 7      | 110       | 36        | 22   | 147      |         |
| 23               | 46         | 10   | 44       | 14      | 67          | 19    | lī               | ! !      | ! 6       |           |      | 120      | 117     |
| AVG              | 36         | 15   | 49       | 11      | 42          | , = : | i                | 2        | 20        |           | :22  | 23<br>15 | .19     |

| 14/70   |  | Ι                     |      |                    |                | 04 N   | LFJA.                                    |   | L.                                       |                   |   |                            |           |    |   | 5-14  | MPH.  |   |  |  |  | 15-74  | МРН  |   |  |           | 25 N | PK                    | ANO | OVE |         | 4  |
|---|--|-----------------------|------|--------------------|----------------|--------|--|---|--|-------------------|---|----------------------------|-----------|----|---|---|---|---|--|--|--|--|--|---|--|-----------|------|-----------------------|-----|-----|---------|--|
| 19/ 99  | - 1  | -                     | art. | 1                  |                | Ş      | er, et                                   | ş | ş  | ş                 |   | £                          |           | Į, | Ş   | Ş   | £ g   | ş   | 9.381.48   | 8<br>5:2   | 4  | Ę  | Ke   | BATT                                    | 414                                      | 5.2       | 16.4 | Ş                     | E   | Ę   | ## 100/ | TOTAL ORS  |
| 19/ 49 1 9 16 10 17 30 3 74 124 64 77 67 4 50 50 12 12 20 4 5 4 7 3 5 164 4 6 1 1 1 1 2 5 1 1 1 7 7 8 8 7 8 8 8 8 8 8 8 8 8 8 8 8 | 99887766556455050500000000000000000000000000 | NONCHONONCHONCIONUNG. |      | и филимили и ф ф ф | PROBERT STREET | 170777 | 10 10 10 10 10 10 10 10 10 10 10 10 10 1 |   | 14 11 11 11 11 11 11 11 11 11 11 11 11 1 | 17 19 19 19 4 N + | 19 22 22 24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 29<br>36<br>36<br>31<br>21 | 203333444 | 11 | 71<br>91<br>96<br>70<br>62<br>66<br>68<br>74<br>65<br>49<br>21<br>11<br>5 | 101<br>149<br>149<br>124<br>109<br>1124<br>175<br>115<br>115<br>115<br>115<br>115<br>115<br>115<br>115<br>115 | 61<br>91<br>98<br>98<br>83<br>71<br>64<br>74<br>87<br>143 | 99<br>139<br>122<br>109<br>97<br>64<br>29<br>64<br>29<br>64 | 47<br>153<br>120<br>119<br>109<br>109<br>113<br>14 | State of Sta | 47<br>50<br>53<br>43<br>19<br>11<br>36<br>47 | 39<br>50<br>66<br>67<br>44<br>23<br>10<br>61 | 15<br>14<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15 | 111111111111111111111111111111111111111 | 24 22 24 24 24 24 24 24 24 24 24 24 24 2 | 1 4 4 4 4 | 1    | 3<br>3<br>2<br>2<br>1 | 1   | •   |         | 23<br>109<br>263<br>4355<br>583<br>794<br>729<br>683<br>673<br>770<br>755<br>642<br>3284<br>89<br>43<br>72 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Yelues are rounded to the mearest whole, but not adjusted to make their sums exactly equal to column or row totals. "4" indicates more than 0 but less than 0.5.

## OCCURRENCES OF PRECIPITATION AMOUNTS:

C

|                |                |    |    |    | 1     | FREC | HJEH | CY ( | JF C | ECU | RRE | KCE | FOR | EAC | нк | DUR | OF    | THE | DAY  | •    |     |    |     | į          | ١.  |
|----------------|----------------|----|----|----|-------|------|------|------|------|-----|-----|-----|-----|-----|----|-----|-------|-----|------|------|-----|----|-----|------------|-----|
| INTENSITIES    |                |    |    |    | 1 M F | 25/2 | CHOI | iG A | 7    |     |     |     |     |     |    | P   | M. F. | DU9 | ENDE | KG A | 7   |    |     |            | 20  |
|                | $\blacksquare$ | 2  | •  | 4  | •     | •    | 7    |      | •    | 10  | 11  | *** | •   |     | 3  | 4   | 5     | 6   | 7    |      | •   | 10 | **  | <b>#-0</b> | WI  |
| TRACE          | 124            | 24 | 24 | 24 | 23    | 27   | 25   | 30   | 29   | 20  | 24  | 24  | 25  | 26  | 24 | 24  | 23    | 22  | 23   | 23   | 25  | 24 | 25  | 25         | 5   |
| 4 #            | 3              | 6  | 6  | 6  | 7     | 6    | 7    | 7    | 8    | 7   | 8   | 6   | 6   | 7   | 6  | 8   | 7     | 8   | ε    | 7    | 6   | 8  | - 6 | 8          | 1   |
| M 70 00 0      | 13             | 14 | 15 | 14 | 135   | Ìè   | 14   | 13   | 13   | 13  | 13  | 12  | 12  | 12  | 14 | 13  | Î4    | 14  | 13   | 13   | 13  | 14 | 14  | 13         | 3   |
| 10 34 M        | 1 4            | 3  | 4  | 5  | 3     | 4    | 4    | 3    | 3    | 4   | 4   | 4   | 3   | 4   | 3  | 4   | - 4   | 4   | 4    | 4    | 4   | 4  | 4   | 4          | 1 2 |
| 15 16 44 FE    | 1              | 1  | 1  | 1  | 1     | 1    | +    | 1    | 1    | 1   | +   | +   | +   | 1   | 1  | 1   | 1     | 1   | 1    | 1    | 2   | 1  | 1   | 1          | l : |
| <b>* * * =</b> | 4              | 4  | ب  | ٠  | 1     | ٠    |      | ب    | ب    | ب   | ٠   | 1   | ب   | ي   | +  | 1   | *     | ٠   | ٠    | •    | 1   | چ  | 2   | ٠          |     |
| NO TO 110 PI   | 1 1            |    |    | +  |       |      |      | ŀ    |      |     |     |     | l   | +   | +  | +   | +     |     |      | +    | +   |    |     | . +        | İ   |
| 80 M M OKE     | 1 1            |    | 1  |    |       |      |      |      |      |     |     | li  | 1   |     |    |     | ! !   | 1   |      |      | 1 1 |    | +   |            | ĺ   |
| CTAL           | 50             | 46 | 49 | 49 | 45    | 53   | 55   | 52   | 54   | 52  | 49  | 49  | 47  | 49  | 49 | 21  | 50    | 50  | 50   | 45   | 51  | 51 | 51  | 51         | 1   |

# PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|             |     |     |             |              | CIU           | 3 ៥៣         | 1     |               |              |     |
|-------------|-----|-----|-------------|--------------|---------------|--------------|-------|---------------|--------------|-----|
| (MEE)       | ٠   | 184 | 298.<br>499 | 100-<br>1780 | 1805.<br>1686 | 5385<br>5385 | 27ES- | 2758-<br>1753 | CNG3<br>1288 | 161 |
| e 10 1/3    | +   | +   | •           | +            | +             |              | +     | +             | •            |     |
| 2/14 10 2/8 | +   |     | •           |              | +             |              | +     | +             | +            |     |
| 1/2 TO 3/4  | •   | •   | 4           |              |               | •            | +     | +             |              |     |
| 1 10 21/2   | +   |     | 1           | 2            | 1             | •            | +     | +             | 1            |     |
| 2 10 4      |     | _+  |             | 2            | ?             | 2            |       | 2             | 2            | _1  |
| 7 10 15     |     | •   | •           | +            | 2             | 1            | 4     | 6             | 44           | 3   |
| 20 70 59    | 1 ( |     |             |              |               | +            | 1     | 1             | 15           | 1   |
| 35 OR MORE  |     |     |             |              |               |              |       |               | +            |     |
| TOTAL       |     | 1   | 2           |              | ٥             | 3            | 6     | _ 10          | 691          | 10  |

A

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

,

B

|           |     |     | HOUR   |       |         | NS OF | WIND    | SPEED        |     |       | 40    |
|-----------|-----|-----|--------|-------|---------|-------|---------|--------------|-----|-------|-------|
| 9-49CH\$N | 0.3 | 4.7 | 8 - 17 | 13 19 | 19 - 20 | 25 31 | 22 - 24 | <b>**</b> ** | 47  | 10"44 | 57100 |
|           |     | 1   | 2      | 1     | +       | +     |         | i            | T   | 3     | 9.1   |
| NNE       |     | i   | i      | ī     |         |       | +       | ı            | 1   | 3     | 20.1  |
| NE        |     | ĺ   | 2      | 1     |         | +     | +       | +            | l   | 5     | 10.5  |
| ENE       |     | ī   | 2      | lī    |         |       | +       |              | +   | 5     | 10.5  |
| Ē         |     | i   | 2      | ī     |         | ٠ ا   |         | ł            | t   | 5     | 9.1   |
| ESE       |     | l ī | Ĭ      | 1     | +       |       | +       | +            | i   | 3     | 6.5   |
| SE        |     | i   | Ž      | 1     |         | +     |         |              | +   | 4     | 9.5   |
| SSE       | 1 + | li  | 2      | i i   |         | ١ +   | i +     |              | ٠.  | 4     | 110.8 |
| 5         |     | Ž   | 3      | ī     |         |       | +       |              | 1   | 7     | 9.8   |
| SSW       | 1   | li  | 2      | i     |         |       |         | +            | l   | 6     | 10.   |
| SW        |     |     | 3      | 1 1   |         |       |         | 1 +          | 1   | l a   | 9.4   |
| WSW       | 1 + | 2   | 3      | l i   | 1       |       |         | i i          | ł   | 1 6   | 9.9   |
| <u> </u>  | l è | 1 2 | 4      | 2     | 1       | ٠ +   | 1 +     |              | i + | 9     | 111.2 |
| MWM<br>-  | 1   | Ž   | 3      | 3     | 2       | 1     |         | 1            | 1   | 1 11  | 13.   |
| NW        |     | 2   | 1      | 3     | l ī     |       | +       | +            | i   | 10    | 12.   |
| NNW       | 1 + | lī  | Ž      | li    |         |       |         |              | 1   | 5     | 111.  |
| CALM      | 1   | 1 - | 1      | 1     | 1       | 1     | 1       | ı            | (   | 3     |       |
| TOTAL     | 1 7 | 24  | 19     | 22    | 6       | 9     |         |              | ٠.  | 1200  | 110-  |

# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND E RELATIVE HUMIDITY:

|           |             | CUD<br>LE 0 |          | W  | י או     |           | Đ                | RE       | ATR              | E H      | CHAL      | ITY (     | %)         |
|-----------|-------------|-------------|----------|----|----------|-----------|------------------|----------|------------------|----------|-----------|-----------|------------|
| OF<br>DAY | <b>6</b> -3 | 47          | 8.<br>13 | də | 4-<br>12 | 13-<br>24 | 25-<br>&<br>0128 | 0-<br>29 | 33-<br>49        | <b>છ</b> | 70-<br>79 | 69-<br>67 | 90.<br>109 |
| 00        | 49          | 11          | 40       | 8  | 72       | 19        | 1                | +        | 5                | 25       | 18        | 25        | 26         |
| 01        | 49          | 11          |          | 9  | 72       | 19        |                  | +        |                  |          | 18        | 25        | 28         |
| 02        | 38          | 11          | 41       |    | 71       | 19        | 1                | •        | 4                | 22       | 16        | 24        | 32         |
| 03        | 49          | 9           | 42       |    |          |           | 1                |          | 3                | 21       | 18        | 24        | 33         |
| 04        | 46          | 11          | 43       | 9  |          | 19        |                  |          | 3<br>2<br>2<br>3 | 20       | 18        | 25        | 35         |
| 05        | 43          | 13          |          |    | 71       | 18        | 1                | ١.       | 2                | 20       | 17        | 25        | 36         |
| 06        | 39          | 14          |          | 20 | 71       | 20        | 1                |          | Z                | 21       | 16        |           |            |
| 07        | 37          | 14          |          |    | 69       |           |                  |          |                  | 25       | 19        |           | 29         |
| 08        | 37          | 14          | 69       |    |          | 26        |                  | *        | 7                |          | 20        |           | 20         |
| 09        | 38          | 15          | 47       |    | 57       |           |                  | 1        | 16               |          | 16        |           | 13         |
| 10        | 37<br>33    | 17          | 46       |    | 55       |           |                  | 2 2      | 27<br>35         |          | 12        |           | 12         |
| 11<br>12  | 31          | 20          | 47       | 6  | 51<br>51 | 40        | 3                | 4        | 132              |          | 10        | 7         | 10         |
| 13        | 31          | 22          | 46       |    |          | 42        | 3                |          |                  |          | 8 7       | 6         | 1          |
| 14        | 31          | 23          | 47       | 4  | 46       |           |                  |          |                  |          | 7         | 5         |            |
| 15        | 33          | 22          |          |    | 48       |           |                  |          |                  |          |           |           | ľ          |
| 16        | 34          | 18          |          |    | 52       |           | 3                | 7        | 40               |          | 8         | 5         | 1          |
| 17        | 39          |             |          |    | 59       |           |                  |          | 33               |          | 9         | 7         | 3          |
| ii        | 41          |             |          |    |          |           | 1                | 1 3      |                  |          |           | 9         | 1          |
| 19        | 42          |             |          |    | 60       |           |                  |          | Zo               |          | 15        | 12        | 1          |
| žó        | 45          |             |          |    |          |           | li               |          |                  |          |           | 16        | li         |
| 21        | 48          |             |          |    |          |           |                  |          | ,                |          | 20        | 19        | i          |
| žž        | 45          |             |          |    |          |           |                  |          |                  |          |           | 22        | Ž          |
| 23        | 49          |             |          |    |          |           |                  |          |                  |          | 19        |           | 2          |
| AVG       | 41          |             |          |    |          |           |                  |          |                  |          |           |           | 19         |

BALTIMORE, MARYLAND Friendship Int. Airpor

#### TEXT LATURE AND WAND EXED-RELATIVE HUMBERY COMPERAGES.

| wee  |    |       | 94   | MJR            |   |  |          |  | \$-14   | M.P.H.   |   |   |                  |                     | 13-34          | MP.H                                 |   |                                  |      | es m  | or.             | / <b>/</b> 20                          | CVSE        |           |   |
|--|----|-------|--|----------------|---|--|----------|--|---|--|---|---|------------------|---------------------|----------------|--------------------------------------|---|----------------------------------|------|---|-----------------|--|-------------|-----------|---|
| PROVING.   |    | 6     | 8  | £              | 8 | 5  |          | E  | •   | 2  | \$  | 8   | 9                | •                   | •              | £                                    | ٤   | 10 14C/6                         | E C. | £   | 30.0            | Parps.                                 | 10 St.      | 01234     | AL 088.   |
| <u></u>  | 1  |       |  | 2              |   | •  | g,       | *  | 4   | £  |   | •   | 25               | *                   | *              | ž.                                   | Ŕ   | ž                                | 38   | #   | #               | 盘                                      | 8           | 8         | TOTAL   |
| 164/166<br>99/ 93<br>94/ 83<br>84/ 80<br>79/ 60<br>69/ 65<br>59/ 35<br>54/ 50<br>49/ 40<br>39/ 35<br>34/ 30<br>29/ 25<br>24/ 20<br>19/ 13<br>14/ 10<br>10/ 10/ 10/ 10/ 10/ 10/ 10/ 10/ 10/ 10/ | 11 | 10010 | 28<br>26<br>20<br>15<br>19<br>25<br>27<br>23<br>17<br>12 | 29<br>22<br>20 | 1 | 96<br>67<br>60<br>41<br>48<br>40<br>34<br>19 | 455423++ | 12<br>40<br>47<br>54<br>56<br>47<br>54<br>59<br>64<br>33<br>27<br>17 | 136<br>161<br>156<br>137<br>102<br>102<br>115<br>139<br>114<br>70<br>33 | 17<br>104<br>122<br>105<br>77<br>74<br>66<br>70<br>58<br>10<br>1 | 157<br>114<br>99<br>06<br>71<br>70<br>72<br>48<br>25<br>2 | 138<br>102<br>103<br>97<br>77<br>75<br>69<br>17 | ++1225555332++14 | 3051999555642362131 | 54<br>65<br>59 | 36<br>29<br>19<br>21<br>13<br>9<br>6 | 58545555<br>5854555<br>5855<br>5855<br>5855<br>5855<br>58 | 61<br>30<br>21<br>20<br>35<br>20 | **** | + 2 2 1 1 1 2 + 2 3 2 2 2 2 1 1 1 1 1 2 4 2 2 2 2 1 1 1 1 2 4 2 2 2 2 | +122492829349++ | 11<br>12<br>22<br>31<br>11<br>11<br>11 | HWARNIHAL++ | .6329532+ | 1<br>19<br>1297<br>524<br>916<br>1079<br>920<br>820<br>820<br>757<br>668<br>724<br>727<br>558<br>371<br>175<br>61 |

In Table A occurrences are for the average year (10-year total divided by 10). In Table C occurrences are for the average year (5-year total divided by 5). Values are rounded to the nearest whole number, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C 1/56 - 12/60 OCCUPRENCES OF PRECIPITATION AMOUNTS:

|              |        |    |     |    | 1     | FREC         | WEN  | CY ( | ¥ C | ccu | RRE | KCΣ  | FOR | EAC | нк | OUR | CF   | THE | DAY  | ,    |    |     |    |     | Γ   |
|--------------|--------|----|-----|----|-------|--------------|------|------|-----|-----|-----|------|-----|-----|----|-----|------|-----|------|------|----|-----|----|-----|-----|
| INTENSITIES  |        |    |     |    | LEA F | <b>3</b> ,31 | ENOR | G AT |     |     |     |      |     |     |    |     | M. H | OUA | EKDZ | ig a | r  |     |    |     | 8   |
|              | $\Box$ | 2  | ٩   | 4  | 9     | •            | 7    | •    | •   | 10  | 11  | 3000 | •   | 2   | 3  | 4   | 5    | •   | ,    | 8    | •  | 10  | 11 | 803 | 1   |
| TRACE        | 26     | 36 | 25  | 22 | 22    | 29           | 25   | 25   | 27  | 24  | 24  | 27   | 25  | SS  | 22 | 2   | 25   | 24  | 36   | 26   | 26 | 20  | 26 | 27  | 4   |
| 66 M         | 9      | •  | 6   | 8  | 3     |              | - 5  | ્ય   | 6   | 6   |     | 7    | 7   | 7   | 7  | 7   | 7    | E   | £    | Ę    | 6  | d   | 7  | 7   | 1 1 |
| 64 10 66 ML  | 111    | 11 | 12  | 13 | 17    | 24           | 14   | 12   | 12  | 11  | 12  | 12   | 13  | 11  | 14 | 16  | 15   | 13  | 12   | 12   | 11 | 12  | 12 | 15  | 3   |
| 16 TO 34 M   | 2      | 2  | 4   | S  | 3     | 2            | 9    | 4    | 3   | 4   | 5   | 3    | 3   | - 4 | 3  | 5   | 9    | G   | 4    |      | 4  | - 9 | 2  | •   | 2   |
| 25 TO 40 RL  | 1 1    | 1  | 2   | 1  | 2     |              | 1    | 1    | 2   | 1   | i   | i    | i   | 1   | 2  | 2   | Ē    | i   | 2    | 1    | 2  | 1   | 1  |     | 1 3 |
| 20 TO 50 M   | 17     | 1  | *   |    | 1     | 1            |      | - 1  | 1   |     | Ī   | 2    | •   | 1   | 4  | ĩ   | -    | 1   | 1    | 4    |    | 4   | 4  |     | ī   |
| 80 TO 190 St |        | •  | 1   |    |       |              |      |      | . ] |     |     | l T  |     | •   | 1  | •   |      | +   |      | 1    |    |     |    |     | li  |
|              | 1      |    | i 1 |    | l i   |              | l l  | .    |     |     | ł   |      | +   |     |    |     | 1    |     |      | Ĭ    |    |     |    |     |     |
| TOTAL        | 52     | 52 | 52  | 50 | 49    | 45           | 49   | 49   | 49  | 47  | 46  | 20   | 40  | 40  | 50 | 52  | 55   | 53  | 52   | 52   | 52 | 6.2 | 51 | 52  | hs  |

PERCENTAGE FREQUENCIES OF CEILING-VIERBILITY:

|            |     |             |            |          | C.            | 3 (12)         | )   |     |              |      |
|------------|-----|-------------|------------|----------|---------------|----------------|-----|-----|--------------|------|
| (MESS)     | ۰   | 165-<br>723 | 255<br>424 | <b>*</b> | 1086-<br>2703 | \$283<br>\$223 | =   | 400 | Over<br>1980 | 901. |
| 6 TO 1/8   | •2  | •2          | +          | +        | +             | +              | -   | +   | • ž          | • 6  |
| 3/4 10 2/8 | +   | •9          | +          | +        |               |                | +   | +   | •1           | •4   |
| 1/2 10 2/4 | +   | . 5         | •2         | • 2      | •             | +              | +   | +   | •1           | •    |
| 1 10 21/2  | 1   | •3          | •9         | 1.0      | •3            | •1             | • 2 | •2  | 1.2          | 4.2  |
| 3 FD 4     |     | ?           | •7         | 3.€      | 2.1           | 8.0            | 1.9 | 2.4 | 38.8         | 38.6 |
| ,7 tO IS   |     | +           | +          |          |               |                |     |     | 2106         |      |
| 30 70 30   |     |             |            |          |               |                |     |     |              |      |
| 35 CR MORE |     |             |            |          |               |                |     | 1   |              | ŀ    |
| . TOTAL    | • 2 | 1.1         | 1.9        | A. 0     | A-7           | 8.1            | 5.6 | 2.0 | 70.6         | 100  |

NORFOLK, VIRGINIA Municipal Airport

## DITY OCCURRENCES:

| - | MPH  |   |  |                         | 25 M | PH.  | NIC         | 0/128        |  | 4          |
|---|--|---|--|-------------------------|------|------|-------------|--------------|--|------------|
| Ī | M.T.   | £                                       | P HIT  | ## ## ##                | B.C. | F-57 | Trans.      | <b>#</b> 655 | *                                      | TOTAL COS. |
|   | 2<br>17<br>30<br>44<br>38<br>36<br>29<br>19<br>19<br>21<br>13<br>6 | 765255555555555555555555555555555555555 | 10<br>10<br>29<br>41<br>30<br>21<br>28<br>35<br>20<br>13 | * * * * * * * * * * * * | 2    | +    | 11222112111 | 123521131+++ | 69<br>55<br>63<br>11<br>35<br>53<br>24 | 14         |
| ú | 283  | 290                                     | 245  | 3                       | 24   | 31   | 16          | 19           | 40                                     | \$767      |

total divided by 10).
otal divided by 5).
djusted to make their
s more than 0 but

## HOUNTS:

| R | OF    | THE | DAY  |       |     |     |     |     |     |
|---|-------|-----|------|-------|-----|-----|-----|-----|-----|
| 7 | M. Fr | CUR | EMON | €G A1 |     |     | _   |     | 3   |
|   | 3     | 6   | ,    | ٥     | •   | 10  | 11  | 443 |     |
| 4 | 25    | 24  | 26   | 26    | 26  | 28  | 26  | 27  | 47  |
| 7 | 7     |     | E    | न     | - 6 | 4   | - 7 | 7   | 11  |
| 4 | 15    | 13  | 12   | 12    | 3.1 | 12  | 13  | 15  | 53  |
| 9 | 爿     | 5   | 4    | 4     | 4   | 9   | 3   | 3   | 23  |
| 2 | 3     | 1   | 2    | દ     | 2   | ્ય  | 2   |     | 20  |
| 1 | +     | 1   | 1    | +     | - 1 | +   | •   | ŀ   | 17  |
| + | +     |     |      | 1     | •   |     |     |     | 14  |
| - | - 1   |     |      |       | - 1 |     |     |     | 3   |
| 2 | 35    | 53  | -52  | 52    | 57  | 5.3 | 53  | 52  | 164 |

)F

| **  | 07E  | NOT. |
|-----|------|------|
| ++  | •1   | • 6  |
| • 2 | 1.2  | 4.2  |
| • 4 | 10.1 | 33.3 |
| •   | 70.4 | 160  |

NORFOLK, VIRGINIA Municipal Airport

B-8

# PERCENTAGE PREQUENCES OF WEND DEPECTION AND SPEED:

В

E

|          |      |      | HOUE   |         |         | 745 CF         |            | 17 <b>9</b> 90 |   |       |     |
|----------|------|------|--------|---------|---------|----------------|------------|----------------|---|-------|-----|
| BHECTION | 0.3  | 4.7  | 8 - 12 | 12 - 19 | 19 - 34 | <b>26 · 36</b> | <b>2.3</b> | 27 - 44        | 4 | 101.M | -   |
| N        | - 5  | 1.1  | 1.7    | 2.1     | • 7     | •1             | +          |                |   | 4.5   | 11  |
| MALE     |      | 1.4  | 2.5    | 2.7     | •7      | -1             |            |                | 1 | 7.6   | 32  |
| NE       | 1    | 1.0  | 3.2    | 2.9     | • 7     | •1             | +          |                |   | 904   | 11  |
| ENE      | .6   | 1.2  | 2.0    | 1.9     | .5      | •1             | +          | +              | + | 6.2   | 11  |
| Ē        | .9   | 1.3  | 1.2    | .5      | •1      | +              | +          | l              | ł | 4.1   | 1 7 |
| ESE      | .7   | 1.1  | 1.0    | .4      | +       | +              | +          | 1              | İ | 3.3   | 1 7 |
| SE       | 1.0  | 1.5  | 1.2    | .5      | .1      | +              | +          | 1              | + | 4.2   | 7   |
| SSE      |      | 1.5  | 1.4    | .7      | 61      | •              | +          | +              |   | 4.4   | i a |
| S        | 1.3  | 2.5  | 2.4    | 1.1     | • 2     | +              | +          | l              |   | 7.5   |     |
| SSW      | 9    | 2.4  | 3.4    | 2.5     | -4      | •1             | +          | +              | ŀ | 9.7   | 10  |
| SW       | 1.2  | 2.6  | 3.9    | 3.3     | -5      | •1             | +          |                | Ī | 11.6  | 10  |
| WSW      | .7   | 1.3  |        |         | .4      | -1             |            |                | ! | 6.0   | 10  |
| K        | .7   | 1.1  | 1.3    | 1.1     | .4      | -1             |            | +              | ŀ | 4.7   | 10  |
| MAK      | .4   |      | 1.1    | 1.4     | .5      | •1             | <b>j</b> + | l              |   | 4.2   | 12  |
| MX       | .6   | 1.1  | 1.2    | 1.2     | .5      | •1             | +          | +              | l | 4.6   | 11  |
| KKA      | .3   | • 7  | 1.0    | 1.4     | .5      | •1             | +          | i              | + | 4.0   | 12  |
| CALH     | 1.9  | 1    |        |         | 1       | i -            |            |                | l | 1.9   | 1   |
| TOTAL    | 13.6 | 23.3 | 30.2   | 25.2    | 6.2     | 1.3            | -2         | +              | + | 100   | 10  |

## PERCENTAGE FREQUENCIES OF SKY COVER, LYIND, AND RELATIVE HUMIDITY:

|                   |      | 962<br>18 0 |    | ٧,       | KID<br>(AL F |           | 89               | E3       | ATR              | 7E 8H     |           | 67Y (     | %)         |
|-------------------|------|-------------|----|----------|--------------|-----------|------------------|----------|------------------|-----------|-----------|-----------|------------|
| HOUR<br>OF<br>DAY | e- 3 | 4-7         | 10 | e 3      | &-<br>12     | 13-<br>24 | 23-<br>&<br>0172 | 6-<br>29 | 30-<br>47        | 10-<br>69 | 79.<br>79 | 85-<br>57 | 99.<br>165 |
| 00                | 49   | 12          | 39 | 20       | 55           | 24        | 1                | +        | 4                | 20        | 18        | 28        | 29         |
| 01                | 49   | 13          | 38 | 19       | 56           | 24        | 1                | +        | 4                | 19        | 17        | 27        | 32         |
| 02                | 49   | 12          | 40 | 20       | 54           | 25        | 1                | 1        | 3                | 18        | 17        | 27        | 35         |
| 03                | 46   | 12          | 40 | 21       | 53           | 25        | 1                | 1        | 3                | 18        | 15        | 27        | 97         |
| 04                | 46   | 13          | 41 | 20       | 53           | 26        | 1                | +        | 3<br>2<br>2<br>3 | 17        | 15        | 27        | 33         |
| 05                | 43   | 14          | 43 | 21       | 53           | 25        | 1                | ļ        | 2                | 17        | 15        | 26        | 39         |
| 06                | 39   | 14          | 47 | 19       | 53           | 27        | 1                | l        | 2                | 17        | 17        |           | 35         |
| 07                | 38   | 14          | 49 | 14       | 54           | 31        | 1                | ŀ        |                  | 21        | 21        | 29        | 26         |
| 08                | 37   | 15          | 48 | 11       | 52           | 36        | 1                | +        | 6                | 31        | 25        | 22        | 16         |
| 09                | 38   | 15          | 47 | 8        | 50           | 40        | 1                | +        | 12               | 41        | 22        | 15        | 10         |
| 10                | 39   | 14          | 47 | 7        | 49           | 42        | 2                | +        | 19               |           |           | 11        |            |
| 11                | 37   | 16          | 47 | 6        | 46           | 44        | 2                | 1        | 26               | 45        | 13        | 8         |            |
| 12                | 36   | 18          | 46 | 5        | 48           |           | 2                | 2<br>3   | 31               | 42        | 12        |           |            |
| 13                | 35   | 19          | 45 | 4        | 48           |           | 2                | 3        | 34               | 39        | 11        |           |            |
| 14                | 35   | 19          | 46 | 4        | 49           |           | 2                | 4        | 35               | 37        | 11        |           |            |
| 15                | 36   | 18          | 46 | 4        | 51           |           | 2 2              | 4        | 34               | 37        |           |           |            |
| 16                | 35   | 18          | 47 | 6        | 55           | 37        |                  | 3        | 30               | 39        |           |           |            |
| 17                | 36   | 17          | 47 | 10       | 58           | 31        | 1                | 2        | 22               | 40        |           | 11        |            |
| 18                | 38   | 15          | 47 | 13       | 60           |           | 1                |          | 15               | 38        | 20        |           | 11         |
| 19                | 40   | 15          | 46 | 16       | 60           |           | 1                | •        | 11               | 34        | 21        | 19        |            |
| 20                | 43   |             | 43 | 19       | 58           |           | 1                |          | 7                | 27        |           | 24        | 17         |
| 22                | 45   | 14          | 42 | 19       | 57<br>55     | 22        | 1                | +        | 6                | 25        |           | 27        | 21         |
| 23                | 46   |             |    | 20       |              | 24        | 2                | *        | 6                |           | 20        |           | 24         |
| AVG               | 41   | 12<br>15    | 40 | 20<br>14 | 54<br>53     | 25<br>31  | 1 2              | i        | 13               | 21        | 19<br>17  |           | 26         |
| MAG               | 74   | 13          | 77 | 4.4      | 73           | 121       | 4                | 1 1      | 1 23             | 30        | 11/       | 19        | 19         |

| <b>PHD</b>   |            |                                | 04 A   | AP.H.  |                      |                        |                      |  | 5-14 A  | AP.H.  |                         |  |  |                            | 15-24                            | мрн.                 |  |   |                  | 25 M        | P.H.         | u+o                     | OVER      |         | ø  |
|--|------------|--------------------------------|--|--------|----------------------|------------------------|----------------------|--|---|--|-------------------------|--|--|----------------------------|----------------------------------|----------------------|--|---|------------------|-------------|--------------|-------------------------|-----------|---------|--|
| 3[]  | g<br>52    | Ę                              | 5  | THE ST | £                    | -                      | 9<br>5 R             | ¥.   | M. OFF.   | A. W.  | 4                       | FE-10FE  | 59   | Š                          | 20.00%                           | 47.4                 | Tary to  | No iera   | #<br>5 A         | 29-473      | 20-46%       | 70.7T&                  | ***       | 98-100% | TOTAL COS  |
| 1700<br>1795<br>1790<br>1790<br>1770<br>1790<br>1790<br>1790<br>1790<br>1790 | ++=======+ | 43<br>149<br>667<br>876<br>422 | + 14 1 2 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | . 6    | 92<br>48<br>27<br>18 | 167<br>228<br>92<br>71 | 16<br>17<br>15<br>11 | 19<br>71<br>69<br>65<br>47<br>53<br>56<br>57<br>49<br>28<br>19 | 2<br>80<br>261<br>170<br>122<br>96<br>86<br>95<br>96<br>107<br>93<br>70<br>46<br>31 | 41<br>179<br>114<br>88<br>67<br>65<br>60<br>64<br>52<br>32<br>15<br>71 | 272<br>171<br>123<br>97 | 312<br>450<br>318<br>261<br>152<br>102<br>56<br>22 | 1<br>2<br>3<br>5<br>7<br>11<br>9<br>11<br>10<br>5<br>2 | 25<br>30<br>35<br>29<br>27 | 37<br>34<br>28<br>28<br>35<br>31 | 20<br>18<br>17<br>17 | 1<br>7<br>35<br>47<br>31<br>21<br>16<br>17<br>17 | 4<br>13<br>64<br>69<br>46<br>28<br>20<br>18<br>97 | 1<br>+<br>+<br>1 | +++1111321+ | +11212212212 | + n n n n n n n n + + + | 1241111++ | ٤       | 2<br>30<br>208<br>536<br>750<br>1341<br>1411<br>1038<br>882<br>698<br>609<br>506<br>377<br>214<br>109<br>49<br>7 |
| ITAL   | 16         | 87                             | 165  | 147    | 297                  | 675                    | 102                  | 633  | 1374  | 866  | 1090                    | 1697   | 67   | 273                        | 439                              | 250                  | 237  | 274   | 4                | 10          | 19           | 18                      | 13        | 17      | 3767   |

In Table A, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

OCCURRENCES OF PRECIPITATION AMOUNTS:

C

DATA NOT AVAILABLE

PERCENTAGE FREQUENCIES OF CEILING—VISIBILITY:

D

|                       |     |            |    |             | CELLIN | G (PEET       | }             |               |              |     |
|-----------------------|-----|------------|----|-------------|--------|---------------|---------------|---------------|--------------|-----|
| VISIBILITY<br>(AMLES) | •   | 140<br>220 | ** | ##-<br>1930 | 1006-  | 3006-<br>2100 | 2506-<br>4600 | 3536-<br>1360 | OVSE<br>7500 | POF |
| 0 TO 1/8              | +   | +          | +  | +           | +      | •             | 4             | *             | +            | 1   |
| 3/16 TO 3/8           | +   | +          | +  | +           | +      | +             | +             | +             | +            | 1   |
| 1/2 TO 3/4            |     | +          | +  | +           |        | +             | •             | +             | +            | 1   |
| 1 10 21/2             | !   |            | •  | •           |        | •             | •             | •             | 1            | 2   |
| 3 10 6                | l l | +          | 1  | 1           | 1      | +             | 1             | 1             | 4            | . 9 |
| 7 10 15               | +   |            | +  | 3           | 4      | 4             | 5             | 4             | 66           | 87  |
| 20 10 30              |     |            | 1  | 1           | į      | i i           |               |               |              |     |
| 35 OR MOSE            |     |            | 1  | 1           | l      | +             |               |               | +            | 4   |
| TOTAL                 | +   | 2          | 2  | 5           | 5      | 5             | 6             | 5             | 71           | 100 |

#### JRRENCES:

| J | · '                                     | 23 M           | PH.   | AND             | OVER                                 |   | 4  |
|---|---|----------------|---|-----------------|--------------------------------------|---|--|
|   | ¥ .                                     | ž              | **  | ma.             | ***                                  | 96-190%                                 | TOTAL OBS.   |
|   | + | ++++111113321+ | +1<br>11<br>12<br>11<br>22<br>11<br>22<br>23<br>32<br>11<br>+ | +13321112111+++ | 1<br>2<br>4<br>1<br>1<br>1<br>1<br>1 | 11<br>66<br>55<br>11<br>11<br>11<br>+++ | 208<br>536<br>750<br>1341<br>1411<br>1038<br>682<br>698<br>609<br>506<br>377<br>214<br>109<br>49 |

ivided by 10). sums exactly .5.

# PERCENTAGE FREQUENCIES B OF WIND DIRECTION AND SPEED:

| DIRECTION |     |     | HOUR   |       |         | ONS OF  |         | SPEED   |            |       | AV    |
|-----------|-----|-----|--------|-------|---------|---------|---------|---------|------------|-------|-------|
| partition | 0 1 | 4.7 | 8 - 12 | 13 17 | 19 - 24 | 23 - 21 | 32 - 36 | 29 - 44 | 47<br>CYES | POTAL | S-GED |
| N         | +   | 2   | 4      | 3     | 2       | +       | +       | +       |            | 11    | 12.3  |
| NNE       | +   | 1   | 2      | 1     |         |         | +       | +       | !          | 6     | 10.5  |
| NE        | +   | 3   | 4      | 1     | +       | +       | +       | 1       | ŀ          | 8     | 9.3   |
| ENE       | +   | 1   | 2      | 1     | +       | +       | +       | 1       | ł          | 4     | 9.6   |
| E         | +   | 2   | 3      | 1     | +       | +       |         | i :     | i          | 6     | 9.7   |
| ESE       | +   | 1   | 1      | 1     | +       | +       | +       | +       | 1          | 3     | 10.6  |
| SE .      | +   | 2   | 3      | 1     | i +     | +       |         | ļ.      | 1          | 7     | 10.0  |
| SSE       | +   | 2   | 3      | 1     | *       | 1 +     | ł       | l       | l          | 7     | 9.7   |
| S         | +   | 3   | 3      | 2     | 1       | +       | +       | +       | +          | 10    | 10.5  |
| SSW       | +   | 1   | 2      | 2 2   | 1       | +       | +       | l       | l          | 6     | 12.3  |
| SW        | +   | 2   | 2      | 1     | +       | +       | +       | 1 +     | 1          | 6     | 10.1  |
| WSW       | +   | 1   | 1      | +     | +       | +       | +       | 1       |            | 3     | 9.5   |
| w         | +   | 2   | 2      | 1     | +       | +       | ł       | i       | 1          | 5     | 8.9   |
| WNW       | +   | 1   | 1      | 1     | +       | +       | +       | 1       | l          | ] 3   | 10.2  |
| NW        | +   | 2   | 2      | 1     | 1       | +       | +       | +       | l          | 6     | 11.0  |
| NNW       | +   | 1   | 2      | 1     | 1       | +       | +       | i       | ١.         | 5     | 12.5  |
| CALM      | 5   | İ   | 1      | İ     | İ       | İ       | ĺ       | Ī       | İ          | 5     | 1     |
| TOTAL     | 7   | 28  | 38     | 20    | 6       | 1       | +       | +       | +          | 100   | 10.0  |

# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND E RELATIVE HUMIDITY:

|           |     | (U)<br>0 31 |          | W  | (M.  |           | 0                | 82       | ATT       | TE H      | JAUD      | NY (      | %)         |
|-----------|-----|-------------|----------|----|------|-----------|------------------|----------|-----------|-----------|-----------|-----------|------------|
| OF<br>DAY | 4 9 | 4-7         | 8-<br>10 | фĦ | 4-12 | 13-<br>24 | 25-<br>&<br>0722 | 0.<br>29 | 30-<br>49 | 50.<br>69 | 70.<br>79 | 80-<br>89 | 90-<br>100 |
| 00        | 54  | 12          | 34       | 11 | 73   | 15        | +                | +        | 3         | 12        | 11        | 22        | 52         |
| 01        | 53  | 13          | 35       | 11 | 73   | 15        | 1                |          | 2         | 11        | 11        | 20        | 55         |
| 02        | 51  | 23          |          | 12 | 72   | 15        | +                |          | 2         | 10        | 11        | 19        | 57         |
| 03        | 49  | 14          | 37       | 11 | 73   | 15        | 1                | 1        | 1         | 10        | 11        | 19        | 59         |
| 04        | 49  | 13          | 38       | 11 | 72   | 17        | +                | 1        | . 1       | 10        | 11        | 19        | 59         |
| 05        | 44  | 16          | 40       | 11 | 73   | 15        | 1                | 1        | 1         | 9         | 11        | 19        | 60         |
| 06        | 40  | 17          | 43       | 8  | 75   | 16        | 1                |          | 1         | 10        | 12        | 23        | 53         |
| 07        | 39  | 17          | 44       | 5  | 71   | 23        | +                | 1        | 2         | 15        | 18        | 31        | 33         |
| Ô8        | 37  | 19          | 44       |    | 63   | 22        | l                | +        | į 7       | 25        | 26        | 22        | 19         |
| 09        | 36  | 20          | 44       | 4  | 58   | 37        | 1                | 1        | 15        | 37        | 23        | 14        | 12         |
| 10        | 34  | 23          | 43       | 4  | 56   | 39        | 2                | 2        | 21        | 42        | 16        | 10        | 8          |
| 11        | 31  | 25          | 44       | 4  | 55   | 40        | 2                | 4        | 26        | 42        | 13        | 8         | 7          |
| 12        | 29  | 26          | 45       | 3  |      | 142       | 2                | 7        | 29        | 39        | 11        | 8         | 6          |
| 13        | 28  | 27          | 45       | 3  |      | 45        | 2                | 8        | 31        | 36        | 11        | 8         | 6          |
| 14        | 29  | 26          | 45       | 3  |      | 45        | 2                | 9        | 30        | 34        | 11        | 8         | 7          |
| 15        | 31  | 24          | 45       | 2  | 49   | 47        | 2                | 9        | 28        | 33        | 12        | 9         | 8          |
| 16        | 34  | 22          | 44       | 2  | 53   |           | ] 1              | 7        | 25        | 33        | 15        | 12        | 8          |
| 17        | 36  | 19          | 45       | 3  | 65   |           | 1                | 2        | 18        | 33        | 18        | 16        | 12         |
| 18        | 38  | 18          | 44       | 4  | 75   | 20        | +                | 1        | 11        | 28        | 22        | 22        | 16         |
| 19        | 42  | 17          | 41       | 7  | 77   | 16        | +                | +        | 6         | 20        | 21        | 28        | 25         |
| 20        | 45  | 17          | 38       | 9  | 75   | 15        | 1                | +        | 5         | 26        | 16        | 30        | 33         |
| 21        | 48  | 16          | 36       | 10 | 74   | 16        | +                |          |           | 14        | 14        | 29        | 39         |
| 22        | 51  | 15          | 34       | 12 | 73   | 15        | ÷                | ÷        | 3         | 13        | 13        | 27        | 44         |
| 23        | 53  | 14          | 34       | 12 | 71   | 14        | +                |          | 3         | 13        | 12        | 25        | 48         |
| AVG       | 41  | 18          | 41       | 7  | 66   | 26        | 1                | į 2      | 11        | 23        | 15        | 19        | 30         |

MOBILE Bates

ates

| _  |                                       |                 |   |                                  |     |  |  |   |                      |   |  |                                       |          |   | -  |  |  |   |                       |                       |   |                           | -                                       |         | ******  |
|--|---------------------------------------|-----------------|---|----------------------------------|-----|--|--|---|----------------------|---|--|---------------------------------------|----------|---|--|--|--|---|-----------------------|-----------------------|---|---------------------------|---|---------|---|
| нФ   |                                       |                 | 04 6  | HTA                              |     | - 1  |  |   | 514                  | u Pil   |  |                                       |          |   | 15 74  | MPH  |  |   |                       | 25 M                  | rii d   | AND I                     | WIR                                     |         | ,   |
| -  | ŧ,                                    | Ş               | \$  |                                  | •   | £ .  | g<br>SR  | 1   | ¥                    | K.  | Lange .  | *.23                                  | S X      | 5   | •  | £  | £  | ٠.×   | ķ                     | ,                     | Ę   | f                         | į                                       | \$ . E. | 10*4. 0   |
| 100<br>95<br>90<br>850<br>850<br>75<br>60<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>40<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>950<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80 | * * * * * * * * * * * * * * * * * * * | - 4654557675454 | 11<br>31<br>21<br>17<br>15<br>12<br>17<br>12<br>17<br>12<br>17<br>6 | 33<br>20<br>18<br>15<br>21<br>20 |     | 300<br>197<br>100<br>66<br>46<br>32<br>20<br>12<br>6 | +<br>1<br>1<br>2<br>4<br>8<br>7<br>6<br>4<br>2<br>1<br>1 | 47<br>57<br>60<br>43<br>43<br>43<br>45<br>57<br>45<br>39<br>29<br>15<br>7 | 98<br>94<br>87<br>61 | 134<br>98<br>75<br>70<br>64<br>61<br>45<br>25 | 305<br>186<br>131<br>117<br>52<br>68<br>45<br>27 | 302<br>238<br>252<br>185<br>109<br>78 | 25.43322 | 39<br>13<br>15<br>24<br>29<br>27<br>33<br>77<br>25<br>13<br>5<br>2+ | 13<br>63<br>719<br>50<br>36<br>45<br>45<br>45<br>18<br>7+1 | 70<br>46<br>317<br>15<br>19<br>18<br>15<br>11+ | +11<br>40<br>37<br>25<br>17<br>17<br>19<br>14<br>11<br>4 | +<br>18<br>34<br>32<br>22<br>21<br>11<br>7<br>2 | +<br>+<br>1<br>+<br>+ | + + 1 1 2 3 2 2 2 1 + | 1<br>2<br>3<br>2<br>2<br>3<br>3<br>4<br>5<br>5<br>3 | -<br>+252<br>1112<br>1221 | 1 |         | 12<br>229<br>620<br>979<br>1671<br>1189<br>987<br>850<br>692<br>621<br>449<br>282<br>128<br>47<br>9 |
| / 15   | 5                                     | 58              | 186   | 232                              | 613 | 917  | 36   | 507   | 1440                 | 911   | 1157   | 1227                                  | 21       | 235   | 529  | 232  | 198  | 170   | _2                    | 13                    | 33  | 18                        | 16                                      | 11      | 0767  |

In Tables A and C, occurrences are for the averago year (10-year total divided by 16). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

| OCCUPATION  | OF   | PRECIPITATION | ALCOURTE. |
|-------------|------|---------------|-----------|
| OCCURRENCES | ( )F | PRECIPITATION | AMOUNIS:  |

C

|                   |   |     |    |    |    | FREC | UEN | CY ( | OF C | ccu  | RREI | HCE. | FOR | EAC | н  |    |     |           |    |     |     |     |    |      |     |
|-------------------|---|-----|----|----|----|------|-----|------|------|------|------|------|-----|-----|----|----|-----|-----------|----|-----|-----|-----|----|------|-----|
| INTENSITIES       | A M HOUR ENDING AT PM HOUR ENDING AT OF |     |    |    |    |      |     |      |      |      |      |      |     |     |    |    |     |           |    |     |     |     |    |      |     |
|                   |   | 2   | 3  | •  | 5  |      | 7   |      |      |      | 11   | NCO4 | 1   | 2   |    | 4  | -5. | 6         | 7  | •   | •   | 10  | 11 | 19-0 |     |
| THACE             | 16                                      | 14  | 16 | 18 | 16 | 17   | 20  | 18   | 2.7  | 18   | 20   | 22   | 27  | 26  | 27 | 24 | 22  | 21        | 22 | 19  | 17  | 17  | 16 | 14   | 50  |
| O1 🖦              | 4                                       | إيد | 5  | 3  | 4  | 4    | 2   | 3    | 3    | 4    | 4    | 6    | 5   | 4   | 7  | 7  | 6,  | 6         | 5  | 4   | 4   | 격   | 4  | 4    | 11  |
| 02 to 00 m        | 6                                       | 5   | 6  | 6  | 6  | 6    | 6   | 7    | 8    | 9    | 10   | 11   | 12  | 12  | 13 | 13 | 11  | 10        | 9  | 9   | 8   | 7   | 7  | 5    | 20  |
| N 10 14 F         | 2                                       | 3   | 2  | 3  | 3  | 3    | 3   | 3    | . 3  | 4    | 3    | 4    | 5   | 6   | 5  | 5  | 퇫   | 4         | 3  | 4   | 2   | . 2 | 3  | 2    | 19  |
| 25 10 49 W        | 1                                       | 1   | 2  | 1  | 2  | 1    | 1   | 2    | 2    | 2    | 2    | 3    | 2   | 2   | .3 | 2  | 1   | 2         | Z  | 1   | 1   | 1   | +  | 1    | 18  |
| 50 to 99 m        | 4                                       | +   | 1  | 1  | +  | 1    | 1   | +    | 1    | 1    | 1    | 1    | 1   | 2   | 1  | 1  | 2   | 1         | 1  | 1   | +   | 1   | 1  | 1    | 18  |
| 100 TO 100 M      | 1 1                                     | +   | +  | 4  | •  | +    | +   |      |      | l li | +    | 4    | 1   | 1   | +  | +  | +   | 4         | 1  | 4   | - + | 4   | •  | *    | 12  |
| 2 00 to 446 CVI R | 1 1                                     |     | +  |    | l  |      |     | +    | +    |      |      | 1    |     |     | +  | •  | +   | - 1       | *  |     |     | 1   | 1  | 1    | 5   |
| TOTAL             | 29                                      | 28  | 31 | 31 | 32 | 31   | 33  | 32   | 33   | 37   | 41   | 48   | 52  | 52  | 55 | 51 | 47  | <u>45</u> | 41 | _37 | _33 | 30  | 31 | _29  | 160 |

PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|                     |          |             |     |     | CERUN        | ट (१६६१       | )             |               |              |     |
|---------------------|----------|-------------|-----|-----|--------------|---------------|---------------|---------------|--------------|-----|
| VIS:BRITY<br>(MXES) | ۰        | 166-<br>328 | *   | 12  | 1936<br>1930 | 3638-<br>7400 | 2014-<br>1780 | 2080-<br>1188 | Ov18<br>1980 | 101 |
| 0 TO 1/8            | •        | •           | +   | +   | •            | +             | +             | +             | +            |     |
| 3/16 TO 3/8         |          |             | +   |     |              |               | +             | •             |              | 1   |
| 1/2 10 3/4          |          |             |     | •   |              | •             | +             |               | +            |     |
| 1 10 21/2           |          | +           | 1   | +   | +            | +             | +             | +             | 1            |     |
| 3 TO 6              | <b>i</b> |             |     |     | 1            | <u> </u>      |               |               | فسا          |     |
| 7 10 15             |          | +           | +   | 2   | 4            | 3             | 3             | 4             | 72           | 8   |
| 20 10 30            | 1        |             |     | i - |              |               |               | Ì             |              |     |
| 35 OR MCRE          |          |             |     |     | l i          | 1             |               |               |              |     |
| TOTAL               |          | 3           | . 1 | - 3 | 5            | . 3           | 4             | 5             | _77          | _10 |

NEW ORLEANS, LA. Moisant Int. Airport

## DITY OCCURRENCES:

| wrll  | <br>  |  | -              | 27 M                                     | rn /                      | uw) (                     | wi#        |                     | 2  |
|---|---|--|----------------|--|---------------------------|---------------------------|------------|---------------------|--|
| £   | £   | e.x.                                       | ş <sup>n</sup> | Š  | Ę                         | Ł                         | 2          |                     | 10°A. 045  |
| 7<br>40<br>46<br>33<br>17<br>15<br>19<br>18<br>15<br>15 | 11<br>40<br>37<br>25<br>17<br>17<br>19<br>14<br>11<br>4 | 18<br>34<br>32<br>22<br>21<br>11<br>7<br>2 | * 1            | + + 1<br>1<br>2<br>3<br>2<br>2<br>1<br>+ | 1 2 3 2 2 2 3 3 4 5 5 3 1 | -<br>+2521<br>112221<br>+ | +441112111 | 1 2 2 1 1 1 1 1 + + | 12<br>229<br>620<br>979<br>1671<br>1189<br>987<br>850<br>692<br>449<br>282<br>128<br>47<br>9 |
| 232   | 198   | 170  | 2              | 13                                       | 33                        | 18                        | 16         | 11                  | 0767   |

'ear total divided by 10). make their sums exactly less than 0.5.

# **MOUNTS:**

| -  |                |       |       |      |       |      | -    |     |      |
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| :  |                | XIE I | ENDIN | G AT |       |      |      | ᅥ   | **   |
| Ť  | <del>, 1</del> | •     | 7     | • 1  | •     | 13 1 | 11 [ | -   | BA15 |
| į, | 22             | 21    | 22    | 19   | 17    | 17,  | 16   | 14  | 50   |
| 7  | 6              | 6     | 5     | 4    | 4     | 2    | 4    | 4   | 11   |
| 3  | 11             | 19    | 9     | 9    | 8     | 7    | 7    | 8   | 26   |
| 5  | 5              | إد    | 3     | 4    | 격     | . 2  | 7    | 2   | 19   |
| 2  | 1              | 궏     | Z     | 1    | ı,    | 4    | **   | 1:  | 18   |
| 1  | 1              | 1     | 1     | 1    | *     | 4    | 4    | 1,  | 10   |
| .1 | *              | • •   | !     | ٦    | ٦     | 7    | ٦    | ٦   | -4   |
| ?  | . ]            |       | ( T   | 37   | 32    | 24   | 21   | 29  | ٦.,  |
| 7  | -1             | 7     |       | -24  | _2.21 | 4    | - 11 | 5.7 | - PU |

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| ** | Over<br>rese | IOI   |
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| ڹ  |              |       |
| •  | 72           | **    |
| _5 | 77           | 100   |

NEW ORLEANS, LA. Moisant Int. Airport

B-10

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

B

E

| •             |       | •          | F 4 167 C | 44.4K      | AIR SE     | . 16 W     | *** '21    | et.        |                 |
|---------------|-------|------------|-----------|------------|------------|------------|------------|------------|-----------------|
| (-00)- b-s pa | • .   | . ,        | • 11      |            |            |            | • "        | ٠.         | er<br>me i kasa |
| 'n            | 1     | 1:         | 2 .       | 2 :        | 1 '        | • :        | • '        | • '        |                 |
| NNE           | , + i | 1;         | 2 .       | 2 .        | 1          | • j        | ٠,         | •          | 6 :             |
| 'NE           | •     | 2 1        | 3         | 2          | + 1        | ٠.         | • ;        | ٠.         |                 |
| CHF.          | +!    | 2 .        | 3         | 2 1        | ٠.         | <b>*</b> . | ٠.         | •          | • B             |
| Ė             | ' + ! | 2          | 2         | 1          | •          | • :        | 4 ,        |            | . 6             |
| FSF           |       | 2 .<br>2 : | 1         | 1          | •          | ٠.         |            |            | 4               |
| SE            |       | 2 .        | 2         | 1          | <b>+</b> ' | •          |            |            | : 5             |
| SSE           |       | 3          | 3         | 2          | ٠          | + ;        | ٠          | +          | 8;              |
| `S            | ! • ] | 3          | 3         | 2          | •          | •          | + *        |            | 9.              |
| '5 SW         |       | 2 '        | 3 .       | 1          | + ·        | •          | ٠.         |            | 7               |
| 'SW           | 1 +   | 2          | 1         | 1          | + +        | • [        | i          |            | 4               |
| WSW           | . •   | 1 :        | 1:        | <b>+</b> ' | <b>+</b> 1 | <b>+</b> : | ٠.         | •          | 2 ′             |
| :W            | . •   | 1 1        | 1.        | ٠.         | •          | <b>*</b> • | •          | . !        | 3               |
| WNW           | +     | 1          | 1 .       | 1          | + ;        | <b>+</b> ! | <b>+</b> . | * ·        | 3 :             |
| INW           | +     | 1          | 1 ;       | 1.         | *          | •          | + !        | <b>*</b> : |                 |
| INNW          | +     | 1          | 2:        | 2          | 1 !        | • •        | •          | •          | ! 6             |
| CALH          | 12    | i          |           |            | - !        | 1          | i          |            | 12              |
| TOTAL         | 16    | 27         | 32        | 19         | 5          | 1 ,        | + 1        | ٠,         | + (100 )        |

# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                   |          | LE O |          | w   | IND<br>(M. F |           | D                  | RE         | ATIV      | E H              | IMIO      | ITY (    | %)<br>       |
|-------------------|----------|------|----------|-----|--------------|-----------|--------------------|------------|-----------|------------------|-----------|----------|--------------|
| HOUR<br>CF<br>DAY | ٠<br>3   | 47   | 8-<br>10 | 0.3 | 4-<br>12     | 12.<br>24 | 25-<br>E<br>::>V(R | 29         | 20-<br>49 | 50-<br><b>69</b> | 70-<br>79 | 50-      |              |
| 00<br>01          | 55<br>55 | 13   | 32<br>32 |     | 60<br>56     | 15        | 1                  |            | 2 2       | 10               | 11        | 33<br>31 | <br>44<br>50 |
| 02                | 53       | 12   | 34       | 31  |              | 14        | 1                  |            | 2         | ; 3              |           | 27       | 54           |
| 03                | 52       | 13   | 35       |     | 52           | 14        | 1                  | i          |           | •                | ۱ ۾       | 25       | 57           |
| 04                | 51       | 13   |          | 34  | 51           | 14        | 1                  | 1          | 1         | ; 8              |           | .23      | 60           |
| 05                |          | 15   | 38       | 34  | 51           | 14        | 1                  | i          | , 1       |                  | 8         | 23       | 60           |
| 90                | 43       | 17   | 41       | 30  | 54           | 15        |                    | :          | 1         | 111              | 1         | 125      | 57           |
| 07<br>08          | 40       | 17   | 41       | 18  | 63           | 118       | 1 1                | į          |           | 20               |           | 127      | 34<br>20     |
| 09                | 38       | 21   | 41       |     | 59           | 26        |                    | ! _        | 7         | 36               |           | 117      | 12           |
| 10                | 37       | 23   | 140      | 1 3 | 57           | 39        |                    | ; <b>†</b> | 'ii       | 48               | 21        |          | •            |
| īī                | 37       | 23   | 40       |     | 1            | 141       | 1 2                | i          | 116       |                  | .15       | . 9      | 7            |
| 12                | • • •    | 22   | 40       | ! 2 |              | .43       | ·2                 | ! ī        |           | :51              | 13        |          | é            |
| 13                | 36       | ,    | 41       | 2   |              | 43        |                    | ž          |           | .47              | .12       | . 9      | . 3          |
| 14                | 36       | 21   | 42       | 3   | 155          | 141       | 1 2                | ! 3        | 27        | 143              | 12        | . 9      | 4            |
| 15                | 36       | 21   | 44       | 12  |              | 137       | 1                  | 4          | 127       | 43               | .15       | 19       | . (          |
| 16                | 36       | 19   | 45       | 4   | 62           | 33        | ; 1                | į 3        | 25        | 40               | 115       | 10       | ; 7          |
| 17                | 36       | 19   | 45       |     | 66           | 25        | 1                  | 1 1        | 19        | 38               | 121       | 14       | : 1          |
| 18                |          | 118  | 44       |     | 68           | ;18       | 1 7                | i 1        | 112       |                  | -25       |          | ٠٩           |
| 19                |          | 18   |          |     | 68           |           |                    | . +        | ! 5       | :25              |           |          |              |
| 20                | •        | 17   | 35       | 19  |              | 115       |                    | : <b>+</b> | 1 -       |                  |           |          | 20           |
| 21                | 51       | 15   | 35       | 20  |              |           |                    | +          |           | 112              | 19        |          | 20           |
| 22                |          | 115  |          | 20  |              |           |                    |            | ! 3       | 11               | :16       |          | .3           |
| 23                | 124      | 14   |          | 22  |              |           | • -                | 1:         | 3         |                  |           |          | 37           |
| AVG               | 1-0      | 17   | 38       | 16  | 59           | 24        | 1                  | 1 2        | 9         | 25               | ុរ6       | .23      | 27           |

| 440  |   |   | 0-4 #                               | aph.          |                                 |  |                                   |   | 5 14 /   | MPH  |   |  |                          |                    | 15-24  | MPH  |   |  |   | 25 M        | PH .                                | AND                            | OVER                        |   | 14   |
|--|---|---|-------------------------------------|---------------|---------------------------------|--|-----------------------------------|---|--|--|---|--|--------------------------|--------------------|--|--|---|--|---|-------------|-------------------------------------|--------------------------------|-----------------------------|---|--|
| * * *  | ŝ,  | Ş   | £                                   | A IN          | nen.                            | <b>U</b>                               | 1.45A                             | N. Co.  | Ş  | 46.0   | wa  | 101 0                                  | and)                     | Keth               | 300  | J. 16. 17.   | 10.89%  | 90 LODY                                      | p.016                                   | ¥           | , F                                 | ****                           | 8.40.                       | * | TOTAL OKS  |
| /100<br>/ 95<br>/ 95<br>/ 80<br>/ 75<br>/ 60<br>/ 55<br>/ 45 | +<br>+<br>1<br>1<br>2<br>2<br>2<br>2<br>1 | 7<br>15<br>10<br>4<br>5<br>6<br>6<br>7<br>5<br>2<br>2 | 15<br>30<br>17<br>10<br>8<br>6<br>7 | 25            | 35<br>87<br>27<br>16<br>10<br>8 | 7<br>145<br>79<br>49<br>41<br>26<br>17 | 116<br>16<br>16<br>13<br>16<br>13 | 1<br>36<br>74<br>54<br>34<br>39<br>44<br>48<br>55<br>43<br>18 | 3<br>106<br>253<br>135<br>67<br>64<br>67<br>68<br>70<br>84<br>78 | 55<br>186<br>101<br>69<br>55<br>52<br>48<br>46 | 196<br>362<br>149<br>120<br>102<br>88<br>71<br>58 | 400<br>313<br>294<br>218<br>166<br>107 | 10<br>12<br>10<br>7<br>4 | 36                 | 197<br>117<br>99<br>64<br>49<br>40<br>47<br>45 | 23<br>71<br>70<br>55<br>29<br>22<br>19<br>22<br>26<br>18 | 1<br>25<br>70<br>89<br>55<br>30<br>29<br>23<br>21 | 2<br>34<br>96<br>100<br>43<br>34<br>31<br>16 | 2 | +1123546437 | 29<br>15<br>14<br>13<br>4<br>5<br>5 | 39<br>14<br>8<br>31<br>22<br>1 | 2<br>12<br>9<br>4<br>1<br>1 |   | 56<br>327<br>677<br>949<br>112<br>980<br>772<br>681<br>570<br>452<br>291 |
| / 35<br>/ 30<br>/ 25<br>/ 20<br>/ 15<br>/ AL                 | •   |   | 117                                 | . 1<br>1<br>1 | 2<br>1<br>+                     | 3 1 +                                  |                                   | 6<br>2<br>+   | 22<br>12<br>1<br>1   | 17<br>8<br>3<br>+                              |   | 15<br>6<br>3                           | ٠                        | 6<br>4<br>1<br>343 | 11<br>6<br>2<br>1                              | 8<br>2<br>1<br>+   | 7<br>4<br>1<br>+                                  | 15<br>6<br>1<br>+                            |   | 1           | 1 +                                 | *                              | •                           | + | 141<br>64<br>18  |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

|              | ~=    |               | * 1 / O T T T T T T |
|--------------|-------|---------------|---------------------|
| CKTHINKENCES | 6 130 | PRECIPITATION | AMOUNTS             |

|                 | T   |     |    | •   |     | REC | UEN   | CY ( | XF C | xccu | RRE | NCE | FOR | EAC | нн  | วบก | OF  | THE | DAY  |      | *** | • •• |               |         |
|-----------------|-----|-----|----|-----|-----|-----|-------|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|------|---------------|---------|
| INTENSITIES     |     |     |    | 7   | M H | NUC | 11043 | G A  | _    |      |     |     |     |     |     |     | M H | OUR | ENDI | KS A | · · |      |               | 4 80    |
|                 |     |     |    | 4   | •   | •   |       | -    | •    | .0   | *** | NO. | •   | 7   | 3   | 4   | •   |     | 77   | 7    | -T  | 10.  |               | DATE    |
| IMACE           | 14  | 15  | 15 | 15  | 17  | 15  | 119   | 23   | 20   | 18   | 21  | 25  | 27  | 25  | 23  | 19  | 19  | 16  | 15   | 14   | 15  | 15   | 13 1          | 4 53    |
| C4 W            | 4   | 5   | 4  | - 5 | 5   | 5   | 3     | 4    | -4   | 4    | -5  | 5   | 5   | 6   | 6   | 7   | 6   | 8   | 4    | 4    | 3,  | 3    | 4             | 4 10    |
| 67 10 00 m      | 1 5 | 5   | 6  | 6   | 7   | 7   | 7     | 7    | 9    | 9    |     | 9   | 11  | 11  | 11! | 10  | 10  | 9   | 7!   | 61   | 6,  | 51   | 6.            | ر<br>ام |
| NO 10 24 M      | 2   | 2   | 3  | 3   | 3   | -2  | 2     | 3    | 3    | 3    | 4   | 3   | 4   | 4   | 4   | أيه | 4   | 2.  | Ž    | 3    | 3   | 2,   | 21            | 2: 19   |
| 25 10 47 6      | ! + | 1   | 1  | 1   | 1   | 1   | 2     | 2    | 1    | 1    | 1   | 1   | 2   | 1   | 2   | 2   | 1   | #   | 1:   | 1    | +   | 11   | 1             | 1 15    |
| to to the in-   | +   | +   | +  | +   | 1   | 1   | 1     | 1    | 1    | +    | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 1   | 4    | أب   | +   | +;   | - <del></del> | + 13    |
| 1 00 1U 119 A   | 1 1 |     | +  | •   | +   | - 1 | +     |      | . +  | . +  |     |     | +   | +   | +   | 1   | +   | +   | 1    | !    |     | 1    | i             | 1 1     |
| 8310 DIA N 00 S | ! ! | 1   |    |     | 1 1 | 1   | 1     |      |      |      |     |     | +   | - 1 | ļ   | _   | 1   | +   | ٦    | į    |     | 1    | +Í            | 4       |
| TOTAL           | 26  | _28 | 29 | 31  | 33  | 31  | 34    | 39   | 37   | 36   | 39  | 44  | 50  | 48  | 46  | 44  | 41  | 35  | 29   | 27   | 27  | 25   | 261 2         | 7151    |

#### City Office Data

C

Table C data obtained from tipping bucket rain gage located at the Federal Bldg., Franklin and Fannin Streets(Houston City Office), at an elevation of 152 feet.

| • | PERCENTAGE FREQUENCIES | OF |
|---|------------------------|----|
| D | CEILING-VISIBILITY:    |    |

| ٦. |             |   |             |   |            | CERLIN       | C (HE          | -   |              | <del></del>  |          |
|----|-------------|---|-------------|---|------------|--------------|----------------|-----|--------------|--------------|----------|
|    | (MILES)     | ٥ | 146-<br>736 | * | 164<br>161 | 1980<br>1980 | 35.00-<br>3760 | *** | 1080<br>7363 | 0452<br>2389 | 101      |
| ŀ  | 0 10 1/8    | + | +           | + | +          | •            | +              | +   | +            | +            | <u>1</u> |
| l  | 3/16 TO 3/8 |   | •           | • | +          | +            | +              | +   | +            | +            | 1        |
| ł  | 17 10 3/4   |   | +           |   | +          | +            | *              | +   | +            | +            | 1        |
| ١  | 1 10 21/2   | 1 | +           | 1 | 1          |              | +              | +   | +            | 1            |          |
| l  | 3 10 4      | 1 |             | 1 | 2          | 1            | 1              | 1   | 1            | 5            | 10       |
| Г  | 7 10 15     |   |             | + | 2          | 5            | 5              | 7   | 5            | 59           | 84       |
| ı  | 20 10 38    |   |             |   | ŀ          |              |                |     | ! !          |              |          |
| ı  | 35 OR HORE  |   |             |   |            | •            |                | +   |              | i            | . 4      |
| ł  | TOTAL       | ه | 1           | 2 | 5          | 6            | - 6            |     | - 6          | 66           | 10       |

## ES:

| MID                 | OVER        |                       | 4                       |
|---------------------|-------------|-----------------------|-------------------------|
| £,                  | S. P.       |                       | 1CTAL OBS               |
| +20054343435121++ 7 | 22941111244 | 4 8 4 2 2 3 3 1 1 + + | 36<br>327<br>677<br>949 |

y 10). etly

# 13 14 53 4 4 10 6 6 29 21 2 19 1 1 15 + + 13 + + 13 26 27151

K.,

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

| В         | C  |     |   | VII |   |     | IRE   |                     | N A     |       | SPE |           | :         |
|-----------|----|-----|---|-----|---|-----|-------|---------------------|---------|-------|-----|-----------|-----------|
| Delicient | i  |     |   |     | H | OUN |       | NATICE<br>TO FILM 1 | 45 OF W | W GHN | לנט |           | :<br>, 4+ |
| 4         | ٠. | ,   |   | . , | • | ,   | 11 10 | IV 24 .             | rs 11 H |       |     | er<br>CMB | K-141     |
| 'n        | ;  | +   | : | 1   | • | 2 . | 2     | 1:                  | •       | • '   | •   | •         | 5 12.4    |
| HNE       | í  | ٠   | i | 1   | • | 2   | 2     | •                   | e ·     | ٠     |     | •         | 5 12.0    |
| HE '      | 1  | •   | : | 1   |   | 2   | 2     | • ′                 | • '     | •     | ٠,  | •         | 6 11 • 2  |
| ENE       | •  | •   | : | 1   |   | 3 : | 2:    | ٠,                  | ٠,      | •     | :   |           | 7 11.0    |
| Ε         | :  | •   | • | 1   | : | 2   | 1     | <b>*</b> :          | • [     | + ;   | :   | 1         | 6 10 - 2  |
| ,ESE      |    | +   | : | 2   |   | 3 ! | 2     | 1:                  | • i     | ٠,    |     | - 1       | 8 10.8    |
| 'SE       | •  | ٠   | 1 | 1   |   | 4   | 3     | 1                   | • i     | ٠.    | • ' |           | 10 12.8   |
| SSE       |    | •   | 1 | 2   |   | 4.  | . 5   | 2,                  | 1 .     | ٠.    | • : | - 7       | :4 (13.8  |
| ,5        |    | +   | ŀ | 1   |   | 3   | 3 -   | 1                   | •       | •     | •   |           | 9;12.6    |
| SSW       |    | +   | • | 1   |   | 2   | Z     | 1.                  | •       | +     |     | 1         | 6 11-7    |
| !SW       |    | +   |   | 1   |   | Ζ,  | . 1   | ٠.                  | •       | •     |     |           | 4, 4.8    |
| WSW.      |    | +   | • | 1   |   | 1   | 1     | *                   | •       | •     | ٠.  |           | 3,9.8     |
| W         |    | ٠   |   | 1   |   | 1   | •     | •                   | •       | •     |     |           | 2 9.3     |
| .WNW      |    | ٠   |   | 1   |   | 1   | 1     | ٠,                  | •       | *     | • 1 | •         | 4 11.2    |
| ·HW       |    | +   | ٠ | 1   |   | 1   | 1     | •                   | •       | *     | •   | • :       | 4 12.4    |
| NNN       | ŀ  | +   | ï | 1   |   | 2   | 7     | 1                   | ٠,      | •     | •:  | •         | 6 13.5    |
| CALH      | i  | 1   | ; |     | : |     |       |                     | _       |       |     |           |           |
| TOTAL     | 1. | . 6 | : | 18  | ĩ | 36  | 78    | 10                  | 2 :     | • •   | ͺͺ  | •         | 100 111-2 |

# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

E

|                   |     | TE O  |           | . W | THO<br>(M. |           | 0                | RE       | LATIN     | /E H      | UMIO      | 17   | (%)        |
|-------------------|-----|-------|-----------|-----|------------|-----------|------------------|----------|-----------|-----------|-----------|------|------------|
| HOUR<br>OF<br>DAY | o a | 4-7   | \$.<br>10 | Ç.  | 4.<br>12   | 13-<br>24 | 25-<br>E<br>GVER | 0-<br>29 | 30-<br>49 | 50-<br>40 | 70-<br>70 | 50-  | 9G-<br>100 |
|                   | -   | '     |           |     |            |           | İ                |          | <u> </u>  |           | !         | •    | •          |
| 00                | 51  | 13    | 35        | 7   | 66         | 26        | 1                | +        | i 🔸       | 11        | .10       | · 32 | 43         |
| 02                | 51  | 13    | 36        | 9   | 66         | 25        | i i              | . +      | 3         | 10        | i 9       | :29  | 44         |
| 02                | 50  |       | 37        | 9   | 66         | 23        | 1.               | . +      | , 3       | : 9       |           | `25  | 54         |
| 03                | 48  | 14    | 38        | 10  | 65         | :24       | , 1              | . +      | ' 3       | 9         |           | ,23  | 58         |
| 04                | 48  | 13    | 39        | 11  | 65         | 23        |                  | •        | , 2       | . 8       | 8         | 22   | 60         |
| 05                | 44  | 16    | 40        | 10  |            | 123       | ` •              | !        | 2         | . B       | . 8       | 21   | 62         |
| 06                | 41  | 14    | 45        | 10  | 165        |           | ; 1              | . +      | ت ن       | 8         | : 8       | .55  | 61         |
| 07                | 39  | 1.    | 47        | 7   |            | 26        |                  | : 🕈      | . 2       | 9         | 14        | .33  | 42         |
| 08                | 33  | 1 = : | 48        |     | 54         |           | 2                | : :      | : •       | 16        | 27        | 28   | -26        |
| 09<br>10          |     | 24    | 49        | 6   |            | 46        |                  | 1        | 13        | 33<br>46  | 24<br>19  | 18   | 15         |
| 11                |     | 25    | 48        |     |            | 46        |                  |          | .19       | -         | 12        |      | 9<br>7     |
| 12                |     |       | 50        |     |            | 50        |                  | 3        | 24        | 50<br>47  | 11        | 9    | 6          |
| 13                | 24  |       | 50        |     | 39         | 51        |                  |          | 29        | 41        | ii        | 7    |            |
| 14                | 24  | 27    | : 49      |     |            | 54        | •                | 7        | . 30      | 40        | 10        | 7    | 6          |
| 15                | 27  |       | 49        | ! 3 |            |           | 6                |          | 28        | 40        | 11        | ż    | 5          |
| 16                | 31  | žź    |           | įŽ  |            | 58        |                  | ; ž      | 125       | 41        | 12        | ė    | 6          |
| 17                | 36  |       |           | Ž   | 37         | 57        | . 3              | 5        | · 21      | 40        | 17        | 11   | 7          |
| 18                | 40  | 16    | 44        | 2   | 42         |           | 2                |          | .15       | 37        | . 20      | :16  | 9          |
| 19                |     | 17    | 41        | 3   | 51         | 145       | lī               | , -      | 9         | 25        | 24        | 25   | 15         |
| 20                | 47  |       | 38        |     |            |           | lī               | ī        | . i       | 17        | 122       | 31   | 22         |
| 21                | 49  |       | 36        |     | 65         | 130       | Ĭ                | +        | 16        | 14        | . 16      | 36   | 28         |
| 22                |     | 14    | 35        | 5   | 66         | 28        | , 1              |          | 5         | 12        | 13        | 36   | 34         |
| 23                | 93  |       | 34        | 6   | • 66       | 27        | <u> </u>         | +        | . 5       | :11       | 11        | 35   | 39         |
| AVG               | 39  | 18    | 43        | 6   | 193        | 18        | 3                | 2        | 11        | 24        | 14        | 21   | 28         |

HOUSTON, TEXAS Int. Airport

| MNO  |           |       | 0-4 A                  | UH.  |   |                                  |       |   | 5-14 /   | APH   |  |   |             |   | 15-24                                       | МРН   |  |   |               | 25 M   | PH .   | AND (                      | OVER           |           | ,   |
|--|-----------|-------|------------------------|------|---|----------------------------------|-------|---|--|---|--|---|-------------|---|---|---|--|---|---------------|--|--|----------------------------|----------------|-----------|---|
| ## ?<br>## ?   | <b>!.</b> | Ş     | Ę                      | 2    | 5   | *                                | SE SE | *   | No.  | E &   | •  | -   | 5 A         | ž.  | Her   | Bare  | <b>§</b>   |   | 26 R          | Ę  | Š  | ř.                         | ٤              | # 195     | TOTAL OILS  |
| 9/ 95<br>%/ 90<br>9/ 85<br>%/ 89<br>9/ 70<br>9/ 65<br>4/ 60<br>9/ 95<br>6/ 50<br>9/ 45<br>4/ 40<br>9/ 35<br>4/ 30<br>9/ 25<br>4/ 20<br>9/ 15 | *         | 22222 | 18 14 6 6 10 8 1 9 3 1 | 7264 | 23<br>14<br>11<br>11<br>11<br>11<br>11<br>+ | 11<br>20<br>23<br>30<br>10<br>10 |       | + 3<br>11<br>12<br>12<br>13<br>13<br>13<br>13<br>13<br>14<br>15<br>12<br>12<br>13 | 144<br>395<br>196<br>125<br>85<br>86<br>85<br>93<br>95<br>59<br>26<br>12 | 2<br>239<br>379<br>194<br>165<br>66<br>62<br>54<br>37<br>17<br>17 | 27<br>643<br>236<br>217<br>153<br>163<br>25<br>63<br>25<br>16<br>3 | 1<br>69<br>120<br>220<br>318<br>198<br>125<br>29<br>15<br>4 | +115051111+ | + 2<br>3<br>9<br>15<br>26<br>27<br>27<br>24<br>16<br>10<br>4<br>2 + | 54<br>62<br>69<br>70<br>47<br>22<br>11<br>6 | 121<br>151<br>63<br>52<br>45<br>33<br>36<br>26<br>18<br>7<br>21 | 145<br>130<br>88<br>77<br>57<br>45<br>37<br>21<br>14<br>4+<br>4+ | 16<br>47<br>83<br>98<br>45<br>31<br>15<br>16<br>4 | + 1 + 1 1 + + | 1<br>1<br>4<br>4<br>8<br>8<br>8<br>8<br>5<br>3<br>1<br>1 | 1<br>2<br>3<br>5<br>7<br>15<br>12<br>13<br>8 | 8<br>4<br>2<br>1<br>+<br>+ | 55354676341 ++ | 444775551 | 62<br>849<br>1763<br>1144<br>1006<br>1007<br>717<br>7557<br>336<br>178<br>77<br>27<br>6 |
| DTAL   | +         | 19    | 94                     | 125  | 153   | 123                              | 7     | 204   | 1213   | 1430  | 1474   | 1213  | 13          | 164   | 594   | 601   | 643  | 443   | 5             | 44   | 71   | 42                         | 40             | 46        | 3767  |

In "ables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole number, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

## C

#### • OCCURRENCES OF PRECIPITATION AMOUNTS:

|                |    |    |    |    | (   | FREC | IUEN | CY (  | XF C | ccu | RRE | NCE | FOR | EAC | H H | อบล | OF  | TKE | DAY | ,    |    |    |    |             |            |
|----------------|----|----|----|----|-----|------|------|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|----|----|----|-------------|------------|
| INTENSITIES    | 1  |    |    |    | M H | OUR  | ENDI | NG AT | ,    |     |     | _   |     | _   |     | •   | M H | OUR | END | NG A | T  |    |    |             | 8          |
|                | 1  | 2  | 3  | 4  | 9   | 6    | 7    | •     | •    | 10  |     | *** | •   | 7   | 3   | •   | 3   | •   | 7   | •    | •  | 10 | ** | <b>#6</b> 0 | SHIR       |
| TRACE          | 10 | 11 | 10 | 12 | 12  | 16   | 17   | 19    | 25   | 22  | 22  | 21  | 18  | 17  | 15  | 18  | 16  | 16  | 16  | 14   | 15 | 13 | 12 | 11          | 41         |
| Ø #4           | 4  | 3  | 3  | 4  | 4   | 4    |      | 4     | 4    | . 5 | 4   | 3   | 4   | 4   | 4   | 4   | 4   | 3   | 3   | 4    | 3  | 4  | 4  | 4           | 9          |
| 82 TO 19 W     | 5  | Ā  | 5  | 6  |     | 7    | 9    | 10    | 6    |     | 9   | 8   | - 4 | 7   | 6   | 7   | 6   | 5   | 5   | 4    | 4  | 4  | 6  | *           | 24         |
| 10 10 24 M     | 2  | 2  | 9  | 3  | 3   | 3    | 2    | 4     | 3    | 3   | 3   | 3   | 3   | 2   | 3   | 2   | 2   | 1   | 1   | 2    | 2  | 2  | 1  | 2           | 18         |
| 25 TO /8 SE    | 1  | 1  | 1  | 1  | 1   | 1    | 2    | 3     | 1    | 2   | 3   | 1   | 1   | 1   | 1   | ı   | 1   | 1   | 1   | 1    | 1  | 4  |    | 1           | 15         |
| 20 to 10 m     |    | 4  | 1  | +  | +   | 1    | •    | 1     | 1    | 1   | +   | 1   | +   | +   |     | 1   | +   | •   | . + | •    |    | 1  | +  | •           | 13         |
| 100 10 1 m m   |    |    |    | l  |     |      | +    | 1     | +    |     |     |     | +   | +   | +   |     | •   | •   |     |      | l  | +  | +  |             | 7          |
| 100 M W B 00CB | i  |    |    |    |     |      | ł    | 1     | l    |     | l   |     |     | ŀ   | l   |     |     |     |     | 1    | 1  |    |    | l           | 2          |
| TOTAL          | 22 | 22 | 23 | 26 | 29  | 32   | 35   | 39    | 43   | 41  | 38  | 37  | 33  | 32  | 29  | 31  | 31  | 27  | 26  | 24   | 24 | 24 | 23 | 21          | <b>B28</b> |

\*City Office

PERCENTAGE FREQUENCIES OF CEILING—VISIBILITY:

|                     |     |     |            |            | CEILS | 3 (1)(1)      | 1   |               |              |      |
|---------------------|-----|-----|------------|------------|-------|---------------|-----|---------------|--------------|------|
| VISIONITY<br>UNKEST | ۰   | **  | 120<br>431 | 22.<br>100 | 1608  | 2233-<br>5788 | **  | 2500-<br>1750 | CV93<br>F860 | 101  |
| 6 TO 1/8            | •2  | دَه | +          |            | +     | 4             | +   | •             | •2           | •7   |
| 3/14 TO 3/8         | •1  | •3  |            | 4          |       | +             | +   |               | • 2          | •8   |
| 1/2 10 3/4          | •   | •Z  | -2         |            | -1    | •             | •   |               | •2           | •7   |
| 1 10 21/2           | . + | •\$ | • 5        | - 2        | •2    | • 1           | 01  | . 1           | •3           | 1.7  |
| 3 10 4              |     | • 2 | •          | 1.2        |       | . 9           |     |               | 2.7          |      |
| 71015               |     | • 1 | • 4        | 2.6        | 5.3   | 3.4           | 3.1 | 4.6           | 38.G         | 38.8 |
| 20 70 20            |     |     |            |            |       |               | l I |               | 1 1          |      |
| 35 OR MORE          |     |     |            | Į į        |       |               |     |               | •            | +    |
| TOTAL               | • 5 | 2.5 | 1.5        | 4.5        | 6.6   | 4.1           | 4.4 | 5.2           | 72.5         | 100  |

GALVESTON, TEXAS Municipal Airport

# DITY OCCURRENCES:

| MPH  |  |   |                             | 25 M   | PH .   | AND                           | OVER   |                         | 4   |
|--|--|---|-----------------------------|--|--|-------------------------------|--|-------------------------|---|
| <b>8</b> .8  | £  | -   | 200                         | ×  | <b>W</b>   | 20.00                         | £ =  | **                      | TOTAL OSS   |
| 1<br>121<br>151<br>63<br>52<br>44<br>45<br>33<br>36<br>26<br>18<br>7<br>21 | 15<br>148<br>130<br>88<br>77<br>57<br>45<br>37<br>21<br>14<br>++ | 40<br>473<br>83<br>845<br>315<br>122<br>64<br>1 | + 1<br>+ 1<br>+ 1<br>1<br>1 | 1<br>1<br>4<br>4<br>8<br>8<br>5<br>3<br>1<br>1 | 1<br>1<br>2<br>3<br>5<br>7<br>15<br>12<br>13<br>8<br>4 | 22 22 23 34 47 78 84 22 11 ++ | 55<br>55<br>35<br>44<br>67<br>77<br>66<br>33<br>44<br>11 | 4 4 4 7 7 7 5 5 5 5 5 1 | 1 62<br>849<br>1763<br>1144<br>1006<br>1042<br>1000<br>717<br>557<br>336<br>178<br>77<br>27<br>62 |
| 601  | 643  | 443   | 5                           | 44   | 71   | 42                            |  | 46                      | 3757  |

10-year total divided by 10). djusted to make their sums a than 0 but less than 0.5.

## **AOUNTS:**

| R  | R OF THE DAY                                     |    |    |    |    |    |    |    |     |  |  |  |  |  |  |
|----|--|----|----|----|----|----|----|----|-----|--|--|--|--|--|--|
| 7  | PM HOUR ENDING AT                                |    |    |    |    |    |    |    |     |  |  |  |  |  |  |
|    | <del>-   -   -   -   -   -   -   -   -   -</del> |    |    |    |    |    |    |    |     |  |  |  |  |  |  |
| •  | 10   | 16 | 16 | 14 | 15 | 13 | 12 | 11 | 41  |  |  |  |  |  |  |
| 4  | 4  | 3  | 3  | 4  | 3  | 4  | 4  | 4  | 9   |  |  |  |  |  |  |
| 7  |  | 5  | 5  | 4  | 4  | 4  | 6  | 4  | 24  |  |  |  |  |  |  |
| 2  | 2  | 1  | 1  | 2  | 2  | 2  | 1  | 2  | 10  |  |  |  |  |  |  |
| ī  | ī  | 1  | ī  | 1  | ī  | •  | •  | ĩ  | 15  |  |  |  |  |  |  |
| ĩ  | Į  | •  | •  | •  | •  |    | •  |    | 13  |  |  |  |  |  |  |
| -  | •  |    |    | 1  | 1  |    | •  |    | 7   |  |  |  |  |  |  |
|    |  |    |    | 1  |    |    |    |    | 2   |  |  |  |  |  |  |
| 2  | 31   | 27 | 26 | 24 | 24 | 24 | 23 | 21 | 126 |  |  |  |  |  |  |
| =1 |  |    |    |    | نت |    |    |    | 3   |  |  |  |  |  |  |

)F

|     | 1200<br>0428 | 101 |
|-----|--------------|-----|
| *   | • 2          | •7  |
| •   |              | .7  |
| • i | . 3          | 1.7 |
| •   | 2.7          | 7.2 |
| •   | •            |     |
|     |              | •   |
| •3  | 72.5         | 100 |

GALVESTON, TEXAS Municipal Airport

B-12

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

В

| :         |      |      | HOUR |       | RVATK<br>N MIS |       | WIND    | STEED. |            |      | ۱,   |
|-----------|------|------|------|-------|----------------|-------|---------|--------|------------|------|------|
| BHBICTICM | • 3  | . ,  | • 12 | 13 14 | 19 30          | 25 31 | 27 - 38 | × 4    | 47<br>CV90 | 1014 | ľ    |
| N         | - 2  | 5    | 1.7  | 2.0   | 1.3            | - 5   | •1      | +      |            | 5.7  | 1    |
| NNE       | - 1  | •6   | 1.7  | 1.5   | 1.0            | • 3   | • 1     |        | +          | 5.6  | 12.4 |
| NE        | • 2  | -8   | 2.2  | 1.9   | •6             | •2    | +       |        | l          | 5.9  | 12   |
| ENE       | - 2  | -6   | 1.4  | 1.3   | .5             | •1    |         |        |            | 4.0  | 12   |
| Ε         | •2   | .9   | 2.2  | 1.9   | •6             | -1    | •       |        |            | 5.9  | 12   |
| ESE       | .1   | 1.1  | 3.7  | 3.3   | •6             | •1    |         |        |            | 8.9  | 1    |
| SE        | -2   | 1.7  | 6.0  | 4.0   | •6             | •1    | +       |        |            | 12.3 | ů.   |
| SSE       | .1   | 1.4  | 6.1  | 4.9   | •6             | +     | 1       |        | •          | 13.2 | 1    |
| S         | .3   | 1.6  | 6.1  | 5.1   | •9             | • 2   | +       |        | •          | 14-0 | 11   |
| SSW       | i .1 | •7   | 2.4  | 2.5   | .7             | -1    | +       | l      | i          | 6.4  | 1    |
| SW        | .2   | . 7  | 2.5  | 1.1   | .4             | • 1   |         |        | 1          | 4.1  | b.   |
| WSW       | .1   | .5   | .8   | • 3   | .:             | +     |         |        |            | 1.0  | y (  |
| ¥         | .1   |      | .7   | •3    | -1             |       |         |        | l          | 1.5  | : 1  |
| WNW       | .1   | -4   | 3.   |       |                | .1    | ۱ .     |        | 1          | 2.1  | h.   |
| NW        | .1   | . 5  |      |       |                | .2    | +       |        |            | 3.1  | 1    |
| KNW       | .1   | - 3  | . 7  | -8    | .7             | .4    | •1      | +      |            | 3.0  | 1    |
| CALH      | 1.1  | ``   | 1    | 1     | 1              | l     |         | 1      | 1          | 1.1  | ıl   |
| TOTAL     | 3.5  | 12.6 | 39.0 | 32.5  | 9.5            | 2.3   | .5      | .1     |            | 100  | 12:  |

## PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND E RELATIVE HUMIDITY:

|           | SCA     | OUP<br>LE O | 10       | W       | HO<br>MLP |           | <b>D</b>         | REI      | ATIN      | # Ht      | MID       | STY (     | <b>%</b> 1 |
|-----------|---------|-------------|----------|---------|-----------|-----------|------------------|----------|-----------|-----------|-----------|-----------|------------|
| OF<br>DAY | O-<br>3 | 4. 7        | g.<br>16 | Ç.<br>3 | 4-<br>12  | 12-<br>24 | 25.<br>&<br>OVE2 | c.<br>29 | 33.<br>49 | 50.<br>69 | 70-<br>79 | 80.<br>81 | 90-<br>100 |
| 00        | 49      | 18          |          | 4       | 57        | 36        | 3                | +        |           | 14        | 25        |           | 28         |
| 01        | 46      | 19          |          | 5       | 56        | 36        |                  | +        |           | 14        | 23        |           | 29         |
| 02        | 47      | 19          | 34       |         | 56        | 35        |                  | +        |           | 13        | 23        | 32        | ; 30       |
| 03        | 45      | 19          | 36       | 6       | 58        | 34        |                  | +        |           | 13        | 22        |           | 31         |
| 04        | 45      | 19          | 36       |         |           | 33        |                  | +        |           | 12        | 22        |           | 33         |
| 05        | 40      | 22          | 38       |         | 59        | 32        |                  | +        | , -       | 11        | 19        | 35        | 34         |
| 06<br>07  | 35      | 23          | 42       |         | 56<br>55  | 33<br>36  |                  | 1        | 1         | 11        | 20        | 35        | 34         |
| 06        | 33      | 24          | 44       |         | 51        |           |                  | ١.       | 1 2       | 18        | 25<br>28  | 33<br>30  | 29         |
| 09        | 31      | 25          |          |         | 48        | 46        |                  | ‡        |           | 25        |           |           | 17         |
| 10        | 31      | 26          | 44       |         | 45        | 50        |                  |          |           | 31        | 29        |           | 12         |
| ii        | 32      | 25          | 43       |         | 43        |           |                  | .        | -         | 35        | 28        | 20        | و ا        |
| 12        | 33      | 24          | 43       |         | 41        |           | 3                | 1        |           | 36        | 27        | 19        | ĺ          |
| 13        | 34      | 24          | 42       | 1       | 40        | 56        | 3                | 1        | 10        |           | 26        |           |            |
| 14        | 35      | 23          | 42       | 1       | 40        | 58        |                  | 1        | 11        | 38        | 24        | 19        | 1 7        |
| 15        | 37      | 20          | 43       | 1       | 42        | 55        | 3                | 1        | 12        | 36        | 25        | 19        | 8          |
| 16        | 38      | 19          |          | 1       | 45        | 51        |                  | 1        | 10        | 35        | 24        | 19        | 10         |
| 17        | 38      | 18          | 46       |         | 51        | 45        |                  | 1        |           |           | 25        | 20        | 14         |
| 18        | 37      | 19          | 44       | 2       | 54        | 41        | 5                | +        |           |           |           |           | 17         |
| 19        | 39      | 20          | 41       | 4       | 57        | 37        |                  | +        |           | 22        | 27        |           | 21         |
| 20        | 42      | 20          | 38       | •       | 57        | 36        | 2                | +        |           | 20        |           |           | 22         |
| 21        | 45      | 20          | 34       | 4       | 58        |           | 2                | 1        |           | 18        |           |           |            |
| 22        | 47      | 20          | 33       | 4       | 57        | 37        |                  | ١.       | 3         | 16        |           |           | 26         |
| 23        | 40      | 19          | 33       | 5       | 56        |           |                  |          |           | 16        |           | 30        | 21         |
| AVG       | 39      | 21          | 40       | 3       | 52        | 42        | 3                |          | 5         | 22        | 25        | 24        | 51         |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

C OCCURRENCES OF PRECIPITATION AMOUNTS:

|                | •    |    | ,  |    | 1    | FREC | HUEN | CY C | e c | CCU | RRE | YCE         | FOR | EAC | HH  | OUR | OF  | THE | DAY  |      |    |    |      |     |   |
|----------------|------|----|----|----|------|------|------|------|-----|-----|-----|-------------|-----|-----|-----|-----|-----|-----|------|------|----|----|------|-----|---|
| INTENSITIES    |      |    |    |    | M. H | OUR  | ENDI | W AT |     |     |     |             |     |     |     | P   | M H | OUR | ENDI | NG A | 1  |    |      |     | Ľ |
|                | •    | 2  |    | •  | 3    | 6    | ,    | •    | •   | 10  | 11  | <b>4004</b> | -   | 2   | ,   | 4   | 153 |     | 7    |      | •  | 10 | 11 1 | H-0 | ľ |
| MCE            | 111  | 12 | 12 | 13 | 12   | 14   | 11   | 12   | 11  | 10  | 9   | 8           | 7   | 7   | 6   | 6   | 7   | 7   | 7    | 7    | 8  | 7  | 7    | 10  | Ī |
|                | 3    | 4  | 3  | 4  | - 4  | 3    | 3    | [ 2  | 3   | 4   | 2   | 1           | 1   | 1   | 3   | 2   | 2   | 1   | 2    | 3    | 2  | 3  | 3    | 3   | į |
| 92 10 09 PV    | 1 3  | 4  | 6  | 6  | 5    | 4    | 5    | 4    | 4   | 3   | 2   | 2           | 2   | 2   | 2   | 3   | 3   | 4   | ٠,   | 4    | 4  | 3  | 4    | 4   | ! |
| 0 10 24 W      | 1    | 1  | 1  | 1  | 1    | 1    | 1    | 2    | 1   | 1   | 1   | 1           | 1   | 1   | 1   | 1   | +   | 1   | 1    | +    | 1  | 1  | 1    | 1   | í |
| 10 49 m        | +    | 4  | •  | +  | +    |      | +    | +    | •   | +   | +   | +           | 1   | +   | li  |     | +   | +   | +    | +    |    | +  | -1   | •   | I |
| 10 99 W        | 1    |    |    | +  |      |      |      | 1    |     | +   |     | 1           | - 1 | i   | 1 1 | +   |     | - 1 |      |      |    | +  |      |     | ı |
| 9 TO 199 at    |      |    |    |    |      |      |      |      |     |     |     |             | •   |     | +   |     |     |     |      |      |    | i  | 1    |     | ı |
| IS RE AND OVER | 1    |    |    |    | . 1  |      |      |      |     |     |     |             | į   |     |     |     |     |     |      |      |    |    |      |     | ı |
| DTAL           | 1 18 | 21 | 23 | 24 | 22   | 22   | 20   | 20   | 19  | 17  | 14  | 13          | 11  | 11  | 92  | 32  | 12  | 13  | 13   | 34   | 15 | 15 | 14   | 17  | ļ |

PERCENTAGE FREQUENCIES OF D CEILING-VISIBILITY:

| <u></u>               |   |             |     |     | CERLIN        | C GEE         | )          |                |              |     |
|-----------------------|---|-------------|-----|-----|---------------|---------------|------------|----------------|--------------|-----|
| VISIBILITY<br>(AKCES) | • | 184.<br>284 | # # | #   | 1006-<br>1100 | 3505-<br>3106 | 330<br>440 | 3863-<br>17308 | CYSE<br>FREC | 101 |
| 0 10 1/8              | • | •           | +   | +   |               |               |            |                | +            |     |
| 2/16 TO 3/8           |   | •           |     | 1 1 | +             |               |            | Ì              |              | +   |
| 1/2 10 3/4            | • | +           | •   |     | +             |               | l          |                | +            | 1   |
| 1 10 21/2             | • | +           | 1   | 1   | +             | +             | +          | •              | 1            | 4   |
| 3 10 6                |   | •           | •   | 3   | 3             | +             | +          | +              | 7            | 13  |
| 7 10 15               |   |             | •   | 2   | 12            | 5             | 4          | 1              | 39           | 62  |
| 26 10 36              | i |             |     |     | 2             | 1             | 2          |                | 9            | 12  |
| 35 OR MORE            |   |             |     | +   | •             |               | 1          | +              | 6            | 7   |
| TOTAL                 |   | 1           | 1   | 6   | 15            | . 7           | 5          | 2              | 62           | 100 |

## ITY OCCURRENCES:

| JH                                     |                   |                        |     | 25 M | PH . | AHO . | OYER |             | 4  |
|--|-------------------|------------------------|-----|------|------|-------|------|-------------|--|
| E                                      | É                 | * 15.                  | 5,8 | Š    | £    | 13.70 | -    | <b>2018</b> | POTAL CES  |
| +<br>2<br>5<br>10<br>11<br>2<br>+<br>+ | + 25<br>13<br>2 + | 1<br>4<br>12<br>3<br>1 |     |      | 21   | * *   | ++1+ | 1 1 +       | 27<br>29<br>126<br>416<br>1016<br>1956<br>2244<br>1736<br>843<br>328<br>59 |
| . 31                                   | 23                | 20                     | 1   | ł    | 2    | 1     | lı   | 2           | 3767   |

ar total divided by 10). ake their sums exactly ess than U.5.

## **OUNTS:**

|     | OF THE DAY |      |      |          |    |     |    |      |  |  |  |  |  |  |  |
|-----|------------|------|------|----------|----|-----|----|------|--|--|--|--|--|--|--|
| -   | -          | ,    | •    | <b>-</b> | 10 | 11  | 40 | BATE |  |  |  |  |  |  |  |
| 7   | - 4        |      |      |          | 7  | 7   | 10 | 30   |  |  |  |  |  |  |  |
| 2   | ា          | 21   | - 1  | 2        | 3  | 3   | *3 | 6.   |  |  |  |  |  |  |  |
| 2   | Ĺ          | 2    | 4    | 1        | 1  | -   | [  | 14   |  |  |  |  |  |  |  |
| 3   | - 7        | 7    |      | 7        | 1  | 7   |    | 10   |  |  |  |  |  |  |  |
| Ţ   |            | -    | I    | - 1      | لد | - 1 |    | 6    |  |  |  |  |  |  |  |
|     | 7          | ٦    | _ Ti | i 1      |    |     | 1  |      |  |  |  |  |  |  |  |
| - 1 |            |      |      | 1        | •  |     |    | 7    |  |  |  |  |  |  |  |
|     |            |      |      |          |    |     |    | 4    |  |  |  |  |  |  |  |
|     |            | !    |      |          |    |     |    |      |  |  |  |  |  |  |  |
| 12  | 13         | [13] | 14   | 15       | 15 | 14  | 17 | 70   |  |  |  |  |  |  |  |

P

| -        |     |                     |
|----------|-----|---------------------|
|          | 911 | 101                 |
| <u>'</u> | •   |                     |
| ٦        | +   | 1                   |
|          | •   | +                   |
|          | •   | 1                   |
| 1        | 1   | 13                  |
| 1        | 39  | 62                  |
| ٠        | 9   | 13<br>62<br>12<br>7 |
| •        | 6   | 7                   |
| 2        | 62  | 100                 |

# PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

В

E

| PRICION | ١   |     |     |       |       | 110 HU    |     |      |     |           | - 1  |            |
|---------|-----|-----|-----|-------|-------|-----------|-----|------|-----|-----------|------|------------|
|         |     | • • | ,   | 13 18 | 19 34 | , 25 - 31 | n n | , 30 |     | el<br>Mil | 1014 | ,          |
| K       | - 3 | 3   | 7   | +     | i ·   | 1 ^       | :   | ï    |     |           | 7    | •          |
| NNE     | 3   | 3   | +   | +     | l     |           | 1   | 1    | 1   |           | 7    | 4          |
| NE      | 4   | 4   | +   | +     |       | l         | i   | 1    | 1   |           | . 8  | 4          |
| ENE     | 2   | 2   | +   | +     | +     | 1         | i   | į    | i   |           | 4    | 4          |
| E       | 2 2 | 1   |     | +     | +     | ! .       | 1   | 1    | - 1 |           | 3    | 4          |
| ESE     | 1   | 1   | +   |       | į.    | 1         | ļ   | :    |     |           | 2    | 4          |
| SE      | 1   | 1   | •   | +     |       | 1         | i   | i    |     |           | 2    | 5          |
| SSE     |     | 1   | 1   | +     | . +   | i +       | •   |      | i   |           | , 2  | 1 7        |
| 5,      | 1   | 2   | 2   | 1     | ; •   |           | :   | :    | •   |           | 5    | 7          |
| SSW     | 1   | 3   | 3   | 1     | . +   |           | ' + | •    |     |           |      | , 8        |
| SW      | i   | 3   | 3   | 1     |       |           | 1   | :    | :   |           | 6    | 7          |
| WSW     | ' i | 3   | : 3 | 1     |       | . +       |     |      | :   |           | · •  | ; (        |
| W       | i   | 3   | : 3 | 1     | i +   | 1         | i   |      | 1   |           | 1 8  | ; 7        |
| WNW     | i   | 3   | 5   | 1     | ! +   | ł         | i   | :    | I   |           | 10   | 8          |
| NW      | 1   | 3   | 4   | 1     | . +   | +         | :   | 1    | - 1 |           |      | ; 7        |
| NNW     | 1   | 3   | 2   | +     |       | 1         | 1   | i    | i   |           | 1 7  | , 6        |
| CALM    | . 6 |     | ļ   | 1     | 1     | 1         | İ   | i    | - 1 |           | 6    | l          |
| TOTAL   | 28  | 38  | 28  | 6     | +     | 1 +       | .1+ | 1.   | 1_  |           | 100  | <u>∟</u> 6 |

## PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                  |    | פרסי<br>סחס   |  | W              | IND      | SPEE         | 2                     | RE       | ATIV      | E HI      | JAIO      | ITY (     | <b>%</b> } |
|------------------|----|---|--|----------------|----------|--------------|-----------------------|----------|-----------|-----------|-----------|-----------|------------|
| OUR<br>CF<br>XAY | 9  | 4. 7  | 8.<br>10                               | . Ģ 19         | 4.<br>12 | 12.<br>24    | 25-<br>&<br>8<br>9768 | 0-<br>29 | 30-<br>49 | 50-<br>69 | 70-<br>79 | 50-<br>57 | 93-<br>180 |
| 00               | 40 |   | 62                                     | 46             | 50       |              | -                     | 1        | -         | 11        | 23        | 47        | 14         |
| 01               | 38 | • •   | 55                                     | 40             | 49       | -            |                       | ,        | 1 3       | 12        | 21        |           |            |
| 02               | 36 | .07<br>77<br>66<br>66<br>81<br>10<br>12<br>13<br>13 | 52557557555555555555555555555555555555 | 46<br>49<br>49 | 49       |              |                       | 1 1 1 1  | 5555      | 11        | 20        |           |            |
| 03               | 36 |   | S.A.                                   | 10             | 49       | 2            |                       | ,        | 5         | 12        | 19        |           |            |
| 04               | 35 | 6   | 50                                     | 49             | 49       | 2            | ľ                     | 1        | 5         | 11        | ! 20      |           |            |
| 05               | 35 | 6   | 59                                     | 49             | 49       | 2            | ٠                     | 1        | 5         | 122       | 20        |           |            |
| 06               | 33 | Ě   | 59                                     | 46             | 50       | 2            | †<br>*                | 1 -2     | 6         | 13        | 24        | 39        | 1 17       |
| 07               | 32 | 10  | 56                                     | 45             | 53       | 2            | 1                     | 2        | 7         | 20        | 30        | ¦ 31      | 10         |
| 08               | 37 | 12  | 51                                     | 34<br>19       | 62       | 4            |                       | 3 5 6 9  | 5         | 31        | 34        |           | 1 4        |
| 09               | 46 | 12  | 42                                     | 19             | 76       | 5<br>9<br>14 | *                     | 5        | 10        | 44        | 29        | 10        | 2          |
| 10               | 54 | 13  | 34                                     | 10             | 81       | 9            | +                     | 8        | 12        | 1 20      |           |           | 1          |
| 11               | 58 | 13  | 28                                     | 3              | 83       | 14           | ; +                   | 1 9      | 13        | 62        |           | ! 3       | •          |
| 12               | 60 | 14  | 26<br>24                               | 1              | 77<br>79 | 18           | ; +                   |          |           | 65        | 10        | 2         |            |
| 13               | 62 | 14  | 24                                     | 1              | 77       | 22           |                       | 9        | 1 29      | . 67      |           | 1         | 1          |
| 14               | 62 |   | 24                                     | 1              | 79       | 20           | •                     |          | 14        | 67        | 8         | 1 2       | 1          |
| 15               | 61 |   |  | 1              | 83       | 16           |                       | ۇ ب      | 1:        | 67        | 11        | 1 2       | ; 1        |
| 16               | 61 |   |  |                |          |              |                       | 1 5      | 1         |           |           | 4         | 1          |
| 17               | 60 |   |  | 6              |          | 9            | 1 1                   | 4        |           | 46        |           | ! . 5     |            |
| 18               | 58 |   | 28                                     | 16             |          |              | 1                     | 1 3      |           | 25        |           |           | 7 3        |
| 19               | 55 | 13  |  | 23             |          | 2            |                       | 1 2      |           | 17        |           |           | ) 3        |
| 20               | 52 |   |  |                |          | 2            |                       | 1        |           |           |           |           |            |
| 21               | 49 | 11  |  |                | 60       | 2            | 1                     |          |           | 1 13      | 29        |           |            |
| 22               | 46 |   |  |                | 57       | Z            | •                     | 1        |           | i 13      | 1 24      | 47        |            |
| 23               | 43 |   |  |                | 52       |              | 1.                    | 1        | 1         | 1 2       | . 24      | * * * 7   | 12         |
| AVG              | 45 | 11  | 41                                     | 28             | 66       | •            | 1                     | ' I      | ין י      | 1; 34     | ! 23      | 26        | יןי        |

A

| WWO  |  |                                       | 04 /                      | U.A.                                      |                                      |                                     | Γ                      |   | 5-14  | H.W  |   |                                   |                  |               | 15-24                | MPM                            |                   |                   |        | 25 M      | PH.                    | A#0     | CVE         |          | 4  |
|--|--|---------------------------------------|---------------------------|---|--------------------------------------|-------------------------------------|------------------------|---|---|--|---|-----------------------------------|------------------|---------------|----------------------|--------------------------------|-------------------|-------------------|--------|-----------|------------------------|---------|-------------|----------|--|
| MA PARTY (**)  | ş,   | Í                                     | Ş                         | R.M.                                      | 200                                  | 5                                   | S<br>ER                | Í   | 30  | S. M   | £   | 4                                 | 2008<br>2        | į             | 5                    | MATER                          | m-m               | VAN CE            | e a    | 5         | wet                    | 36.92   | 404         | 1001 100 | TOTAL COL  |
| 109/105<br>104/100<br>99/95<br>94/90<br>84/90<br>79/95<br>74/70<br>69/65<br>64/60<br>59/55<br>54/50<br>49/45<br>49/45<br>39/35 | + 1<br>2<br>4<br>9<br>11<br>15<br>14<br>13<br>11<br>5<br>3 | 13<br>27<br>39<br>39<br>31<br>13<br>6 | 90<br>71<br>44<br>13<br>2 | 36<br>132<br>174<br>156<br>76<br>39<br>15 | 223<br>444<br>371<br>185<br>73<br>18 | 22<br>141<br>701<br>164<br>59<br>11 | 46<br>33<br>~ .17<br>9 | 21<br>40<br>54<br>75<br>87<br>81<br>60<br>28<br>7 | 206<br>393<br>390<br>302<br>177<br>94<br>50<br>12 | 12<br>143<br>315<br>323<br>208<br>75<br>30<br>10 | 25<br>220<br>346<br>294<br>118<br>40<br>9 | 19<br>73<br>143<br>105<br>28<br>4 | 8<br>9<br>5<br>1 | 17<br>13<br>5 | 61<br>51<br>28<br>13 | 11<br>17<br>19<br>13<br>5<br>1 | 10<br>5<br>2<br>1 | 14<br>7<br>2<br>4 | 11221+ | 1 3 4 2 1 | + + 11 31 4 51 +<br>11 | 1 1 1 2 | +<br>1<br>1 | 1        | 11<br>4<br>7<br>28<br>117<br>380<br>881<br>1654<br>2193<br>1704<br>428<br>107<br>10<br>10<br>428 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

# C OCCURRENCES OF PRECIPITATION AMOUNTS:

|                  |      |    | FREQUENCY OF OCCURREN |    |     |     |       |       |     |    |       |      | FOR | EAC | н н | OUR | OF  | THE | DAY |      |    |       |    |       | _    |
|------------------|------|----|-----------------------|----|-----|-----|-------|-------|-----|----|-------|------|-----|-----|-----|-----|-----|-----|-----|------|----|-------|----|-------|------|
| INTENSITIES      |      |    |                       |    | M H | OUR | ENINI | VG 41 | ,   |    |       |      |     |     |     | P   | R H | OUR | END | NG A | 7  |       |    |       | or   |
|                  | 1    | ,  | ,                     | 4  | 3   | 6   | ,     | •     | •   | 12 | 11    | 9000 | •   | 7   |     | 4   | •   | •   | 7   |      | •  | 10    |    | Brad) | 34.5 |
| 1#41             | 8    | 10 | 11                    | 11 | 15  | 14  | 13    | 13    | 11  | e  | 9     | 8    | 6   | 7   | - 6 | 7   | 6   | 8   | 8   | ₹ 8  | 7  | 7     | 7  | 8     | 27   |
| (# 1%            | 2    | 3  | 3                     | 3  | 2   | 3   | 3     | 3     | 1   | 2  | 3     | 1;   | 2   | 2   | 3   | 2   | 2   | 1   | 2   | 3    | 2  | 2     | 2  | 2     | 4    |
| 12 10 mm         | 4    | 4  | 3                     | 4  | 4   | 4   | 4     | 3,    | . 3 | 3  | 2     | 3    | 4   | 3   | 3   | 3   | 3   | 3   | 4   | 3    | 4  | 5     | 5i | 4     | 10   |
| HI 11 24 FF      | 21   | 1  | 1                     | 1  | 1   | 1   | 1     | 1     | 1   | 1  | ' 1   | 1    | 1   | 1   | 1   | 1   | 1   | 1   | 1   | •    | 1  | 11    | 1; | 1     | 7    |
| 25 10 41 6       |      | -  | 1                     | 1  | 1   | +   | •     | •     | +   |    | , 1   | +    | +   | 1   | +   | +   | . + | +   |     | •    | 1  | +!    | ٠, | 1     | . 6  |
| to to me         | 1 1  | +  |                       | +  | i   |     | i     | 4     | •   |    | •     | •    | Į   |     |     |     |     |     |     | !    | 1  |       | •  |       | 5    |
| tier for tier to |      |    |                       |    |     |     |       |       |     | Ì  | İ     | 1 1  | •   |     |     |     |     |     | ļ   |      |    | li    | ł  |       | 1    |
| 2141 PA ANI 1918 | 1 1  |    |                       |    |     |     |       |       |     |    |       |      | •   |     |     |     |     |     |     | i .  |    | 1     |    |       |      |
| TUTPL            | 1 17 | 18 | 20                    | 19 | 23  | 22  | 21    | 19    | 17  | 14 | 1 1 5 | 14   | 13, | 13  | 13  | 14  | 13  | 14  | 14  | 14   | 14 | : 15i | 16 | 16    | 61   |

#### PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY: D CERNIG UTETI VISIBELLY 363 444 700 (40) (ASTES) 0 10 1/5 3/16 10 3/8 \* + + 1 + 1 6 17 37 5 1/2 10 3/4 + 2 4 3 + 13 26 48 6 110 21/2 3 10 4 7 10 15 20 10 30 35 CH MARE IOIAI

LOS ANGELES, CAL. Int. Airport

## IDITY OCCURRENCES:

| 5 / | MPA                       |                             |                   |                | 23 AL     | P H. /        | 446   | 040         |        | 4         |
|-----|---------------------------|-----------------------------|-------------------|----------------|-----------|---------------|-------|-------------|--------|-----------|
|     | £                         | £                           | 10 HOL            | <b>8</b><br>58 | Ş         | Š             | r R   | <b>1</b> 50 | San da | TOTAL OCA |
| )   | 11<br>17<br>19<br>13<br>5 | +<br>2<br>6<br>10<br>5<br>2 | 3<br>14<br>7<br>2 | 11221+         | 1 3 4 2 1 | + + 1 3 4 3 + | 1 1 1 | 1 1         | 1      |           |
|     | 66                        | 27                          | 25                | 6              | lii       | İ 11          | ! 2   | 2           | 1 2    | 767       |

-year total divided by 10).
> make their sums exactly
t less than 0.5.

## MOUNTS:

| UR | OF ' | THE      | DAY |      |     |    |      |     |          |
|----|------|----------|-----|------|-----|----|------|-----|----------|
|    |      | ו ויוניכ |     | G AT |     |    |      | 二   | <b>.</b> |
| -  | 7]   | •        | 7   | • 1  | =   | 10 | 11 1 | 2   |          |
| 7, | 6    | el       | 8   | 81   | 7   | 7, | 7    | 8   | 27       |
| Z. | 2    | 1        | 2   | 3    | 2   | 2  | 2;   | 2,  | 4        |
| 3; | 3    | 3        | 4   | 3    | 4   | 5  | 51   | 4   | 10.      |
| 1  | 1    | 1        | 1   | *    | - 1 | 1, | 1;   | 31  |          |
| •  | 1    | •i       | Ì   | 1    | - 4 | 7  | Ţ,   | *!  | 5        |
|    |      | 1        | i   | ı    | 1   |    | ï    | - 1 | í        |
| i  |      |          | . ! | ı    |     | l  | - 1  | -   | Ī.       |
| 14 | 13   | 14       | 14  | 14   | 14  | 15 | 16   | 16  | 61,      |

OF

| 3000<br>7300 | 0712     | 101           |
|--------------|----------|---------------|
|              | •        | 1             |
| <b>*</b>     | 1 6      | 1<br>2<br>13  |
| 1            | 17<br>37 | . 26          |
| 1 *          | 5 2      | 6<br>2<br>100 |
| 7            | 68       | 100           |

LOS ANGELES, CAL. Int. Airport

B-14

# Precentage frequencies Of wind direction and speed:

|             |     |      | HOUR   | Y OSE   | ZVATE   | THE U    | CHIN  | SALES.       |                |       |    |
|-------------|-----|------|--------|---------|---------|----------|-------|--------------|----------------|-------|----|
| \$200CT-GBH | • • | 4 7  | 8 - 13 | 13 - 16 | 10 - 54 | 27 M     | n · 2 | <b>39</b> 44 | 91.72<br>G1:72 | 101M  | ľ  |
| H           | 1   | 1    | +      | *       | +       | +        | +     |              |                | 2     |    |
| NAE         |     | 2    | 1      | +       |         | •        | ļ     |              | 1              | Z     |    |
| NE          | 1   | 2    | 1      | +       | +       | l        | i     | i            | 1              | 1 :   | 1  |
| ENE         | 1   | 3    | 1      |         | •       | •        | ļ     | l l          | i              | ! ?   | 1  |
| E           | 2   | 3    | 1      | +       | +       | ł        | 1     |              | 1              | 1 2   | ı  |
| ESE         | 1   | 2    | 1      | •       | +       | l        | I     | 1            |                |       | ļ. |
| SE          | 1   | 2    | 1      | •       | 1 +     | +        | I     | i            | 1              | 4     | i  |
| SSE         | 1   | 1    | •      | +       | +       | +        | 1 *   | 1            | 1              | 2 2 2 | Į  |
| S           | 1   | 1    | +      | +       |         |          | ł     | 1            | 1              | 1 2   | ı  |
| 55W         | 1   | 1    | +      |         | +       |          | 1     | 1            | 1              | 1 7   | ı  |
| SW          | 1   | Z    | 3      | 1       | +       | 1        | i     | 1            | 1              | 1     | 1  |
| WSW         | 1   | 5    | 10     | 4       | +       | +        | •     | !            | 1              | 20    | 1  |
| ¥           | 1   | 5    | 7      | 4       | +       |          | 1 *   | i i          | 1              | 17    | i  |
| MAM         | 1   | 2    | 1      | 1 +     | +       | •        | ١.    | į .          | 1              | 1 3   | 1  |
| HW          | 1 2 | 1    |        | i +     |         | +        | 1 *   | ł            | 1              | 1 3   | 1  |
| HNW         |     | 1    |        | . +     | +       |          | 1 *   | 1            | 1              | 1 .2  | 1  |
| CALM        | 13  | 1    | ١.     | I       | i.      |          | 1.    | ĺ            | 1              | 133   | 1  |
| TOTAL       |     | 1.33 | 127    | اللل    | لمن     | <b>∸</b> |       |              |                | 7100  |    |

## PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

E

| -                 |      |      |             |              |     |            |                  |              |           |            |           |       |       |   |
|-------------------|------|------|-------------|--------------|-----|------------|------------------|--------------|-----------|------------|-----------|-------|-------|---|
|                   |      | LE O |             | ₩            | IND | SPEE       | D                | RE           | LATIV     | E H        | JMIS      | HTY ( | (%)   |   |
| HOUR<br>OF<br>DAY | 0-   | 4. 7 | \$-<br>10   | g.<br>3      | 4-  | 13-<br>24  | 25-<br>B<br>OVER | 0-<br>27     | 30-<br>47 | 50-<br>69  | 70-<br>79 | 80-   | 100   |   |
|                   |      | ļ    |             |              |     | ļ          |                  |              | İ         | i<br>!     | !         |       | 1     | : |
| 00                | 51   | 9    |             |              | 54  |            |                  | 2            | . 6       |            |           |       |       |   |
| 01                | 49   | ] 7  | 44          | 46           |     | 3          | . +              | į 2          | 6         |            |           |       |       |   |
| 02                | 47   |      | 45          | 47           |     |            | •                | 1 2          | 6         |            |           |       |       |   |
| 03                | 45   | i A  | 4 48        |              | 51  | 3          | 4                | 2            | ۽ إ       |            |           |       |       |   |
| 04                | 43   |      | . 50        |              |     | , 2        | 1                | 1 3          | . 7       | 9          | 14        | 43    |       |   |
| 05                | 1 40 |      | 52          | 48           | 50  | 2          |                  |              | 7         | 4 9        | 7 1:      | 42    | 25    | ï |
| 06                | 37   |      | 54          | 46           | 51  | 1 3        |                  |              |           | 1 19       |           |       |       |   |
| 07                | 35   |      |             | 43           | 54  | 1 3        | 1 1              | 1            |           |            | . 2       |       |       |   |
| 08                | 39   |      | IJ 51       | 36           |     | i :        |                  | ! !          |           |            |           |       |       |   |
| 09                | 44   |      |             |              |     |            |                  | 1            | 1         |            |           |       |       | : |
| 10                | 59   |      |             | 16           | 77  | 1          |                  | 4 1          |           | 3 50       |           |       | •     | Ľ |
| 11                | 58   | 12   | 2 3:<br>3 2 | , ,,         | 7   | 2 2        | י וכ<br>ע        | ìi           | 2 1       |            |           |       |       | i |
| 13                | 61   |      | 3 4         | <b>;</b> ;   | 1 6 | 3          | ] :              | 1 1          |           |            |           |       |       | i |
| 14                | 6    | 1 11 | 2 2<br>2 2  | <b>;</b> ;   | 1 5 |            |                  |              | B: 1      |            |           |       |       | i |
| 15                | 6    | 3: 1 | 3 2         |              | 1 5 |            | i                | 1            | 7, 1      |            |           | 7     |       |   |
| 16                | 1 5  | 7, 1 | 3 5         | 7            | 2 6 |            | 2                | 2            | 5 1       |            |           | 5, 1  | 6     | 2 |
| 17                | 15   |      | 2 2         | o i          | 5 6 | 9 2        | 6.               | +            | 3         | 7 3        |           | 5 1   | 7( )  | 3 |
| 18                | 5    |      | 2, 3        | 3 1          |     | 4 1        | 5                | •            | 2.        | 5 2        |           |       | 9     | 5 |
| 19                | 5    |      | 1 3         | <b>ال تو</b> |     |            | ci .             | #            | 3         | 5 1        | 7, 3      | 1 3   | 7' 1  | 8 |
| 20                | 5    |      |             | 4 2          |     |            | . نو             | <b>4</b>     | 2         | 5 1<br>5 1 | 4' 2      |       | 0. 1: | 1 |
| 21                | 5    | 6 4  | 9 3         | 5 3          |     | 3.         | 5                | <b>+</b> j . | 2:        | 6' 1       | 2 2       | 5i 4  | 2, 1  | 3 |
| 22                | 5    | 5    | 7 3         | 71 3         |     | o <u>i</u> | 3                | <b>+</b> !   | 2,        | 6 1        |           |       | 4-1   | - |
| 23                | 5    | 2    | 7 3         | 7, 4         |     | 7          | 5<br>3<br>3      | +            | 2i        |            |           |       | 6 1   |   |
| AV                | લંક  | 1 1  | o s         | 9, 2         | 6 6 | 1 1        | 2                | +            | 5         | 0, 2       | 7: 2      | 31 2  | B 1   | 1 |
|                   | l    | 1    | 1           | J            | ì   | ı          | 1                | 1            | l         | 1          |           | •     | :     |   |
|                   |      |      |             |              |     |            |                  |              |           |            |           |       |       |   |

| WWWD  |                     |   | 04 /  | MPJK.            |  |                                     |              |  | 5-14 /  | AP.K  |                      |  |            |  | 15-24                | мрн  |    |              |            | 25 M            | PH.                                     | AND                       | OVER               |           | 4   |
|---|---------------------|---|---|------------------|--|-------------------------------------|--------------|--|---|---|----------------------|--|------------|--|----------------------|--|----|--------------|------------|-----------------|---|---------------------------|--------------------|-----------|---|
| 3 ( )   | \$<br>5.8           | N. S.   | £   | ar a             | ***  | 4 161                               | <b>4</b> 000 | *  | 5   | £ 2   | 4                    | THE STATE OF   | riche<br>R | ş  | Ç                    | The state of the s | 1  | <b>18</b> 19 | <b>5</b> x | n a             | MA                                      | £                         | 4                  | 6         | TOTAL OBS   |
| 4/100<br>9/ 95<br>4/ 97<br>9/ 89<br>4/ 80<br>9/ 77<br>4/ 55<br>9/ 65<br>9/ 45<br>4/ 35<br>4/ 30<br>9/ 15<br>6/ 105<br>9/ 15 | 11 22 11 22 1 + + + | 13<br>12<br>12<br>13<br>13<br>13<br>13<br>14<br>116 | +2105<br>1031<br>1031<br>1031<br>114<br>469 | 32<br>113<br>135 | 191<br>170<br>135<br>147<br>87<br>32<br>12 | 167<br>210<br>205<br>117<br>30<br>1 | •            | 30<br>69<br>108<br>75<br>46<br>34<br>29<br>15<br>32<br>+ | 24<br>14<br>164<br>2434<br>177<br>95<br>210<br>106<br>4<br>31 | 57<br>171<br>174<br>140<br>102<br>137<br>21 | 112<br>39<br>11<br>1 | 11<br>31<br>85<br>120<br>139<br>171<br>138<br>62<br>10 | 1 +        | 12<br>12<br>12<br>13<br>14<br>19<br>13<br>6<br>4<br>5<br>6<br>13 | 17<br>22<br>35<br>38 | *27<br>17<br>3509<br>28<br>52  | 13 |              | + +        | * +121+1++<br>5 | * | + + + + + 1 3 4 4 1 1 1 1 | * * 15762 + 2 + 23 | 1 2 2 1 + | 1<br>6<br>23<br>54<br>126<br>211<br>373<br>581<br>1001<br>1316<br>1274<br>1271<br>1238<br>772<br>343<br>123<br>40<br>10<br>10 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "4" indicates more than 0 but less than 0.5.

# C OCCURRENCES OF PRECIPITATION AMOUNTS:

|                |     |    |    |     | 1     | FREC | UEN  | CY ( | OF C | xcu | RRE | NCE  | FOR | EAC | :н н | OUR | OF  | THE | DAY  | •    |          |     |     |     |     |
|----------------|-----|----|----|-----|-------|------|------|------|------|-----|-----|------|-----|-----|------|-----|-----|-----|------|------|----------|-----|-----|-----|-----|
| INTENSITIES    |     |    |    | . / | NE. H | OUR  | ENDI | G A  | r    |     |     |      |     |     |      | ,   | M H | OUR | ENDI | NG A | T        |     |     |     | 2   |
|                | 1   | 7  | ,  | 4   | 5     | . 6  | 7    |      | •    | 10  | 11  | M004 | •   | 2   | ,    | 4   | •   | 4   | ,    | •    | •        | 10  |     | 20  | DAT |
| TRACE          | 38  | 36 | 36 | 38  | 45    | 46   | 47   | 49   | 43   | 42  | 46  | 47   | 45  | 48  | 47   | 43  | 42  | 39  | 40   | 36   | 34       | 32  | 38  | 36  | 4   |
| OF 199         | 14  | 15 | 16 | 16  | 14    | 14   | 15   | 17   | 16   |     |     | 13   |     | 15  | 17   | 17  | 16  | 15  | 14   |      | 16       |     |     | 15  | 1   |
| 02 TO 09 PM    | 21  | 25 | 25 | 26  | 23    | 24   | 23   | 22   | 24   | 22  |     | 22   |     | 25  | 25   | 26  | 24  | 24  | 23   |      |          |     |     |     | , - |
| 16 TO 24 IN    | 3   | 3  | 4  | 3   | 3     | 3    | - 4  | 3    | •    | 3   |     | 3    | 2   | 4   | 4    | 4   | 4   | 3   | 4    |      | -3       | - 5 | ~ 2 | • 4 | 12  |
| 25 10 49 m     | +   |    | +  | •   |       | [    |      | +    | +    | 1   |     | -    | +   | i   | +    |     |     | ī   |      | 4    | <b>4</b> | 1   | -   | _   | ! 4 |
| 90 TO 99 M     | 1 1 |    | 1  | l   | 1     |      |      |      |      | 1 1 |     |      |     |     |      |     | 1   |     |      |      |          |     |     |     | 1 7 |
| 00 TO 199 M    |     |    | ľ  |     | 1     |      | 1 1  |      |      | 1   |     |      |     |     |      |     |     |     | 1    |      |          | 1   |     |     | 1 - |
| RIVO DAY NO DO | i   |    | l  |     |       |      | l i  |      |      | li  |     |      |     |     |      |     |     |     | 1    |      |          |     |     |     |     |
| TOTAL          | 76  | 78 | 81 | 84  | 84    | 87   | 89   | 91   | 87   | 83  | 83  | 85   | no  | 92  | 93   | 80  | 85  | 82  | 81   | 78   | 76       | 77  | 75  | 73  | 50  |

# PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|                       |   |             |   |            | CETUR         | 3 (FEE       | 2            |               |              |     |
|-----------------------|---|-------------|---|------------|---------------|--------------|--------------|---------------|--------------|-----|
| VISIBILITY<br>(MULES) | ۰ | 146.<br>786 | - | ##4<br>### | 1886.<br>1980 | 2004<br>2100 | 2000<br>2000 | 5008-<br>9388 | 0v40<br>1700 | 101 |
| 0 TO 1/8              | 1 | +           | + | +          | +             | +            | +            | +             | 4            | 1   |
| 3/16 TO 3/8           | • |             |   | +          | +             | +            |              | +             | 4            | ī   |
| 1/2 TO 2/4            |   |             |   |            |               | +            |              |               | انا          | ī   |
| 1 TO 21/2             |   | +           | + | 1          | +             |              |              | +             | i            | 3   |
| 3 TO 6                |   | 4           | • | 1          | 2             | 1            | 2            | 3             | الما         | 11  |
| 7 10 15               | + | +           | + | 1          | 4             | 4            | 12           | 10            | 27           | 38  |
| 20 TO 36              |   |             |   |            | +             | 1            | 4            | 4             |              | 16  |
| 15 OR MORE            |   |             |   | +          |               |              |              | 1             | 7            | - 9 |
| TOTAL                 | 1 | 1           | 1 | 2          | 7             | 7            | 18           | 16            | 48           | 100 |

|              | NO                                      | OVER               |                            | 4   |
|--------------|---|--------------------|----------------------------|---|
|              | KK                                      | 4                  | 1                          | TOTAL OES.  |
| W ++NNNNNH++ | 111111111111111111111111111111111111111 | * * 257 62 + 2 + 3 | 11<br>33<br>22<br>21<br>11 | 1<br>6<br>23<br>54<br>211<br>373<br>581<br>10015<br>1274<br>1271<br>1238<br>772<br>343<br>123<br>40<br>10<br>10<br>40 |

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## PERCENTAGE FREQUENCIES OF WIND DIRECTION AND SPEED:

| Descrion |     |     |     | •  | но | UÁ | LY  | oes |    |    |      | OF  |   | ND | SP       | ED |            |       | Av   |
|----------|-----|-----|-----|----|----|----|-----|-----|----|----|------|-----|---|----|----------|----|------------|-------|------|
| DIRECTOR |     | 1   | •   | ,  | •  | 13 | ;;  | 18  | 19 | 24 | , 25 | 21  | × | ×  | <b>*</b> | *  | 47<br>Ovte | TOTAL | 2440 |
| N        | •   | 1   | •   | 1  | •  | +  | • • | +   |    | +  | :    |     | - |    |          | _  | -          | 3     | 5.1  |
| NNE      |     | + ' | ,   | +  |    | +  |     | +   |    |    | İ    |     |   |    | •        |    | ļ          | ii    | 4.0  |
| NE       | ,   | 1   | ļ   | +  |    | +  |     | +   |    | +  | 1    |     |   |    |          |    |            | i     | 4.1  |
| ENE      |     | +   | •   | +  |    | +  |     | +   |    | +  |      | +   |   |    |          |    |            | 1     | 7.4  |
| Ε        |     | 1   | i   | 1  |    | 1  | x   | 1   |    | +  | ì    | +   |   | +  |          |    |            | 4     | 10.1 |
| ESE      |     | 1   | •   | 3  |    | 4  |     | 4   |    | 1  | •    | +   |   | +  |          |    |            | 13    | 10.8 |
| SE       |     | 1   | i   | 2  |    | 2  | 1   | 1   |    | +  |      | +   |   |    | į        | -  |            | 6     | 7.9  |
| SSE      |     | 1   |     | 1  |    | 1  |     | 1   |    | 4  |      | +   |   | +  |          |    |            | 4     | 8.0  |
| 5        |     | 1 - | •   | 1  |    | 2  |     | 2   |    | 1  |      | +   |   | +  |          | +  | į          | 7     | 11.3 |
| SSW      |     | +   |     | 1  |    | 2  |     | 2   |    | 1  | t    | +   |   | +  |          | +  | +          | 7     | 13.0 |
| SW       |     | 1   | •   | 1  |    | 1  |     | 1   |    | +  | ,    | +   |   |    | ,        |    |            | 4     | 8.3  |
| WSW      |     | 1   |     | 1  |    | 1  | ,   | +   |    | +  |      | + . |   |    |          |    |            | 1 3   | 7.4  |
| W        |     | 1   | :   | 2  |    | 1  |     | +   |    | +  |      | +   |   |    |          | 1  |            | 1 4   | 5.8  |
| WNW      |     | 2   | į   | 4  | •  | 4  | •   | 1   |    | +  | į    | +   |   |    |          |    |            | 111   | 7.6  |
| NW       | :   | 3   | ļ   | 5  |    | 5  |     | 1   |    | +  |      | +   |   |    | Ŧ        | j  | [          | 14    | 7.3  |
| NNW      |     | 1   | 1   | 2  |    | 2  |     | 1   |    | +  | 1    |     | , |    |          |    |            | 6     | 7.3  |
| CALM     | 1   | 1   | ı   |    |    |    |     | _   |    |    | 1    |     | • |    | ŧ        | i  |            | l i i |      |
| TOTAL    | . 2 | 8   | : 4 | 27 | 2  | 5  | . : | 16  |    | 4  | ,    | 1   | į | +  | ŀ        | +  | +          | 100   | 7.7  |

# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

Ē

|            |          | LE O |          | W        | IMD<br>(M. I |     | 0         | RE  | LATIN    | Æ H | UANO     | ITY ( | (%) |
|------------|----------|------|----------|----------|--------------|-----|-----------|-----|----------|-----|----------|-------|-----|
| HOUR<br>OF | ۵        | 4    | 8.       | 0-       | 4-           | 13- | 25-       | 0-  | 30-      | 50- | 70-      | 20-   | 50- |
| DAY        | 3        | 7    | 10       | 3        | 12           | 24  | A<br>OYER | 29  | 49       | 69  | 79       | 89    | 100 |
| 00         | 37       | 9    | 54       | 36       | 50           | 13  | 1         | +   | 1        | 12  | 22       | 36    | 29  |
| 01         | 35       | 9    | 56       |          | 47           | 13  |           | +   |          | 9   | 19       | 39    | 32  |
| 02         | 33       | 9    | 59       |          | 45           | 13  | +         | +   | 1        | 7   | 17       | 39    | 36  |
| 03         | 30       | 8    | 61       |          | 45           |     | *         | +   | 1        | 6   | 15       | 40    | 39  |
| 04         | 27       | 9    | 64       |          | 42           | 13  | 1         | +   | 1        | 5   | 13       | 38    | 43  |
| 05         | 23       | 9    | 68       |          | 43           |     | 1         | +   | 1        | 4   | 12       | 39    | 44  |
| 06         | 20       | 9    | 72       | 42       | 44           |     | 1         | +   |          | 5   | 14       | 39    | 42  |
| 07<br>08   | 17<br>17 | 9    | 74       | 38       | 47           | ,   | 1         | +   |          | 7   | 20       | 37    | 35  |
| 08         | 18       | 10   | 75       | 32<br>27 | 51           | 16  | 1         | +   | 1        | 14  | 26       | 31    | 27  |
| 10         | 20       | 10   | 72<br>70 | 23       | 54<br>56     |     | 1         | +   | 2        | 27  | 25       | 25    | 20  |
| 11         | 23       | 10   |          | 20       | 57           |     | 1         | 1   | .5       | 37  | 22       | 22    | 14  |
| 12         | 25       | 10   | 65       | 16       | 58           |     | 1         | 2   | 10<br>17 | 41  | 19       |       | 10  |
| 13         | 25       | 12   |          | 14       | 60           |     | i         | 3   | 23       | 38  | 16<br>14 | 16    | 8   |
| 14         | 26       | 12   | 62       | 13       | 60           |     | i         | 4   | 27       |     | 13       | 13    | ا   |
| 15         | 27       | 11   |          | 14       | 56           |     | î         | 5   | 28       | 33  | 13       | 13    | 8   |
| 16         | 27       | 11   |          | 15       | 55           |     | î         | 5   | 28       | 32  | 13       | 14    | 9   |
| 17         | 28       | 12   | 60       | 16       | 55           |     | i         | ١ 🛪 | 23       | 33  | 13       | 17    | 13  |
| 18         | 30       | 12   | 58       | 18       | 54           |     |           | 3 2 | 18       | 33  | 15       | 18    | 13  |
| 19         | 31       | 12   | 56       | 21       | 56           |     | î         | ī   | 11       | 34  | 17       | 20    | 17  |
| 20         | 34       | 11   | 55       | 23       | 58           |     |           |     | 6        |     | 21       | 23    | 19  |
| 21         | 35       | 12   | 53       | 25       | 57           |     |           |     |          | 25  | 25       | 25    | Ži  |
| 22         | 36       | 10   | 53       | 28       |              | 16  | 1         |     | 3        | ZO  | 26       | 28    | 23  |
| 23         | 36       | 10   |          | 33       |              | 15  |           | +   | Ž        | 15  | 25       | 33    | 25  |
| AVG        | 28       | 10   | 62       | 28       | 52           | 19  |           | 1   | 9        |     | 18       | 27    | 22  |

PORTLAND, OREG Int. Airport

| WHO  |          |                         | 04 A                                   | LP.H. |     |                                |               |                                | 5-14 /  | ap.H.   |   |  |               |   | 15-24                              | MPJL                           |                             |                           |         | 25 M                                      | P.H.   | AHO   | OVER                                       |                     | -1   |
|--|----------|-------------------------|--|-------|-----|--------------------------------|---------------|--------------------------------|---|---|---|--|---------------|---|------------------------------------|--------------------------------|-----------------------------|---------------------------|---------|---|--|---|--|---------------------|--|
| es.<br>Haparis.<br>Tipuro.<br>CPI  | \$<br>5R | <b>1</b>                | 5                                      | Ę     | S a | 4014                           | 5,5           | 5                              | Ş   | 30.00   | <u> </u>  | ** 100.0                               | 5.7           | ×   | 2                                  | Ap.1976                        | Barrie                      | 14111                     | ž<br>Sa | SO-CE                                     | r e  | No.   | 4  | 1.001.16            | TOTAL OSS  |
| 99/ 95<br>94/ 90<br>89/ 89<br>89/ 89<br>79/ 75<br>74/ 70<br>69/ 60<br>59/ 55<br>54/ 50<br>49/ 35<br>34/ 30<br>39/ 35<br>34/ 30<br>19/ 19<br>19/ 19<br>170TAL | 11++++   | 1 2 5 9 7 5 5 5 5 1 4 3 | 128<br>422<br>316<br>227<br>178<br>424 | 15    | 16  | 66<br>117<br>107<br>135<br>125 | 2 + 1 1 1 + + | 19<br>15<br>11<br>11<br>6<br>3 | 199<br>230<br>173<br>127<br>104<br>40<br>21<br>14<br>76 | 26<br>124<br>169<br>135<br>131<br>107<br>61<br>21<br>74<br>33 | 67<br>222<br>245<br>237<br>224<br>142<br>49<br>10 | 201<br>327<br>291<br>335<br>256<br>135 | 1 2 2 1 + + + | 44<br>29<br>20<br>20<br>14<br>11<br>18<br>54<br>21<br>20<br>7 | 23723568<br>37268<br>3726524<br>42 | 74<br>62<br>16<br>8<br>4<br>21 | 117<br>145<br>63<br>12<br>4 | 99<br>97<br>85<br>27<br>5 |         | 1<br>1<br>1<br>2<br>2<br>3<br>1<br>+<br>+ | + 22<br>44<br>66<br>99<br>11<br>3<br>4<br>11 | + 22<br>55<br>88<br>13<br>12<br>2<br>1<br>1 + + | +1<br>15<br>12<br>25<br>27<br>10<br>1<br>+ | 17<br>13<br>12<br>2 | 26<br>24<br>62<br>123<br>258<br>448<br>750<br>1272<br>1465<br>1408<br>914<br>427<br>104<br>39<br>20<br>3<br>8767 |

In Table  $\hat{A}$ , occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

OCCURRENCES OF PRECIPITATION AMOUNTS:

DATA NOT AVAILABLE

# PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

D

|                      |   |    |             |          | CEILIN        | G (FEE        | )             |               |              |      |
|----------------------|---|----|-------------|----------|---------------|---------------|---------------|---------------|--------------|------|
| VISHILITY<br>(MILES) | 0 | ** | )35-<br>487 | 52<br>78 | 1990-<br>1990 | 5200-<br>2700 | 3394-<br>4108 | ;500-<br>1200 | 0166<br>9530 | POF. |
| 0 TO 1/8             | 1 | 1  | •           | •        | +             | •             | +             | +             | +            | Ē    |
| 3/16 TO 3/8          |   |    |             | +        | +             | +             | +             | +             | +            | 1    |
| 1/2 10 2/4           | + | +  |             | +        |               | <b>+</b>      | +             | +             | +            | 1    |
| 1 10 21/2            | + | +  | 1           | 1        | 1             | +             | +             | +             | 2            | 4    |
| 3 10 4               | J | +  |             | 1        | 2             | 1             | 1             | 1             | 3            | 9    |
| 7 10 15              |   | +  | +           | 2        | 7             | 6             | 9             | 8             | 26           | 58   |
| 20 10 30             | 1 |    | +           | +        | 1             | 1             | 2             | 3             | 10           | 17   |
| 35 OR AYORE          | ( | ĺ  | i .         |          | +             | +             |               | 1 1           | 6            | 8    |
| TOTAL                | 1 | 2  | 2           | 4        | 10            | 9             | 13            | 13            | 47           | 100  |

SEATTLE, WASHINGTON Seattle-Tacoma Airpo

#### IMIDITY OCCURRENCES:

| 15-24  | MPM |   |      |    | 25 M                                   | P.H.  | AHD    | OVIR                             |   | . 4  |
|--|-----|---|------|----|--|-------|--------|----------------------------------|---|--|
| ş  | Ę   | E | *100 | 1. | r a                                    | B.OT. | 76,79% | mm.                              | 4 | TOTAL ON   |
| 1<br>23<br>57<br>72<br>755<br>60<br>30<br>17<br>12<br>65<br>44 |     | ! | i    |    | 11 11 11 11 11 11 11 11 11 11 11 11 11 | 1     |        | +1<br>15<br>12<br>25<br>27<br>10 | , | 2<br>6<br>24<br>123<br>258<br>448<br>750<br>1272<br>1445<br>1405<br>914<br>427<br>104<br>39<br>20<br>3 |

(10-year total divided by 10). Id to make their sums exactly but less than 0.5.

I AMOUNTS:

ES OF

| * * | 300-<br>7200 | 01/88<br>1188 | 101. |
|-----|--------------|---------------|------|
| -+  | +            | •             | 2    |
| •   | +            | *             | 1    |
| *   | 1            | ,             | 1    |
| 1   | i            | 3             |      |
| •   | 8            | 26<br>10      | 58   |
| ź   | 3            |               | 17   |
| 13  | 13           | 47            | 100  |
| _   |              |               |      |

SEATTLE, WASHINGTON Seattle-Tacoma Airport

B-16

# PERCENTAGE FREQUENCIES B OF WIND DIRECTION AND SPEED:

|          |      |     | HOUR   |            | RYATK<br>M MCts |         |          | SPEED    |            |
|----------|------|-----|--------|------------|-----------------|---------|----------|----------|------------|
| SALCTION | 0.3  | 4.7 | 9 - 12 | 13 - 18    | 10 - 24         | 25 - 31 | 22 - 30  | 39 - 44  | et<br>Ovte |
| N        | +    | 1   | 3      | 3          | +               | +       | +        |          |            |
| NNE      | +    | 1   | 3      | 3          | +               | +       |          |          | Į          |
| NE       | +    | 1   | 3      | 2          | +               | •       | ŀ        |          |            |
| ENE      | +    | 1   | 1      | +          | +               | +       | l        | ĺ        |            |
| E        |      | 1   | 1      | 1          | +               | +       | l        | 1        |            |
| ESE      | +    | 1   | 2      | 1          | +               | +       | +        | 1        | ŀ          |
| SE       | +    | 2   | 3      | 1          | +               | +       | 1        |          | l          |
| SSE      | +    | 1   | 2      | 1          | +               | +       | i        |          |            |
| 5        | +    | 2   |        | 3          | 1               | +       | +        | +        | 1          |
| SSW      | +    | 1   | 3      | 4          | . 5             | 1       | +        | +        |            |
| SW       | +    | 1   |        | 5          | 2               | 1       | +        | +        | ŀ          |
| WSW      | +    | 1   | 2      | 1          | +               | +       | +        | +        | +          |
| W        | +    | 1   | 1      | 1          | +               | +       | +        |          |            |
| AHA      | +    | 1   | 1      | <b>i</b> + | +               | l       | 1        |          |            |
| NW       | +    | 1   | 1      | +          | +               | +       | 1 +      | +        | l          |
| NNW      | +    | +   | 1      | 1          | +               | +       | +        | l        | l          |
| CALM     | 10   | 1   |        |            |                 |         | 1.       |          |            |
| TOTAL    | 1.13 | 116 | 135    | _26_       | 8               | 1 2     | <u> </u> | <u> </u> |            |

#### PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                      |  |   | W  |   |  | <u> </u>  | RE   | ATIV  | E HI  | DIME  | TY.  |
|----------------------|--|---|--|---|--|---|--|---|---|---|--|
| O- 3                 | 47   | 8.<br>10  | 9<br>0-  | 4-<br>12  | 12-<br>24  | 25-<br>A<br>OYER  | 0-<br>29   | 30-<br>47                                   | 50-<br>67   | 7C-<br>79   | 80-<br>89  |
| 33<br>32<br>29<br>27 | 10<br>9<br>9   |   | 14<br>16<br>17<br>17   | 55  | 26   | 2   | *  | 1 1   | 5   | 13<br>11<br>10  | 33<br>31<br>30   |
| 20<br>18<br>16<br>16 | 10<br>11<br>10   | 70<br>71<br>74<br>74  | 20<br>19<br>18<br>17   | 54<br>55<br>55  | 24<br>25<br>26<br>28   | 2   | * * * *  | 1 1 2                                       | 3<br>4<br>7<br>12   | 10<br>14<br>20  | 30<br>30<br>30   |
| 19<br>20<br>21<br>22 | 13<br>13<br>15   | 70<br>67<br>64  | 13<br>11<br>10   | 50<br>48<br>48  | 33<br>37<br>38<br>42   | 4   |  | 3   | 36<br>40<br>39  | 22<br>20<br>17<br>17  | 1 1  |
| 24<br>25<br>26       | 14<br>13<br>14   | 66  | 10   | 46  | 41   | 3   |  | 2 2 2 2 2 2 2                               | 34  | 14  | 1 1 1 1  |
| 31<br>32<br>33       | 14<br>12<br>11   | 50<br>50<br>50<br>50  | 12   | 51<br>50<br>54  | 36   |   | 2 2 2 2  |   | 2 1 1 1   | 1 20<br>1 20<br>2 10  | 2 2 3  |
|                      | 33<br>32<br>29<br>27<br>24<br>20<br>16<br>16<br>17<br>19<br>20<br>21<br>22<br>23<br>24<br>25<br>26<br>27<br>28<br>27<br>28<br>28<br>29<br>29<br>20<br>21<br>20<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21 | 33 10<br>33 10<br>33 10<br>32 9<br>29 9<br>27 10<br>24 10<br>16 10<br>16 10<br>17 10<br>18 11<br>20 13<br>21 15<br>22 14<br>25 13<br>26 14<br>27 14<br>28 13<br>31 14<br>32 13<br>33 11 | 33 10 57<br>32 9 59<br>29 9 61<br>27 10 63<br>24 10 66<br>20 10 70<br>18 11 71<br>16 10 73<br>19 11 70<br>20 13 67<br>21 15 64<br>22 14 64<br>23 14 63<br>24 14 64<br>23 14 63<br>24 14 64<br>25 13 62<br>26 14 60<br>27 14 66<br>32 13 55<br>33 11 55<br>33 11 55<br>33 11 55 | 33 10 57 14<br>32 9 59 16<br>29 9 61 17<br>27 10 63 17<br>24 10 66 19<br>20 10 70 20<br>18 11 71 19<br>16 10 74 18<br>16 9 74 17<br>17 10 73 15<br>19 11 70 13<br>20 13 67 11<br>20 13 67 11<br>20 13 67 12<br>21 15 64 10<br>22 14 64 9<br>25 13 62 10<br>22 14 64 9<br>25 13 62 10<br>26 14 60 11<br>27 14 60 12<br>28 14 58 13<br>31 14 56 13<br>32 13 55 12<br>33 11 55 12<br>33 11 55 12 | 33 10 57 14 53 32 9 59 16 54 29 9 61 17 55 27 10 66 19 55 20 10 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 67 11 70 13 50 20 13 14 50 12 50 31 14 56 13 45 32 13 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 55 12 50 33 11 56 12 50 33 11 56 12 50 33 11 56 12 50 33 11 56 12 50 30 30 30 30 30 30 30 30 30 30 30 30 30 | 33 10 57 14 53 31 32 9 59 16 54 28 29 9 61 17 55 27 27 10 63 17 55 26 24 10 66 19 55 24 24 10 70 20 54 24 18 11 71 19 55 25 16 10 74 18 55 26 16 10 74 18 55 26 16 10 73 15 52 30 17 10 73 15 52 30 17 10 73 15 52 30 19 11 70 13 50 33 10 57 14 83 38 22 14 64 9 46 42 23 14 64 9 46 42 24 14 62 9 46 42 25 13 62 10 46 41 27 14 60 11 47 40 27 14 60 11 47 40 27 14 60 11 47 40 27 14 60 11 47 40 27 14 60 11 47 40 27 14 60 11 47 40 27 14 60 11 47 40 28 14 58 25 25 33 31 15 56 13 49 36 32 13 55 12 50 36 33 11 55 12 50 36 33 11 55 12 50 36 33 11 56 12 52 33 | 33 10 57 14 53 31 2 24 0712 25 3 7 10 3 12 24 0712 25 3 7 10 3 12 24 0712 25 3 10 57 14 53 31 2 24 10 66 19 55 24 2 20 10 66 19 55 24 2 20 10 70 20 54 24 2 18 11 71 19 55 25 16 10 74 18 55 26 2 2 16 9 74 17 53 28 2 17 10 73 15 52 30 3 19 11 70 13 55 33 2 20 13 67 11 48 37 4 2 2 14 69 74 10 48 38 4 2 2 14 69 9 46 41 2 2 14 69 9 46 41 2 2 14 69 9 46 41 2 2 13 62 10 66 11 47 40 2 2 13 62 10 66 11 47 40 2 2 13 62 10 66 11 47 40 2 2 13 62 10 66 41 3 2 2 13 62 10 66 11 3 7 6 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | C- 4- 8- 0- 4- 12- 25- 0- 10 2 12 24 4 2 29 | SCATE 0-10 (M.P.N.)  0-4-8-0-4-12-25-0-30-33-31-2-4-29-69-09-61-17-55-27-2-4-12-24-10-66-19-55-24-2-4-12-20-10-70-20-54-24-2-4-12-10-61-0-74-18-55-26-2-4-12-10-61-0-74-18-55-26-2-4-12-13-13-13-13-13-13-13-13-13-13-13-13-13- | SCATE 0-10  Q. 4- 8- 0- 4- 12- 25- 0- 30- 50- 37 10 2 12 24 | SCATE 0-10  0-4-8-9-10  12-24-0712  33 10 57 14 53 31 2 + 2 9 16 32 9 59 16 54 28 2 + 2 7 13 27 10 66 19 55 24 2 + 1 4 9 16 11 51 02 10 70 12 54 24 10 66 19 55 24 2 + 1 5 10 24 10 66 19 55 24 2 + 1 3 8 18 11 71 9 55 26 2 + 1 5 10 66 10 74 18 55 26 2 + 1 7 14 16 16 10 74 18 55 26 2 + 1 7 14 16 16 10 74 18 55 26 2 + 1 7 14 16 17 10 73 15 52 30 3 + 3 20 22 17 10 73 13 52 30 3 + 5 29 22 17 10 73 13 52 30 3 + 5 29 22 17 10 73 15 52 30 3 + 5 29 22 17 10 73 15 52 30 3 + 5 20 22 17 10 73 15 52 30 3 + 5 20 22 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 13 67 11 48 37 4 1 9 36 20 20 20 13 67 11 48 37 4 1 3 32 33 14 63 8 45 42 4 2 15 39 15 20 1 |

|  |               |   | 0-4 /   | MPH                              |   |   |   | 5-14 M.P.H   |  |  |                                   |  |          |  | 15-24  | MPH                          |  |  |           | 25 M                    | P.H. /          | AND                                     | OAES                                    |   | ر<br>ا  |
|--|---------------|---|---|----------------------------------|---|---|---|--|--|--|-----------------------------------|--|----------|--|--|------------------------------|--|--|-----------|-------------------------|-----------------|---|---|---|---|
| 3 1 8 8  | S R           | ***   | To the same   | Je. 1916                         | we  | 44.Herb   | 105 R                                       | X  | ¥.   | T. R.  | W.F.                              | PO 1804  | N S      | <b>Larce</b>   | ***  | TALES.                       | re a                                   | # 150 P  | 200 X     | E S                     | Web.            | <b>2</b>                                | 4                                       | \$ 100°                                 | 10TH 985.   |
| 77105<br>1/100<br>1/90<br>1/85<br>1/86<br>1/70<br>1/65<br>1/55<br>1/40<br>1/35<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30<br>1/30 | + + + + + + + | 4 8 14 13 12 29 9 9 9 8 7 7 2 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 18<br>22<br>30<br>34<br>36<br>30<br>31<br>35<br>35<br>42<br>31<br>11<br>8<br>4<br>4 | 27 3 5 5 8 4 4 2 8 3 2 1 5 3 + 4 | 1<br>23<br>51<br>51<br>45<br>37<br>30<br>30<br>31<br>19<br>8<br>2 | 53<br>44<br>34<br>30<br>29<br>32<br>195<br>+<br>1 | + 1 3 2 5 7 9 12 12 12 10 6 5 2 1 1 1 1 1 1 | 1<br>12<br>40<br>96<br>96<br>106<br>66<br>78<br>80<br>83<br>81<br>70<br>61<br>62<br>57<br>38<br>27<br>12 | 12<br>63<br>129<br>147<br>152<br>133<br>124<br>136<br>137<br>179<br>2173<br>70<br>32<br>115<br>1 | 22<br>33<br>79<br>65<br>92<br>79<br>67<br>82<br>52<br>52<br>11<br>1<br>+ | 109<br>87<br>66<br>73<br>68<br>57 | #3<br>65<br>83<br>82<br>83<br>72<br>74<br>62<br>45<br>1<br>1<br>+<br>+ | 3322121+ | 3453<br>3472<br>453<br>453<br>154<br>24<br>154<br>24 | 327<br>327<br>327<br>327<br>455<br>690<br>1992<br>1992<br>1992 | 17<br>10<br>6<br>3<br>2<br>+ | 11<br>12<br>12<br>13<br>13<br>18<br>16 | 4<br>6<br>12<br>14<br>19<br>21<br>35<br>22<br>4<br>3 | 1 + + + + | + + 41 422 733565323+ 0 | ++111114343311+ | + + + + + 1 1 + + + + + + + + + + + + + | + 1 1 1 1 1 1 1 + + + + + + + + + + + + | +11133111111111111111111111111111111111 | + 2<br>21<br>79<br>200<br>383<br>615<br>819<br>814<br>755<br>697<br>784<br>846<br>637<br>360<br>202<br>109<br>38<br>11<br>2 |

In Tables A and C, occurrences are for the average year (10-year total divided by 10). Values are rounded to the nearest whole, but not adjusted to make their sums exactly equal to column or row totals. "+" indicates more than 0 but less than 0.5.

## C • OCCURRENCES OF PRECIPITATION AMOUNTS:

D

|                  |   | <del></del> |
|------------------|---|-------------|
|                  | FREQUENCY OF OCCURRENCE FOR LACH HOUR OF THE DAY  | 1 1         |
|                  |   | 1           |
| INTENSITIES      | AM HOUR ENDING AT . PM HOUR ENDING AT   | ╛╬          |
|                  | 1 2 3 4 3 6 7 1 1 9 10 11 60 1 2 1 1 4 1 5 1 6 1 8 1 9 10 11 11 110                                   | WITH        |
|                  |   | - MILEN     |
| TRACE            | 28 27 28 26 31 26 29 32 33 29 30 30 29 32 30 28 27 26 27 28 27 27 29 29                               | 60          |
| O1 =4            | 7 8 4 9 6 7 9 8 8 8 8 7 8 6 6 6 8 8 7 7 9 6 8 8 8   | 12          |
| OF TO UP IN      | 17 16 17 16 15 15 14 15 14 14 14 14 14 14 15 14 14 15 14 14 15 15 15 15 16 15                         |             |
| 16 TO 24 M       | યુકી કી કી કી કો હું યું હું કી હો હતું કી લો છે. જે હો કો લો હો કે ક                                 | 27          |
| 23 TO 48 W       |   | 1 31        |
| 9J TO 99 HI      | ુન નું નું મું મું નું નું નું નું મું મું નું નું નું નું નું નું નું નું નું ન                      | 20          |
| 100 10 199 94    |   | 9           |
| RIVO DEA SE CO S |   | li          |
| TOTAL            | <u>571 561 581 571 581 561 561 691 691 591 561 561 551 571 571 551 521 521 551 551 551 571 591 56</u> | 182         |

PERCENTAGE FREQUENCIES OF CEILING-VISIBILITY:

|                     |     |      |            |             | CEILIN     | G (FEE)      | ,            |               |              |       |
|---------------------|-----|------|------------|-------------|------------|--------------|--------------|---------------|--------------|-------|
| VISIBRITY<br>(MHES) | ٥   | 196- | 308<br>408 | 109.<br>108 | 370<br>166 | 2008<br>2908 | 3000<br>4708 | 3000-<br>1300 | 0vts<br>1330 | 101   |
| 0 10 1/8            | +   | +    | +          | +           |            |              | +            |               | +            | +     |
| 3/14 10 3/8         | +   | +    | +          | +           | +          | +            | +            | <b>.</b> +    |              | +     |
| 1/2 10 3/4          | +   | +    | +          | +           | +          | +            | +            | +             | +            | 2     |
| 1 10 21/2           | 1 1 | +    | 1          | 3           | 1          | +            | +            | 1             | 3            | 9     |
| 3 10 6              | l   | +    | +          | 2           | 3          | 1            | 2            | 2             | 12           | 23    |
| 7 10 15             | +   |      | +          |             | - 2        | 2            | 6            | 7             | 49           | 66    |
| 20 10 30            |     |      |            |             |            | _            | _            |               |              | • • • |
| 33 OR MORE          | 1   |      |            |             |            |              | 1            | l             | i 1          |       |
| TOTAL               | +   | 1    | 1          | 6           | 6          | 4            | 8            | 10            | 65           | 100   |

|          |     |     | HOUR |       | ERVATION   |            | CIND     | SPEED      |             |      | -            |
|----------|-----|-----|------|-------|------------|------------|----------|------------|-------------|------|--------------|
| DMKL.IQM |     |     |      | • •   |            |            | _        |            | •           |      | . S/100      |
|          | • > | 4 / | . 13 | 13 18 | 19 24 2*   | 11 32      | 10       | » 4°       | e?<br>·rvii | *CFA |              |
| N        | · . | 1   | ż    | 1     | + .        | •          | •        | + ;        | ·;          | 4    | 10.2         |
| NNE      | +   | 2   | 3    | 2     | +          | •          | +        | + '        | •           | 8    | 10.4         |
| NE       | 1   | 2   | 2    | 2     | <b>.</b>   | •          | +        | <b>+</b> ; | ì           | 6    | 9.6          |
| ENE      | +   | 1   | 1    | 1     | <b>+</b> ; | +          | +        | •          |             | 4    | 9.7          |
| Ε        | 1:  | 1   | 1    | •     | + 1        | <b>+</b> . | +        | <b>+</b> 1 | i           | 4    | 7.6          |
| ESE      | •   | 1   | ٠2   | 1     | <b>+</b> . | <b>4</b> 1 | +        | +,         |             | 4    | : 8.9        |
| SE       | • • | 1   | 1    | 1     | <b>♦</b> ` | + :        |          | . 1        |             | 2    | . 8.8        |
| SSE      | +1  | 1   | 2    | 1     | <b>*</b> : | + ;        | +        | : :        |             | 4    | 9.1          |
| 5        | 1 4 | 1   | 1    | 1     | • ·        | + !        | +        | !          | !           | 4    | 8.0          |
| SSW      | 1   | 3   | 3    | 2     | <b>+</b> ` | + ,        | +        | +          |             | 9    | 8.9          |
| S₩       | 2:  | 4   | 3    | 1     | +1         | <b>+</b> , | 4        | i          | i           | 10   | 7.5          |
| WSW      | 1   | 3   | 3    | 2     | + :        | •          | +        | ; !        | . !         | 8    | 9.1          |
| W        | 1   | 2   | 2    | 2     | <b>*</b> . | •          | +        | +          |             | 7    | 10.1         |
| WNW      | +   | 1   | 3    | 3     | 1 '        | <b>+</b> ] | +        | +          |             | 9    | 12.4         |
| NW       | +   | 1   | 2    | •     | 1 .        | * .        | 4        | . +        |             | 8    | 13.0         |
| NNW      | +   | 1   | 2    | 3     | 1          | + 1        | •        | ;          |             |      | 112.8        |
| CALM     | 1   |     | • -  | ,     | 1          | i          |          |            |             | 1    | 1            |
| TOTAL    | 11  | _25 | 34   | . 24  | 5          | نند        | <u>*</u> | <u>:</u>   | <u></u> *   | 100  | j <u>9.8</u> |

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# PERCENTAGE FREQUENCIES OF SKY COVER, WIND, AND RELATIVE HUMIDITY:

|                   |         | LE O |          | W       | IND      | SPEE      | D                | RE       | LATIV     | E H       | U#110     | ITY       | ( <del>~)</del><br>    |
|-------------------|---------|------|----------|---------|----------|-----------|------------------|----------|-----------|-----------|-----------|-----------|------------------------|
| HOUR<br>OF<br>DAY | с.<br>3 | 4-7  | 8-<br>10 | о.<br>З | 4-<br>12 | 13-<br>24 | 25-<br>&<br>GVER | 0.<br>29 | 39-<br>49 | 50-<br>69 | 70-<br>19 | 80-<br>89 | <del>5</del> 0.<br>100 |
| 00                | 48      | 8    | 44       | 16      | 65       | 18        | 1                | <br>+    | 8         | 35        | 21        | 19        | 17                     |
| 01                | 48      |      |          | 17      |          |           |                  |          |           |           |           |           |                        |
| 20                | 48      |      | 43       | 20      | 62       | 18        |                  | *        | 5         | 32        |           |           |                        |
| 03                | 48      | 8    |          |         | 62       |           | +                |          | 4         | 30        |           |           |                        |
| 04                | 46      | 10   |          | 20      | 63       |           | 4                | +        | 3         | 28        |           |           |                        |
| 05                | 42      | 11   | 46       | 19      | 63       | 17        | 1                |          | 1 3       |           |           |           |                        |
| 06                | 38      | 11   | 50       | 18      | 63       | 18        | 1                | l        | 3         | 30        |           |           |                        |
| 07                | 36      | 13   | 52       | 14      | 63       |           | , ī              |          | 5         | 36        |           |           |                        |
| 80                | 36      |      |          |         | 60       | 28        | 1                |          | 11        | 41        | 17        | 16        |                        |
| 09                | 37      | 14   |          |         | 58       | 33        | ! 1              | 1        | 20        | 43        | 14        |           |                        |
| 10                | 35      | 15   | . 50     | 7       | 56       | 36        | 2                | 1        | 29        |           |           |           |                        |
| 11                | 33      | 17   | : 50     | 6.      |          | 39        | 2                | 2        | ' 38      |           |           |           |                        |
| 12                | 31      | 18   | 51       | 5       | 51       | 42        | . 2              | 4        | 43        |           |           |           |                        |
| 13                | 31      |      | 52       | 4       | 48       |           | 2                | 6        | 45        |           |           |           |                        |
| 14                | 30      |      | 51       |         | 48       | 47        |                  | 7        | 46        | 27        | 7         | 6         |                        |
| 15                | 31      | 19   |          |         |          | 45        | 3                | 7        | 44        | 27        | 8         | . 7       |                        |
| 16                | 33      |      |          |         |          |           | : 2              | 7        | 41        | 29        |           | ' 7       |                        |
| 17                | 36      |      |          | •       | 57       | 38        | . 1              | 15       | . 36      | 33        | 10        |           |                        |
| 18                | 39      |      |          |         | 62       | . 31      |                  | 3        |           | 37        | - 12      | 10        | 9                      |
| 19                | 41      |      |          | 8       | 65       |           | 1                | 2        | 23        | : 39      |           |           |                        |
| 20                | 43      |      |          |         |          |           |                  | i        |           | 40        | 16        | 13        |                        |
| 21                | 45      | 11   |          |         | 64       |           | 1 1              | 1        |           |           | 18        | 15        |                        |
| 22                | 46      |      |          | 12      | 65       |           |                  | +        |           | 39        | 19        | . 17      | 14                     |
| 23                | 47      |      |          | 14      | 64       |           | 1                | +        | ; 9       | : 38      | 19        |           | 16                     |
| AVG               | 40      | 13   | 47       | 11      | 59       | 29        | <b>i 1</b>       | 2        | 121       | 34,       | 15        | 14        | : 14                   |
|                   | i :     |      | : 1      |         |          | i         | i                | İ        | i         |           | 1         | •         |                        |

NEWARK, N Newark Ai

| _         |              | Mobile, Alabama  |  |
|-----------|--------------|--|--|
| _         | STATION HO   | OCCURRENCES OF PRECIPITATION ANDUNTS:  | NO. YEARS  |
| -         | 101-5478 ANN | FREQUENCY OF OCCURRENCES FOR EACH HOUR OF THE DAY  | <u> </u>   |
| _         | INTENSITIES  | - 1 -2 -3 -4 -5 -6 -7 -8 -9 10 11 12   1 - 2 -3 - 5 -6 -7 -8 -9 10                                     | ICAYS  |
|           |              |  |  |
|           |              |  |  |
|           |              | -3 - 4 - 2 - 3 - 2 - 3 - 4 - 4 - 4 - 5 - 4 - 5 - 4 - 5 - 4 - 5 - 5                                     |  |
|           |              | <sup>7</sup> <sup>7</sup> <sup>7</sup> <sup>7</sup> <sup>7</sup> <sup>7</sup> <sup>7</sup> <sup></sup> |  |
|           |              |  |  |
|           |              |  |  |
| <b>CC</b> |              |  |  |
| -18       |              |  |  |
|           | TOTAL        | 17 16 15 15 16 14 16 16 18 20 18 19 23 29 29 27 26 24 26 21 20 15                                      |  |
|           |              |  |  |
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| STATION MO.  |  |
|--|--|
| INTERSITES   A.M. HOUR ENDING AT   DAYS   DA | מא צפודו   |
| 1 2 3 4 5 6 7 8 9 10 11 121 1 2 3 4 5 6 7 8 9 10 11 121 NTH  .01 II.   | 7433 ANN   |
| .07 TL .07 IN. 19 21 27 28 27 21 21 27 25 17 19 22 20 21 20 24 24 26 23 22 20 18 20 35 55 .10 TA .2. IN. 2 3 2 2 3 4 4 4 2 3 2 3 3 3 3 2 3 3 4 3 2 4 3 5 43 .20 TA .47 IN. * * * * * * * * * * * * * * * * * * *   | NTERSITES   1 1  |
| .10 Th .2+ IN. 2 3 2 2 3 4 4 4 2 3 2 3 3 3 3 2 3 3 4 3 2 4 3 5 43  .20 Th .4+ IN. * * * * * * * * * * * * * * * * * * *  | 1 1 1  |
| .20 TJ .49 IN. * * * * * * * * * * * * * * * * * * *   | 17 TU +09 TH+ 19   |
| .50 TJ .77 IN. *  1.JO TJ 1.99 IN.  2.00 II. A.D GVER  TOTAL 41 49 58 62 50 39 36 60 34 30 31 34 36 38 41 41 48 52 52 41 34 36 36 59 156   | 10 TO .2+ IN. 2  |
| 1. JO T.J 1.99 IN.  2. CO I I. A.D GVER  TOTAL 41 49 58 62 50 39 36 40 34 30 31 34 36 38 41 41 48 52 52 41 84 36 36 \$9 156  | * •NI 64. LT ca  |
| 2.50 11. A-7 CVER TOTAL 41 49 58 62 50 39 36 40 34 30 31 34 36 38 41 41 48 52 52 41 84 36 39 39 6  | 10 Ta .77 IN.  |
| TOTAL 41 49 58 62 50 39 36 40 34 30 31 34 36 38 41 41 48 52 52 41 84 36 36 59 156  | 10 TJ 1.99 IN.   |
|  | O II. A-D GVER   |
| B-12   | rat 41   |
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|  | do Nacional de parametro de Marina de Adminis de de Compaño de Com |

# APPENDIX B, EXHIBIT B

FREQUENCY OF ANNUAL WEATHER OCCURRENCES BY WORK SHIFT

# Location Portland, ME

|                                    |                                  |                                  | Dry                           | /bulb Te                      | nperature                        | •                    |                             |                      |
|------------------------------------|----------------------------------|----------------------------------|-------------------------------|-------------------------------|----------------------------------|----------------------|-----------------------------|----------------------|
| Shift<br>Day<br>Afternoon<br>Night | <5<br>.016<br>.013<br>.008       | .074<br>.069<br>.057             | 20-29<br>.118<br>.118<br>.108 | 30-39<br>.171<br>.192<br>.207 | 40-79<br>.579<br>.586<br>.611    | .039<br>.022<br>.009 | 90-99<br>.003<br>.001<br>.0 | .0<br>.0<br>.0       |
|                                    |                                  | ******                           |                               | ective T                      | emperatur                        | ·e                   | •                           | ···                  |
| Shift<br>Day<br>Afternoon<br>Night | <5<br>.069<br>.057<br>.044       | 5-19<br>.165<br>.161<br>.147     | 20-29<br>.160<br>.175<br>.181 | 30-39<br>.156<br>.168<br>.183 | .40-79<br>.408<br>.416<br>.436   | .039<br>.022<br>.009 | .003<br>.001<br>.0          | .0<br>.0<br>.0       |
|                                    | <u></u>                          | lind Spee                        | e <b>d</b>                    |                               |                                  | C10                  | oud Cover                   | •                    |
| Shift<br>Day<br>Afternoon<br>Night | <13<br>.5813<br>.8438<br>.8375   | 13-24<br>.3975<br>.2212<br>.2571 | .0213<br>.0125<br>.01         | •                             | <u>Shift</u><br>Day<br>Afternoon |                      | Sunny<br>.4200<br>.1837     |                      |
|                                    |                                  | Precipit                         | ation                         |                               | ٠                                | 1                    | Fog                         |                      |
| Shift<br>Day<br>Afternoon<br>Night | None or<br>Trace<br>.916<br>.913 | .01<br>.022<br>.027              | .0209<br>.046<br>.048         | .1+<br>.016                   |                                  |                      | y <1/16 N                   | ••                   |
| Might                              | .898                             | .031                             | .053                          | .018                          |                                  |                      |                             |                      |
|                                    | Rela<br>Humi                     |                                  |                               |                               | Correc<br>Temperatu              |                      | Effective Painters          |                      |
| Shift<br>Day                       |                                  | 90-100                           |                               | -                             | < <u>5</u> 5-                    | <u>19 20</u>         | 0-29 3                      | 0-39                 |
| Afternoon<br>Night                 | .835<br>.700<br>.510             | .165<br>.300<br>.490             |                               |                               | .057                             | 138                  | .050<br>.081<br>.086        | .013<br>.018<br>.022 |

# Location Boston

# FREQUENCY OF ANNUAL OCCURRENCES

Drybulb Temperature

|                     |                  |                  |                  | Julia          |                       |                |          |              |
|---------------------|------------------|------------------|------------------|----------------|-----------------------|----------------|----------|--------------|
| Shift               | <5               | 5-19             | 20-29            | 30-39          | 40-79                 | 80-89          | 90-99    | 100+         |
| Day                 | 0.002            | 0.036            | 0.089            | 0.168          | 0.641                 | 0.055          | 0.009    | 0.0          |
| Afternoon           | 0.002<br>0.001   | 0.030            | 0.080            | 0.174          | 0.664                 | 0.046          | 0.005    | 0.0          |
| Night               | 0.0              | 0.019            | 0.064            | 0.179          | 0.706                 | 0.028          | 0.003    | 0.0          |
|                     |                  |                  |                  |                | •                     |                |          |              |
|                     |                  |                  |                  | •              | ,                     |                |          |              |
|                     |                  |                  |                  | •              |                       |                |          |              |
|                     |                  |                  | Effe             | ctive To       | emperatur             | e              |          |              |
| Shift               | <5_              | <u>5-19</u>      | 20-29            | 30-39          | 40-79                 | 80-89          | 90-99    | 100+         |
| Day                 | 0.063            | 0.163            | 0.153            | 0.150          | 0.407                 | 0.055          | 0.009    | 0.0          |
| Afternoon<br>Night  | 0.052            | 0.146            | 0.156            | 0.163          |                       | 0.046          | 0.005    | 0.0          |
| Might               | 0.037            | 0.131            | 0.165            | 0.173          |                       | 0.028          | 0.003    | 0.0          |
|                     |                  |                  |                  |                |                       |                |          |              |
|                     |                  |                  |                  |                |                       |                |          |              |
|                     |                  |                  |                  |                |                       |                |          |              |
|                     | W                | ind Spee         | ed               |                |                       | Clo            | oud Cove | r            |
| Shift               | <13              | 13-24            | 25+              |                | Shift                 |                | Sunny    |              |
| Day                 |                  |                  | 0.000            |                | Day                   | . 0            | .4150    |              |
| Afternoon           | 0.3925<br>0.4838 | 0.5413<br>0.4750 | 0.0688<br>0.0450 |                | Afternoor             |                | .1812    |              |
| Night               | 0.5838           | 0.3800           | 0.0325           | •              |                       | •              |          |              |
|                     |                  |                  |                  |                | •                     |                |          |              |
|                     |                  |                  |                  |                |                       |                |          |              |
|                     |                  | Dunninii         |                  |                |                       | 1              | Fog      |              |
|                     |                  | Precipit         | acton            | <del></del>    |                       |                |          | 1127 - 1     |
| CLICA               | None or          |                  | n2 na            | .1+            | (A.                   | isibilit;<br>· |          | -            |
| <u>Shift</u><br>Day | Trace            | .01              | .0209            |                |                       | Average        |          | .01          |
| Afternoon           | 0.912            | 0.027            | 0.043            | 0.018          |                       |                |          |              |
| Night               | 0.912<br>0.903   | 0.027<br>0.031   | 0.045<br>0.046   | 0.016<br>0.020 |                       |                |          |              |
|                     | 0.503            | 0.031            |                  |                |                       |                |          |              |
|                     |                  |                  |                  |                |                       |                |          |              |
|                     |                  |                  |                  |                | •                     |                |          | •            |
|                     |                  | tive             |                  |                | Corre                 | ction of       |          |              |
|                     |                  | dity_            |                  | -              |                       |                |          |              |
| Shift               | 90               | 90-100           |                  | -              | <u>&lt;5</u> <u>5</u> | <u>-19</u> 2   | 0-29     | <u>30-39</u> |
| Day<br>Afternoon    | 0.8900           | 0.110            | 0                | C              | .063 (                | 0.101          | 0.040    | 0.003        |
| Night               | 0.8500           | 0.150            | 0                | 0              | .052                  | 0.091 (        | 0.041    | 0.003        |
| •                   | 0.7800           | 0.220            | 0                | C              | 0.037 (               | 0.076          | 0.041    | 0.005        |
|                     |                  |                  |                  |                | -                     |                |          |              |

| ]      |                    |                            | Location                   | New '                      | York                    |                         |                         |                     |                         |
|--------|--------------------|----------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|---------------------|-------------------------|
| }      |                    | FRE                        | QUENCY OF                  | ANNUAL                     | OCCURREN                | CES                     |                         |                     |                         |
| _      |                    |                            | <del></del>                | Dr                         | ybulb Tei               | mperatur                | e                       |                     |                         |
| Ĺ      | Shift<br>Day       | <u>&lt;5</u>               | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                   | <u>80-89</u>            | 90-99               | 100+                    |
| ]      | Afternoon<br>Night | 0.0<br>0.0<br>0.0          | 0.007<br>0.005<br>0.003    | 0.072<br>0.061<br>0.047    | 0.168<br>0.170<br>0.169 | 0.719                   |                         | 0.004               | 0.0<br>0.0<br>0.0       |
| ]      |                    | -                          |                            | Eff                        | ective To               | emperatu                | re                      |                     |                         |
|        | Shift<br>Day       | <u>&lt;5</u>               | <u>5-19</u>                | <u>20-29</u>               | <u>30-39</u>            | 40-79                   | 80-89                   | 90-99               | 100+                    |
| ]      | Afternoon<br>Night | 0.028<br>0.023<br>0.016    | 0.121<br>0.108<br>0.095    | 0.154<br>0.162<br>0.156    | 0.161<br>0.165<br>0.172 |                         | 0.053<br>0.042<br>0.029 | 0.003               | 0.0<br>0.0<br>0.0       |
|        |                    |                            |                            |                            |                         |                         |                         |                     |                         |
|        | Shift              |                            | lind Speed                 |                            |                         | *L 2 C1                 | <u></u>                 | oud Cover           | <del></del>             |
| 1      | Day                | <13                        | 13-24                      | 25+                        | Ī                       | Shift<br>Day            |                         | Sunny               |                         |
|        | Afternoon<br>Night | 0.4763<br>0.5713<br>0.7059 | 0.4800<br>0.4000<br>0.2738 | 0.0450<br>0.0313<br>0.0200 | F                       | \fternoor               | 1                       | 0.5612<br>0.1912    |                         |
|        |                    |                            | Precipita                  | ution.                     |                         |                         |                         | •                   |                         |
| ļ<br>1 |                    | None or                    |                            | 161011                     |                         | - (vi                   |                         | og<br>/ <1/16 M     | 57.1                    |
| i      | Shift<br>Day       | Trace                      | .01                        | .0209                      | <u>.1+</u>              | (**                     | 3(0)1110                | / <1/10 P           | 116)                    |
|        | Afternoon<br>Night | 0.926<br>0.925<br>0.920    | 0.020<br>0.021<br>0.021    | 0.039<br>0.040<br>0.042    | 0.015<br>0.014<br>0.017 |                         | Average                 | 0.01                | -                       |
|        |                    | Relat<br>Humic             |                            |                            |                         | Correc<br>emperatu      | tion of<br>re for P     | Effectiv<br>ainters | e<br>Only               |
|        | Shift<br>Day       | 90                         | 90-100                     |                            |                         | <u>&lt;5</u> <u>5</u> - | 19 20                   | <u>3 - 29</u>       | 0-39                    |
| `      | Afternoon<br>Night | 0.8862<br>0.8362<br>0.7325 | 0.1138<br>0.1638<br>0.2675 |                            | C                       | .023                    | .067 (                  | .040                | 0.006<br>0.006<br>0.006 |

# Location Philadelphia

|                           | <del> </del>               |                            | Dry                        | bulb Te                 | mperature               | <b>:</b>                |                         |  |
|---------------------------|----------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|-------------------------|--|
| Shift<br>Day              | <u> &lt;5</u>              | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                   | <u>80-89</u>            | <u>90-99</u>            | 100+                                   |
| Afternoon<br>Night        | 0.0<br>0.0<br>0.0          | 0.021<br>0.017<br>0.013    | 0.070<br>0.064<br>0.048    | 0.167<br>0.172<br>0.171 | 0.659                   | 0.097<br>0.077<br>0.046 | 0.017<br>0.011<br>0.004 | 0.000<br>0.0<br>0.0                    |
| •                         |                            |                            | Effe                       | ctive ]                 | [emperatur              | ·e                      |                         | ······································ |
| Shift<br>Day              | <u>&lt;5</u>               | <u>5-19</u>                | 20-29                      | <u>30-39</u>            | <u>40-79</u>            | 80-89                   | 90-99                   | 100+                                   |
| Afternoon<br>Night        | 0.019<br>0.016<br>0.011    | 0.105<br>0.096<br>0.071    | 0.144<br>0.150<br>0.145    | 0.150<br>0.158<br>0.168 | 0.493                   | 0.093<br>0.077<br>0.046 | 0.016<br>0.011<br>0.004 | 0.000<br>0.0<br>0.0                    |
|                           | W:                         | ind Spee                   | <u>d</u>                   |                         |                         | C1c                     | oud Cove                | <u>r</u>                               |
| Shift<br>Day              | <13                        | 13-24                      | 25+                        |                         | Shift<br>Day            |                         | Sunny                   |  |
| Afternoon<br>Night        | 0.6188<br>0.7425<br>0.8188 | 0.3613<br>0.2475<br>0.1788 | 0.0175<br>0.0100<br>0.0063 |                         | Afternoor               | 1                       | 0.4275<br>0.1925        |  |
|                           |                            | Precipit                   | ation                      |                         | -                       |                         | Fog                     |  |
| Shift                     | None or<br>Trace           | .01                        | .0209                      | .1+                     | (Vi                     | sibility                | y <1/16                 | Mile)                                  |
| Day<br>Afternoon<br>Night | 0.935<br>0.929<br>0.923    | 0.018<br>0.020<br>0.020    | 0.036<br>0.037<br>0.039    | 0.011<br>0.014<br>0.018 |                         | Average                 | 9 0.0                   | 01                                     |
|                           | Relat<br>Humid             |                            |                            | -                       | Correc<br>Temperatu     | tion of<br>re for I     | Effecti<br>Painters     | ve<br>Only                             |
| Shift<br>Day              |                            | 30-100                     |                            | -                       | <u>&lt;5</u> <u>5</u> - | 19 20                   | 0-29                    | 30-39                                  |
| Afternoon<br>Night        | 0.9062<br>0.8800<br>0.7137 | 0.0938<br>0.1200<br>0.2863 |                            | İ                       | 0.016 0                 | .073 0                  | .055                    | 0.012<br>0.015<br>0.019                |

# Location Baltimore

|                    |                 |                | Dry            | bulb Te      | emperature   | 9            |                 |  |
|--------------------|-----------------|----------------|----------------|--------------|--------------|--------------|-----------------|--|
| Shift              | <5              | 5-19           | 20-29          | 30-39        | 40-79        | 80-89        | 90-99           | 100+   |
| Day<br>Afternoon   | .0              | .017           | .065           | .163         | .622         | .107         | .025            | .0   |
| Night              | .0              | .016           | .061           | .160         | .660         | .087         | .017            | .0   |
|                    | .0              | .015           | .055           | .166         | .714         | .048         | .004            | .0   |
|                    |                 |                |                |              | ,            | f            |                 |  |
|                    |                 |                | Effe           | ctive        | Temperatu    | re           |                 |  |
| Shift              | <5_             | <u>5-19</u>    | 20-29          | <u>30-39</u> | 40-79        | <u>80-89</u> | 90-99           | 100+   |
| Day<br>Afternoon   | .023            | .110           | .157           | .163         | .415         | .107         | .025            | 9  |
| Night              | .016<br>.012    | .093<br>.078   | .151<br>.144   | .162         | .475<br>.547 | .087<br>.048 | .017<br>.004    | 0<br>0   |
|                    |                 |                | •              |              |              |              |                 |  |
|                    | 1               | Wind Spee      | ıd             |              |              | C1           | oud Cove        | r  |
| Shift              | <13             | 13-24          | 25+            |              | Shift        |              | Sunny           | <u>•                                      </u> |
| Day                |                 |                |                |              | Day          |              |                 |  |
| Afternoon<br>Night | .5900<br>.7136  | .3813<br>.2688 | .0300<br>.0138 |              | Afternoo     | n            | 4688<br>.2062   |  |
| 5                  | .8025           | .1888          | .01            | •            |              |              |                 |  |
|                    |                 |                |                |              |              |              |                 |  |
|                    | <del></del>     | Precipit       | ation          | <del></del>  |              |              | Fog<br>ty <1/16 | Wile!  |
| Shift              | None o<br>Trace |                | .0209          | .1+          | ()           | 15101111     | ty <1/10        | milej  |
| Day                |                 |                |                |              |              | Avera        | ige •           | 01   |
| Afternoon<br>Night | .933<br>.927    |                | .035<br>.037   |              |              |              |                 |  |
| <b>3</b>           | .929            |                | .038           |              |              |              |                 |  |
|                    | Re1             | a+*.e .        |                |              | Corre        | ction o      | f Effecti       | ive  |
|                    | Hum             | idity          |                |              |              | ture for     | Painters        | 5 Only   |
| Shift              | 90              | 90-100         |                |              | <u>&lt;5</u> | 5-19         | 20-29           | <u>30-39</u>                                   |
| Day<br>Afternoon   | .8912           | .1088          |                |              |              | .074         | .051            | .009   |
| Night              | .8575<br>.6837  | .1425<br>.3163 |                |              |              | .068<br>.061 | .056<br>.058    | .011<br>.015                                   |

# Location Norfolk, VA.

|                                    |                         |                         | Dry                           | /bulb Ter                   | mperatur             | <del>2</del>         |                      |                            |
|------------------------------------|-------------------------|-------------------------|-------------------------------|-----------------------------|----------------------|----------------------|----------------------|----------------------------|
| Shift<br>Day                       | <5                      | 5-19                    | 20-29                         | 30-39                       | 40-79                | 80-89                | 90-99                | 100+                       |
| Afternoon<br>Night                 | .0<br>.0<br>.0          | .003<br>.001<br>0       | .033<br>.026<br>.019          | .111<br>.106<br>.100        | .704<br>.752<br>.811 | .121<br>.097<br>.063 | .028<br>.018<br>.008 | .0<br>.0<br>.0             |
|                                    |                         | -                       | Effe                          | ective Te                   | emperatuı            | re                   |                      |                            |
| Shift<br>Day                       | <u>&lt;5</u>            | 5-19                    | 20-29                         | <u>30-39</u>                | 40-79                | 80-89                | 90-99                | 100+                       |
| Afternoon<br>Night                 | .007<br>.004<br>.002    | .060<br>.049<br>.036    | .112<br>.104<br>.092          | .158<br>.155<br>.155        | .514<br>.573<br>.645 | .121<br>.097<br>.063 | .028<br>.018<br>.008 | .0<br>.0                   |
| Shift                              | <u> </u><br>_<13        | lind Spee               | d                             |                             | <u>Shift</u>         | Clo                  | oud Cover<br>Sunny   | ·                          |
| Day<br>Afternoon<br>Night          | .5550<br>.7250<br>.7313 | .4263<br>.2625<br>.2588 | .0175<br>.0125<br>.0100       |                             | Day<br>Afternoor     | 1                    | .4700<br>.1987       |                            |
|                                    | None or                 | <u>Precipit</u>         | ation                         |                             |                      | F<br>isibility       | og<br>/ <1/16 N      | lile)                      |
| Shift<br>Day<br>Afternoon<br>Night | .935<br>.927<br>.032    | .017<br>.020<br>.018    | .0209<br>.033<br>.035<br>.037 | .1+<br>.015<br>.018<br>.013 | •                    | Average              |                      | <b>.</b> ,                 |
| Shift                              |                         | tive<br>dity<br>90-100  |                               | _1                          | Temperatu            |                      | ainters              | re<br><u>Only</u><br>10-39 |
| Day<br>Afternoon<br>Night          | .9375<br>.8375<br>.6612 | .0825<br>.1625<br>.3388 |                               | •                           | 007 .0               | 039<br>030           | .028<br>.027<br>.024 | .007<br>.008<br>.011       |

Location Mobile

|                           | Drybulb Temperature     |                            |                            |                         |                         |                         |                                |                         |  |  |
|---------------------------|-------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|--------------------------------|-------------------------|--|--|
| Shift                     | <5                      | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                   | 80-89                   | 90-99                          | 100+                    |  |  |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0       | 0.000<br>0.0<br>0.0        | 0.008<br>0.006<br>0.004    | 0.043<br>0.037<br>0.028 | 0.689<br>0.789<br>0.874 | 0.210<br>0.145<br>0.086 | 0.049<br>0.023<br>0.008        | 0.000<br>0.0<br>0.0     |  |  |
|                           |                         | -,                         | Eff                        | ective 1                | Temperati               | ure                     |                                |                         |  |  |
| Shift<br>Day              | <u>&lt;5</u>            | <u>5-19</u>                | 20-29                      | <u>30-39</u>            | <u>40-79</u>            | <u>80-89</u>            | 90-99                          | 100+                    |  |  |
| Afternoon<br>Night        | 0.001<br>0.0<br>0.0     | 0.022<br>0.015<br>0.009    | 0.059<br>0.048<br>0.036    | 0.117<br>0.101<br>0.082 | 0.541<br>0.667<br>0.779 | 0.210<br>0.145<br>0.086 | 0.049<br>0.023<br>0.008        | 0.000<br>0.0<br>C.0     |  |  |
|                           |                         | lind Spee                  |                            |                         |                         | <u>C</u>                | loud Cove                      | er                      |  |  |
| Shift<br>Day              | <u>&lt;13</u>           | 13-24                      | 25+                        |                         | Shift<br>Day            |                         | Sunny                          |                         |  |  |
| Afternoon<br>Night        | 0.7775                  | 0.4088<br>0.2163<br>0.1638 | 0.0175<br>0.0050<br>0.0063 |                         | Afternoo                |                         | 0.4862<br>0.2087               |                         |  |  |
|                           |                         | Precipit                   | ation                      |                         |                         |                         | Fog                            | *******                 |  |  |
| Shift                     | None or<br>Trace        | <u>.01</u>                 | .0209                      | .1+                     | (1                      | Visibili                | ty <1/16                       | Mile)                   |  |  |
| Day<br>Afternoon<br>Night | 0.941<br>0.938<br>0.957 | 0.011<br>0.013<br>0.010    | 0.026<br>0.028<br>0.020    | 0.022<br>0.021<br>0.013 |                         | Average 0.01            |                                |                         |  |  |
| Shift                     |                         | tive<br>dity<br>90-100     |                            |                         | Tempera                 | ture for                | f Effecti<br>Painters<br>20-29 |                         |  |  |
| Day<br>Afternoon          | 0.9087                  | 0.091                      | 3                          | •                       |                         |                         |                                |                         |  |  |
| Night                     | 0.7187<br>0.4650        | 0.281<br>0.535             | 3                          |                         | 0.001<br>0.0<br>0.0     | 0.012<br>0.007<br>0.004 | 0.011<br>0.010<br>0.006        | 0.001<br>0.001<br>0.001 |  |  |

# Location New Orleans

|                           | Drybulb Temperature     |                         |                        |                      |                       |                      |                      |                      |  |
|---------------------------|-------------------------|-------------------------|------------------------|----------------------|-----------------------|----------------------|----------------------|----------------------|--|
| Shift                     | <5                      | <u>5-19</u>             | 20-29                  | 30-39                | 40-79                 | 80-89                | 90-99                | 100+                 |  |
| Day<br>Afternoon<br>Night | .0<br>.0<br>.0          | .0<br>.0<br>.0          | .001<br>.0<br>.0       | .023<br>.020<br>.015 | .682<br>.758<br>.870  | .245<br>.197<br>.106 | .048<br>.026<br>.008 | .0<br>.0             |  |
|                           | Effective Temperature   |                         |                        |                      |                       |                      |                      |                      |  |
| Shift<br>Day              | <u>&lt;5</u>            | <u>5-19</u>             | 20-29                  | 30-39                | <u>40-79</u>          | 80-89                | 90-99                | <u>100+</u>          |  |
| Afternoon<br>Night        | .0<br>.0                | .012<br>.009<br>.005    | .043<br>.031<br>.019   | .090<br>.077<br>.058 | .560<br>.662<br>.804  | .246<br>.197<br>.106 | .048<br>.026<br>.008 | .0<br>.0<br>.0       |  |
|                           |                         | Wind Spee               | ed                     |                      |                       | Clo                  | oud Cover            | ·                    |  |
| Shift<br>Day              | <13                     | 13-24                   | 25+                    |                      | Shift<br>Day          |                      | Sunny                |                      |  |
| Afternoon<br>Night        | .6025<br>.8038<br>.8425 | .3825<br>.1888<br>.1475 | .015<br>.0001<br>.0001 |                      | Afternoon .6150 .2075 |                      |                      |                      |  |
|                           |                         | Precipit                | ation                  |                      |                       |                      | og                   |                      |  |
| Shift                     | None o<br>Trace         |                         | .0209                  | .1+                  | {V                    | isibility            |                      | •                    |  |
| Day<br>Afternoon<br>Night | .938<br>.946<br>.960    | .012<br>.013<br>.010    | .028<br>.025<br>.017   | .022<br>.016<br>.013 |                       | Avera                | ge .0                | 1                    |  |
|                           | Hum:                    | ative<br>idity          |                        |                      | Temperati             |                      |                      |                      |  |
| Shift<br>Day              | 90                      | 90-100                  |                        | _                    | <u>&lt;5</u> <u>5</u> | -19 20               | 0-29                 | 30-39                |  |
| Afternoon<br>Night        | .9125<br>.8087<br>.4800 | .0875<br>.1913<br>.5200 |                        |                      | .0 .                  | . 100                | .002<br>.002<br>.001 | .001<br>.002<br>.003 |  |

# Location Houston

|                           |                                 | Drybulb Temperature        |                            |                         |                         |                         |                         |                   |  |
|---------------------------|---------------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------|--|
| Shift                     | <5                              | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                   | 80-89                   | <u>90-99</u>            | <u>100+</u>       |  |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0               | 0.0<br>0.0<br>0.0          | 0.002<br>0.001<br>0.002    | 0.024<br>0.024<br>0.022 | 0.652<br>0.728<br>0.855 | 0.248<br>0.202<br>0.108 | 0.073<br>0.045<br>0.013 | 0.0<br>0.0<br>0.0 |  |
|                           | Effective Temperature           |                            |                            |                         |                         |                         |                         |                   |  |
| Shift<br>Day              | <u>&lt;5</u>                    | <u>5-19</u>                | <u>20-29</u>               | <u>30-39</u>            | 40-79                   | <u>80-89</u>            | 90-99                   | 100+              |  |
| Afternoon<br>Night        | 0.001<br>0. <del>0</del><br>0.0 | 0.014<br>0.012<br>0.011    | 0.048<br>0.044<br>0.033    | 0.106<br>0.094<br>0.081 | 0.510<br>0.602<br>0.754 | 0.248<br>0.203<br>0.108 | 0.073<br>0.045<br>0.013 | 0.0<br>0.0<br>0.0 |  |
|                           | W                               | ind Speed                  | <u>d</u>                   |                         |                         | C1c                     | oud Cove                | <u>r</u>          |  |
| Shift                     | <13                             | 13-24                      | 25+                        |                         | Shift<br>Day            |                         | Sunny                   |                   |  |
| Day<br>Afternoon<br>Night | 0.4713<br>0.5600<br>0.7463      | 0.4838<br>0.4188<br>0.2425 | 0.0463<br>0.0188<br>0.0100 |                         | Afternoon               | I                       | 0.4400<br>0.2000        |                   |  |
|                           |                                 | Precipit                   | ation                      |                         |                         | 1                       | Fog                     |                   |  |
| Shift                     | None or<br>Trace                | .01                        | .0209                      | .1+                     | (Vi                     | isibilit                | y <1/16                 | Mile)             |  |
| Day<br>Afternoon<br>Night | 0.953<br>0.955<br>0.960         | 0.013<br>0.013<br>0.012    | 0.026<br>0.026<br>0.017    | 0.018<br>0.012<br>0.011 |                         | Average                 | 0.                      | 01                |  |
|                           | Relat<br>Humic                  |                            |                            | ,<br><del></del>        | Correc<br>Temperati     | ction of<br>ure for     |                         |                   |  |
| Shift<br>Day              | 90                              | 90-100                     |                            | -                       | <u>&lt;5</u> <u>5</u>   | <u>-19</u> <u>2</u>     | 0-29                    | <u>30-39</u>      |  |
| Afternoon<br>Night        | 0.9000<br>0.8000<br>0.4637      | 0.1000<br>0.2000<br>0.5363 |                            |                         | 0.001<br>0.0<br>0.0     | 0.005<br>0.004<br>0.004 | 0.004<br>0.004<br>0.003 | 0.0<br>0.0<br>0.0 |  |

# Location Galveston

|                           | Drybulb Temperatur?        |                            |                            |                         |                         |                         |                         |                   |  |
|---------------------------|----------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------|--|
| Shift                     | <5                         | <u>5-19</u>                | 20-29                      | <u>30-39</u>            | 40-79                   | <u>80-89</u>            | <u>90-99</u>            | 100+              |  |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0          | 0.0<br>0.0<br>0.0          | 0.0<br>0.0<br>0.0          | 0.013<br>0.012<br>0.009 | 0.653<br>0.681<br>0.717 | 0.324<br>0.301<br>0.270 | 0.010<br>0.007<br>0.004 | 0.0<br>0.0<br>0.0 |  |
|                           | Effective Temperature      |                            |                            |                         |                         |                         |                         |                   |  |
| Shift                     | <5                         | <u>5-19</u>                | 20-29                      | 30-39                   | <u>40-79</u>            | 80-89                   | <u>90-99</u>            | 100+              |  |
| Day<br>Afternoon<br>Night | 0.001<br>0.0<br>0.0        | 0.015<br>0.015<br>0.012    | 0.041<br>0.036<br>0.028    | 0.089<br>0.080<br>0.066 | 0.519<br>0.561<br>0.619 | 0.324<br>0.301<br>0.270 | 0.010<br>0.007<br>0.003 | 0.0<br>0.0<br>0.0 |  |
|                           | W                          | ind Spee                   | d                          |                         | ٠                       | <u>C1</u>               | oud Cove                | <u>r</u>          |  |
| Shift<br>Day              | <13                        | 13-24                      | 25+                        |                         | Shift<br>Day            |                         | Sunny                   |                   |  |
| Afternoon<br>Night        | 0.4550<br>0.5763<br>0.6275 | 0.5163<br>0.3975<br>0.3438 | 0.0300<br>0.0263<br>0.0300 |                         | Afternoo                | n                       | 0.4987<br>0.2112        |                   |  |
|                           |                            | Precipit                   | ation                      |                         |                         |                         | Fog                     |                   |  |
| Shift                     | None or<br>Trace           | .01                        | .0209                      | .1+                     | (1                      | Mile)                   |                         |                   |  |
| Day<br>Afternoon<br>Night | 0.955<br>0.968<br>0.963    | 0.011 (                    | 0.021<br>0.014<br>0.016    | 0.013<br>0.008<br>0.011 |                         | Averag                  | e .00                   | 5                 |  |
| 01.00                     | Rela<br>Humi               | dity                       | ,                          | . •                     | Temperat                | ture for                | f Effecti<br>Painters   | Only              |  |
| Shift<br>Day              | 90                         | 90-100<br>0.1150           | <b>1</b>                   | •                       |                         |                         | 20-29                   | 30-39             |  |
| Afternoon<br>Night        | 0.8850<br>0.7987<br>0.69   | 0.2013<br>0.31             |                            |                         | 0.001<br>0.0<br>0.0     | 0.002<br>0.002<br>0.001 | 0.001<br>0.001<br>0.0   | 0.0<br>0.0<br>0.0 |  |

# -tocation San Diego, CA

|                           |                         | Drybulb Temperature     |                         |                      |                         |                       |                  |                |  |  |
|---------------------------|-------------------------|-------------------------|-------------------------|----------------------|-------------------------|-----------------------|------------------|----------------|--|--|
| Shift                     | <5                      | <u>5-19</u>             | 20-29                   | 30-39                | 40-79                   | 80-89                 | 90-99            | 100+           |  |  |
| Day<br>Afternoon<br>Night | .0<br>.0                | .0<br>.0                | .0<br>.0                | .001<br>.0<br>.0     | .963<br>.986<br>.991    | .033<br>.013<br>.008  | .003<br>.0<br>.0 | .0<br>.0<br>.0 |  |  |
| \                         |                         |                         | Effe                    | ective T             | emperatu                | re                    |                  |                |  |  |
| Shift                     | <5                      | <u>5-19</u>             | 20-29                   | 30-39                | 40-79                   | 80-89                 | 90-99            | 100+           |  |  |
| Day<br>Afternoon<br>Night | .0<br>.0<br>.0          | .0<br>.0                | .0<br>.0<br>.001        | .018<br>.016<br>.018 | .946<br>.971<br>.973    | .033<br>.013<br>.008  | .003<br>.0<br>.0 | .0<br>.0       |  |  |
|                           |                         | lind Spee               |                         |                      |                         | <u> </u>              | oud Cove         | r              |  |  |
| <u>Shift</u><br>Day       | <u>&lt;13</u>           | 13-24                   | 25+                     | :                    | <u>Shift</u><br>Day     |                       | Sunny            |                |  |  |
| Afternoon<br>Night        | .8638<br>.9638<br>.9800 | .1350<br>.0350<br>.0200 | .0025<br>.0013<br>.0013 | •                    | Afternoor               | 1                     | .6265<br>.2750   |                |  |  |
|                           |                         | Precipit                | ation                   | -                    |                         |                       | og               |                |  |  |
| Shift                     | None or<br>Trace        | .01                     | .0209                   | <u>.1+</u>           | (Vi                     | isibility             | <u>.</u> -       | Mile)          |  |  |
| Day<br>Afternoon<br>Night | .983<br>.981<br>.975    | .006<br>.006<br>.009    | .007<br>.010<br>.013    | .004<br>.003<br>.003 |                         | Avera                 | ge .o            | 1              |  |  |
| Relative<br>Humidity      |                         |                         |                         |                      | Correc<br>Temperati     | ction of<br>are for F | Effectivainters  | ve<br>Only     |  |  |
| Shift<br>Day              |                         | <u>90-100</u>           |                         | -                    | <u>&lt;5</u> <u>5</u> - | <u>-19</u> <u>20</u>  | )-29             | 30-39          |  |  |
| Afternoon<br>Night        | .9862<br>.9512<br>.8275 | .0138<br>.0488<br>.1725 |                         |                      | .0                      | .0<br>.0<br>.0        | .0<br>.0<br>.0   | .0<br>.0<br>.0 |  |  |

# Location Los Angeles

## FREQUENCY OF ANNUAL OCCURRENCES

|                           |                            | Drybulb Temperature        |                            |                         |                            |                         |                     |                                       |  |
|---------------------------|----------------------------|----------------------------|----------------------------|-------------------------|----------------------------|-------------------------|---------------------|---------------------------------------|--|
| Shift                     | <u>&lt;5</u>               | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                      | 80-89                   | 90-99               | 100+                                  |  |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0          | 0.0<br>0.0<br>0.0          | 0.0<br>0.0<br>0.0          | 0.001<br>0.000<br>0.002 | 0.988                      | 0.030<br>0.011<br>0.009 | 0.002<br>0.0<br>0.0 | 0.000<br>0.0<br>0.0                   |  |
|                           |                            |                            | Effe                       | ctive T                 | emperatur                  | ·e                      |                     | ·                                     |  |
| Shift                     | <u>&lt;5</u>               | <u>5-19</u>                | 20-29                      | 30-39                   | 40-79                      | 80-89                   | 90-99               | 100+                                  |  |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0          | 0.000<br>0.0<br>0.0        | 0.006<br>0.002<br>0.004    | 0.049<br>0.040<br>0.041 |                            | 0.030<br>0.011<br>0.009 | 0.002<br>0.0<br>0.0 | 0.000<br>0.0<br>0.0                   |  |
|                           | W                          | ind Speed                  | <u>i</u>                   |                         |                            | Clo                     | ud Cover            | · · · · · · · · · · · · · · · · · · · |  |
| Shift<br>Day              | <u>&lt;13</u>              | 13-24                      | 25+                        |                         | Shift Sunny<br>Day         |                         |                     |                                       |  |
| Afternoon<br>Night        | 0.7838<br>0.8675<br>0.9738 | 0.2100<br>0.1275<br>0.0263 | 0.0063<br>0.0038<br>0.0013 |                         | Afternoon 0.3950<br>0.2600 |                         |                     |                                       |  |
|                           |                            | Precipita                  | ation                      |                         |                            | F                       | og                  |                                       |  |
| Shift                     | None or<br>Trace           | .01                        | .0209                      | <u>.1+</u>              | _ (Vi                      | sibility                | <1/16 M             | lile)                                 |  |
| Day<br>Afternoon<br>Night | 0.974<br>0.978<br>0.977    | 0.006<br>0.005<br>0.007    | 0.008<br>0.014<br>0.011    | 0.012<br>0.003<br>0.005 |                            | Average                 | 0                   | .01                                   |  |
|                           | Rela:<br>Humid             |                            |                            | _                       | Correc<br>Temperatu        | tion of<br>re for P     | Effectiv<br>ainters | /e<br>Only                            |  |
| Shift<br>Day              | 90                         | 90-100                     |                            | •                       | <u>&lt;5</u> <u>5</u> -    | <u>19</u> <u>20</u>     | <u>-29</u>          | 30-39                                 |  |
| Afternoon<br>Night        | 0.9737<br>0.9112<br>0.7762 | 0.0263<br>0.0888<br>0.2238 |                            | ,                       | 0.0                        | .0 (                    | ).0<br>).0<br>).0   | 0.0<br>0.0<br>0.0                     |  |

## Location Portland, OR

## FREQUENCY OF ANNUAL OCCURRENCES

|                     |                         |   | Dry                     | /bulb To             | emperatur              | <u>e</u>             |                      |                      |
|---------------------|-------------------------|---|-------------------------|----------------------|------------------------|----------------------|----------------------|----------------------|
| Shift<br>Day        | <u>&lt;5</u>            | <u>5-19</u>                             | 20-29                   | 30-39                | 40-79                  | 80-89                | 90-99                | 100+                 |
| Afternoon<br>Night  | .0<br>.0                | .002<br>.001<br>.0                      | .019<br>.018<br>.019    | .097<br>.111<br>.176 | .84°<br>.834<br>.803   | .033<br>.032<br>.002 | .006<br>.004<br>.0   | .0<br>.0             |
|                     |                         | *************************************** | Effe                    | ctive                | Temperatu              | re                   |                      |                      |
| <u>Shift</u><br>Day | <5_                     | <u>5-19</u>                             | 20-29                   | 30-39                | <u>40-79</u>           | <u>80-89</u>         | 90-99                | 100+                 |
| Afternoon<br>Night  | .006<br>.004<br>.001    | .034<br>.034<br>.032                    | .096<br>.102<br>.135    | .184<br>.200<br>.275 | .641<br>.624<br>.554   | .033<br>.032<br>.002 | .006<br>.004<br>.0   | .0<br>.0<br>.0       |
| Shift               | <u> </u><br><13         | dind Spec                               | ed                      |                      | Shift                  | <u> </u>             | oud Cover            | <u>r</u>             |
| Day<br>Afternoon    | .7638                   | .2238                                   |                         |                      | Day<br>Afternoon       |                      | Sunny                |                      |
| Night               | .7638<br>.7763<br>.8600 | .2238<br>.2163<br>.1325                 | .0100<br>.0088<br>.0075 |                      | Ar ternoor             | 1                    | .2987<br>.1500       |                      |
|                     |                         | Precipit                                | tation                  |                      |                        | 1                    | Fog                  |                      |
| Crier               | None or                 |   | 00 00                   | • .                  | (Vi                    |                      | / <1/16 1            | file)                |
| Shift<br>Day        | Trace                   | <u>.01</u>                              | .0209                   | .1+                  | ,                      | Averag               | e .01                |                      |
| Afternoon<br>Night  | .880<br>.884<br>.885    | .043<br>.043<br>.041                    | .067<br>.063<br>.065    | .010<br>.010<br>.009 |                        | •                    |                      |                      |
|                     |                         | tive<br>dity                            |                         |                      | Correc<br>Temperatu    | tion of<br>re for l  | Effectiv<br>Painters | /e<br>Only           |
| Shift<br>Day        | 90                      | 90-100                                  |                         | -                    | <u>&lt;5</u> <u>5-</u> | <u>19</u> <u>20</u>  | <u>)-29</u>          | <u>30-39</u>         |
| Afternoon<br>Night  | .8712<br>.8275<br>.6250 | .1288<br>.1725<br>.3750                 |                         |                      | .004 .0                | )34 .                | .016<br>.019<br>.029 | .012<br>.015<br>.028 |

# Location Seattle

# FREQUENCY OF ANNUAL OCCURRENCES

|                           |                            |                            | Dry                        | bulb Ter                | mperature               | <u> </u>                |                         |                         |
|---------------------------|----------------------------|----------------------------|----------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| Shift                     | <5                         | 5-19                       | 20-29                      | 30-39                   | 40-79                   | <u>80-89</u>            | 90-99                   | 100+                    |
| Day<br>Afternoon<br>Night | 0.0<br>0.0<br>0.0          | 0.003<br>0.002<br>0.001    | 0.018<br>0.017<br>0.015    | 0.123<br>0.138<br>0.199 | 0.838<br>0.830<br>0.783 | 0.016<br>0.013<br>0.002 | 0.002<br>0.001<br>0     | 0.0<br>0.0<br>0.0       |
| ,                         |                            |                            |                            | *                       |                         |                         |                         |                         |
|                           |                            |                            | Effe                       | ctive T                 | emperatu                | re                      |                         | <del></del>             |
| Shift                     | <5                         | <u>5-19</u>                | 20-29                      | <u>30-39</u>            | 40-79                   | <u>80-89</u>            | 90-99                   | <u>100+</u>             |
| Day<br>Afternoon<br>Night | 0.005<br>0.002<br>0.001    | 0.056<br>0.056<br>0.064    | 0.158<br>0.169<br>0.211    | 0.247<br>0.263<br>0.320 | 0.517<br>0.496<br>0.402 | 0.016<br>0.013<br>0.002 | 0.002<br>0.001<br>0     | 0.0<br>0.0<br>0.0       |
|                           |                            | Wind Spee                  | ď                          |                         |                         | CI                      | oud Cove                | r                       |
| Shift                     | <13                        | 13-24                      | 25+                        |                         | Shift                   |                         | Sunny                   |                         |
| Day<br>Afternoon<br>Night | 0.6000<br>0.6088<br>0.7200 | 0.3638<br>0.3688<br>0.2638 | 0.0338<br>0.0225<br>0.0188 | ,                       | Day<br>Afternoo         | n                       | 0.2962<br>0.1475        |                         |
|                           | <u></u>                    | Precipit                   | ation                      |                         |                         |                         | Fog<br>ty <1/16         | M:Io\                   |
| Shift                     | None o                     |                            | .0209                      | .1+                     | (1                      |                         | • .                     | -                       |
| Day<br>Afternoon<br>Night | 0.902<br>0.883<br>0.864    | 0.031<br>0.047<br>0.058    | 0.059<br>0.061<br>0.068    | 0.008<br>0.009<br>0.010 | <b>)</b>                | Ave <del>r</del> ag     | e 0.02                  |                         |
|                           |                            | ative<br>nidity            |                            |                         |                         |                         | f Effect<br>Painter     |                         |
| Shift                     | 90                         | 90-100                     |                            |                         | <u>&lt;5</u>            | <u>5-19</u>             | 20-29                   | 30-39                   |
| Day<br>Afternoon<br>Night | 0.8050<br>0.7600<br>0.4925 | 0.1950<br>0.2400<br>0.5075 | )                          |                         | 0.005<br>0.002<br>0.001 | 0.022<br>0.027<br>0.018 | 0.025<br>0.027<br>0.040 | 0.009<br>0.011<br>0.020 |

#### APPENDIX C

### WEATHER EFFECTS ON OUTDOOR WORK EFFICIENCY

A review of the literature was undertaken to establish, to the extent possible, quantitative efficiency coefficients for outdoor workers engaged in "shipyard-like" activities, as influenced by climatic conditions. Unfortunately, the published literature in this area provides little useful information in a form that can be directly applied. Where data are available, generally they are in the form of physiological factors which are not directly related to either weather factors or laborer efficiency.

From the limited literature which is applicable (see Bibliography at end of the Appendix), the following summary of weather effects can be established.

The important climatic conditions affecting outdoor workers are:

- Temperature: high, low, diurnal and annual range
- Precipitation: rain, snow, sleet and ice
- Humidity: also presences of salt
- Wind: also presence of sand or dust
- Miscellaneous: sunlight, fog.

## <u>Temperature</u>

Figure 1 summarizes data from eight sources. Variations reflect measurements of work activities requiring different skills. Furthermore, some efficiency loss data were campiled from studies where only the tempo of the actual work was measured. Time to warm the hands or feet in winter, or time to cool off in summer, was not included. These higher estimates of efficiency are, therefore, probably conservative, since total loss in work time was not

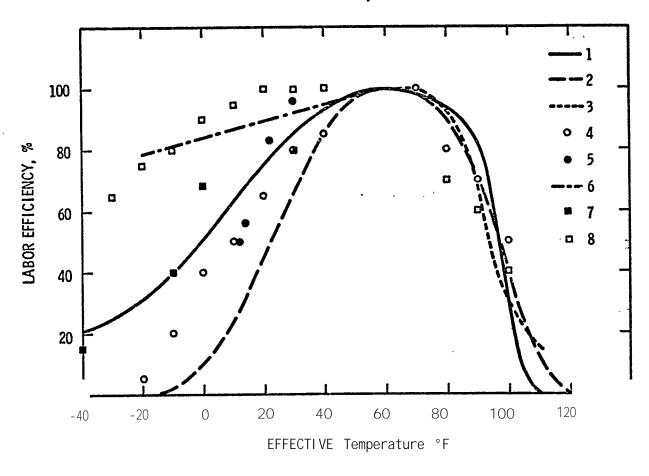


FIGURE C-1. Outdoor Worker Efficiency

#### **LEGEND**

- Doyle, "Controlling Climate Effects", Tool Engr., 1955 (efficiency curve prepared under condition of little or no wind).
   General Dynamics, Quincy (DX Study).
   ASHVE Guide and Data Book (men at work 90,000 ft-lb of work per hour).
   Constructor, May 1972 (welders, pipefitters, carpenters, electricians).
   Unidentified shipyard estimate (converted from equivalent temperature)

- to effective temperature).

  6. Bechtel construction project in Canada (winter) (Converted from wind chill temperature and corrected to 100% efficiency at 60"F).

  7. ASHVE Guide and Data Book (Armstrong's data for line-maintenance job).

  8. Constructor, May 1972 (laborers, ironworkers, operating engineers].

really considered. Another factor that would decrease efficiency even further is bad "ground" conditions resulting from ice, water or mud. When such conditions prevail, the estimates are quite conservative.

#### Wind

Human efficiency is significantly affected by cooling, which is a function of both temperature and of wind speed. Studies by the U.S. Army Quartermaster Corps resulted in the computation of a "wind chill factor" by which the effect of temperature and wind can be objectively evaluated (see Figures C-2 and C-3). Most outdoor operations cease when the chill factor reaches 1200, "bitter cold".

Wind also hinders the movement and positioning of large pieces and increases paint losses. Wind "noise" reduces effective communication between workers. Wind-blown dust and salt sprays increase maintenance problems with equipment.

Another method used to measure the effective of temperature and wind is <u>effective</u> temperature (ET). The ET is determined from dry- and wet-bulb temperatures and air motion by reference to standard ET charts. When a wind is blowing, the ET can be estimated by lowering the measured temperature one degree for each one mile per hour of wind, using a practice adopted by environmental engineers.

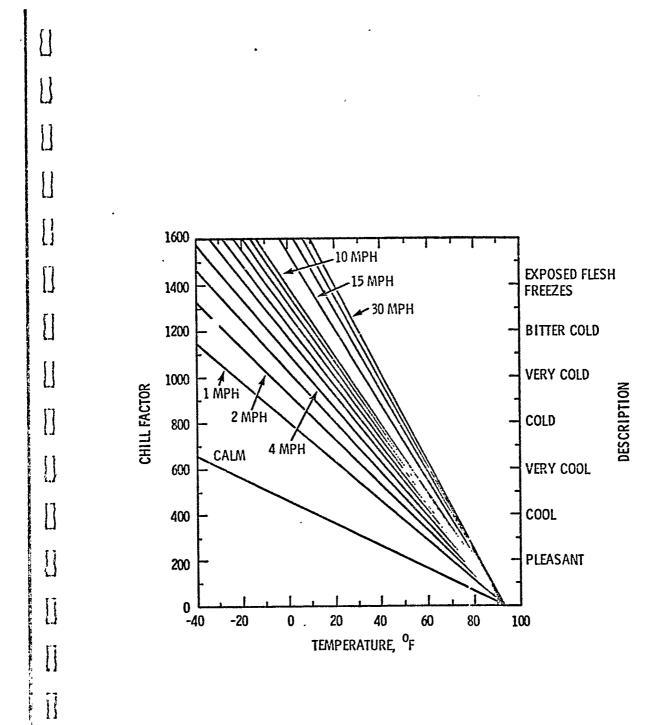
The curves in Figure 1 are plotted against ET although the difference between ET and wind chill temperature (equivalent temperature) is seldom great. The ET index is most applicable to warm atmospheres when radiation effects are not significant. An ET of 78 represents the threshold of sweating, while an ET of 90 is the upper limit for continuous exposure of heat-acclimatized men engaged in light activities. The upper permissible limit for moderately hard work is an ET of 85, and for heavy work, 80 ET. In hot spaces of Naval ships (underway), 91 ET is well tolerated during the usual 4-hr watches. (1)

At moderate temperatures, depending upon the work being done, labor efficiency gradually declines with increasing wind speeds over 15 mph and

| TEMP- | <u>≻35</u> | 30_         | 25              | 20             | 15           | 10       | 5            | 0      | <u>-5</u> | -10  | -15         | -20_ | -25    | -30  | -35  | -40         | -45     |
|-------|------------|-------------|-----------------|----------------|--------------|----------|--------------|--------|-----------|------|-------------|------|--------|------|------|-------------|---------|
| MPH   |            |             |                 |                |              |          |              |        | D CHI     |      |             |      | C. CC. |      |      |             |         |
| * 1   | (EQUI)     |             | LIEW            | PERATUR        | F) - F       | QUIV     |              | ניסט א | LING F    | OWER | ON EXP      |      |        |      |      |             | DITIONS |
| CAIM  | 35         | 30          | 25              | 20             | 15           | 10       | 5            | 0_     | -5-       | 10-  | —-15<br>——- | -20  | -25    | 30   | 35   | -40         | -45     |
| 5     | 33         | 27          | 21              | 16             | -12          | 7        | 1            | 6-     | -11       | -15  | -20-        | -26  | 31=    | -35  | -41  | -47         | -54     |
| 10    | 21         | 16<br>Vi    | .RY C           | 2              | ·· 2         | .9       | -15          | 22     | -27       | -31  | -38         | -45  | -52    | -58  | -64  | ;-70        | -77     |
| 15    | 16         | 11          | 1               | δ<br>BITT      | -11<br>ERLY  | -18/     | -25          | -33    | -40       | -45  | -51         | -60  | -65    | -70  | -78  | -85         | -90     |
| 20    | 12         | 3           | j <sup>-4</sup> | -9 CO          | EXTRE<br>COL |          | -32·         | -40    | -48       | -52  | -60         | -68  | -76    | -81  | -88  | <b>-9</b> 6 | -103    |
| 25    | 7          | 0/          | -7              | -15            | -22          | -29      | -37          | -45    | -52       | -58  | -67         | -75  | -83    | 89   | -96  | -104        | -112    |
|       |            |             |                 |                |              | <b>'</b> | <b>EXPOS</b> | ED FLE | SH FRE    | EZES |             |      |        |      |      |             |         |
| 30    | 5          | <b>/</b> -2 | -11             | -18<br>/       | -26<br>/     | -33      | -41          | -49    | -56       | -63  | -70         | -78  | -87    | -94  | -101 | -109        | -117    |
| 35    | 3          | -4          | -13             | <b>/</b> -20 / | -27          | -35      | -43          | -52    | -60       | -67  | -72         | -83  | -90    | -98  | -105 | -113        | -123    |
| 40    | 1          | -4          | -15             | -22            | -29          | -36      | -45          | -54    | -62       | -69  | -76         | -87  | -94    | -101 | 107  | -116        | -128    |
| 45    | 1          | -6          | -17             | -24            | -31          | -38      | -46          | -54    | -63       | -70  | -78         | -87  | -94    | -101 | -108 | -118        | -128    |
| 50    | Ö          | -7          | -17             | -24            | -31          | -38      | -47          | -56    | -63       | -70  | -79         | -88  | -96    | -103 | -110 | -120        | -128    |

WIND SPEEDS GREATER THAN 40 MPH HAVE LITTLE ADDITIONAL CHILLING EFFECT

Figure C-2 - The U.S. Army Wind Chill Index



 $\underline{ \mbox{Figure C-3}} \mbox{ - Chill Factor for Selected Wind Speeds}$ 

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rapidly approaches zero between 40 and 60 mph. Winds of 40 mph are likely to stop work on exposed staging.(1)

## **Precipitation**

Rain decreases efficiency. Under rainy conditions at 50°F and without wind, workers well clothed in rain trousers, jackets, hats and boots lose only about 10% in efficiency. When exposed to rain and strong winds, men cannot remain dry for much more than one hour regardless of how well they are clothed.

At low temperatures, labor efficiency and safety are still further impaired by precipitation. Sleet or ice are considered more limiting to outside work than rain or snow. Workers will generally not continue working during a sleet storm. Precipitation has been found more serious than freezing temperatures in reducing efficiency of an outside railroad car building line in a mild climate. In 23 days of rain, 97 cars or about 35% were lost out of a scheduled 278. During 5 days of ice, snow, sleet and rain, 28 cars or 50% were lost out of a scheduled 56. Only 4 cars out of 14 were reported lost because of cold weather alone.

Besides discomfort, precipitation decreases efficiency by decreasing visibility; making parts, tools, and equipment slippery and hard to handle; and making working conditions more hazardous.

#### Humidity

Several comfort indexes have been devised to express the effect of temperature and humidity. There is general agreement that the comfort zone for normally efficient work extends to about 80°F with 50% relative humidity and to the mid-70's with 75% relative humidity. Discussions with construction personnel indicate that operations are not significantly affected until the temperature rises above 80°F. It is estimated that a reasonable threshold of temperature-humidity would be 85°F and 50%. This corresponds to a U.S. Weather Bureau Temperature-Humidity Index value of 77, and Table 1 gives several combinations of temperature and relative humidity that are equivalent. (2)

TABLE 1. U.S. Weather Bureau Temperature-Humidity Index

| <u>Temperature</u> | Relative Humidity | Index |
|--------------------|-------------------|-------|
| 86                 | 79                | 77    |
| 85                 | 50                | 77    |
| 90                 | 24                | 77    |
| 95                 | 8                 | 77    |

Reduced efficiency appears to occur at the following limits of temperature and humidity: (8)

| Maximum<br><u>Temperature</u> |     | Humidity        |
|-------------------------------|-----|-----------------|
| 85-89°                        | and | <u>&gt;</u> 50% |
| 90 <b>-</b> 94°               | and | <u>&gt;</u> 30% |
| 95-99°                        | and | <u>&gt;</u> 20% |
| 100°                          | and | Any             |

## Night Lighting

Shipyard estimates for improper lighting (outdoor areas) range from 10 to 25% productivity loss. Survey results by others show increases in work output of 3 to 20% are possible for heavy work activities similar to shipbuilding. These increases were brought about by illumination changes. Atypical example: original-4.6 fc, new-12.7 fc.

#### <u>FOQ</u>

The, effect of fog is to reduce visibility. In shipbuilding this affects primarily riggers and crane operators who must be able to see the boom, the load being lifted and hand signals. Reduction of visibility to less than the boom length or the distance to a signaler stops crane work.

The 100% humidity accompanying fog also affects painting operations. It usually prevents painting outdoors.

## Sun1ight

The effect of sunlight, e.g. hot summer sun, is to reduce worker efficiency not only by raising the effective temperature but by heating steel plates to uncomfortably high temperatures. Personnel working on sun-heated surfaces are often forced to retire to a shaded area, provide shade or find work in a cooler location.

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#### APPENDIX D

#### TYPICAL HEATHER PROTECTION STRUCTURES IN U.S. SHIPYARDS

In the course of the study, nine U.S. Shipyards were visited. Photographs of some of the weather protective devices and structures were obtained and are shown on the following pages.

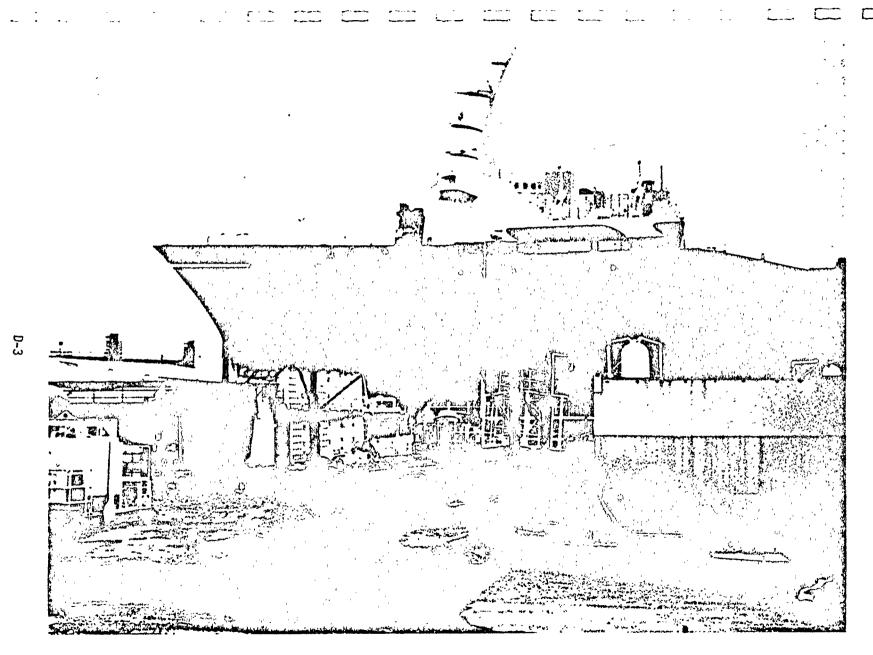
In addition to those devices pictured, numerous shelters of a temporary nature--plywood, tarpaulin or plastic on wood or scaffold framework--are used for rain and wind protection. Several shipyards use portable weather protective devices to keep welding electrodes dry. Each welder has a heated container which holds 10 pounds of electrodes and can be carried from place to place and plugged in to an outlet nearby. Used containership containers have also been utilized for storage, shops and office space in a U.S. shipyard.

An all-weather painting facility at the General Dynamics yard in Quincy, Massachusetts, has been in operation since 1968. It is able to handle subassemblies up to 50 ft square and 30 ft high. The facility includes climate control for painting and drying, telescoping doors for access, and a heating-ventilating system rated at 75,000 cfm.

The Ingalls Shipyard at Pascagoula, Mississippi, has installed a weather-protected shotblasting facility. It is able to handle 56 ft by 56 ft sections up to-100 tons.

Other examples of weather protection are shown in the following photographs.

<u>Figure D-1</u> - A portable steel shelter used to provide rain protection and shade for shipyard work either on the ground or on the deck of a ship or barge. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.



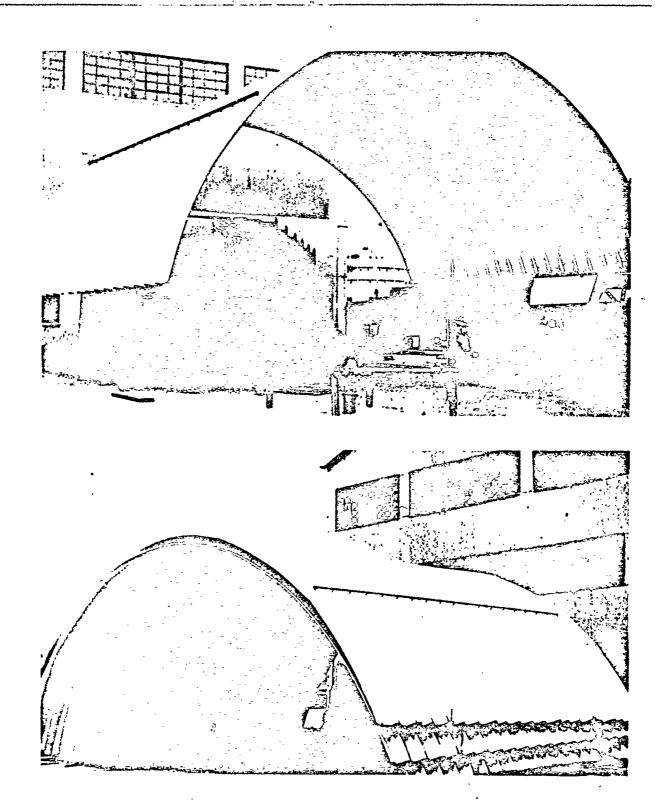
<u>Figure D-2</u> - A portable steel shelter used to provide rain protection and shade for shipyard work either on the ground or on the deck of a ship or barge. Courtesy of Avondale Shipyards, Inc., New Orleans, Louisiana.

 $\frac{\text{Figure D-3}}{\text{protection from the rain and hot sun both of which tend to shorten machine life.}} - \text{A close-up of a weather protective device for welding machines.}$  The roof provides protection from the rain and hot sun both of which tend to shorten machine life. Fastening the machines to the frames gives an added bonus of rapid portability.} Courtesy of Todd Shipyards Corporation, Houston, Texas.}

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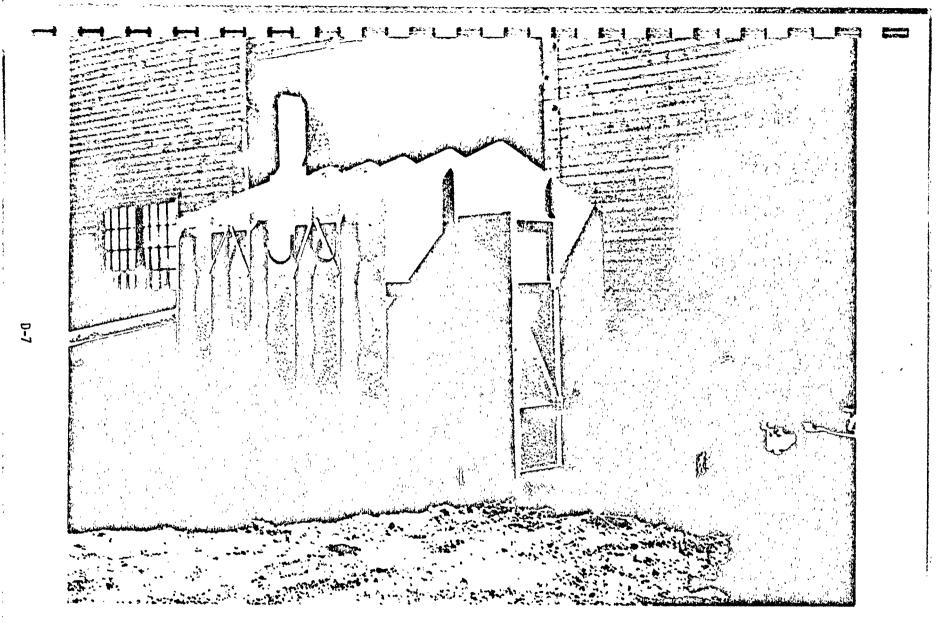
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Author to the



 $\frac{\text{Figure D-4}}{\text{for rain and shade protection for various operations.}} \text{ --- Heavy corrugated sheet metal roofs ("Wonderbuilding" arches) used for rain and shade protection for various operations.} \text{ Units can be nested for strage as shown in lower photo.}$ 

<u>Figure D-5</u> - A lean-to addition used for rain and sun protection in heavy manufacturing (rail car). The shelter allows work to proceed in bad weather when it might otherwise be forced to shut down. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.



<u>Figure D-6</u> - An all-weather protective shed for storage of paint and paint pumps. Electrically heated, it is a complete, portable paint station which prevents freezing of stored paint and the paint pumps and pots themselves. Courtesy of FMC, Marine and Rail Equipment Division, Portland, Oregon.

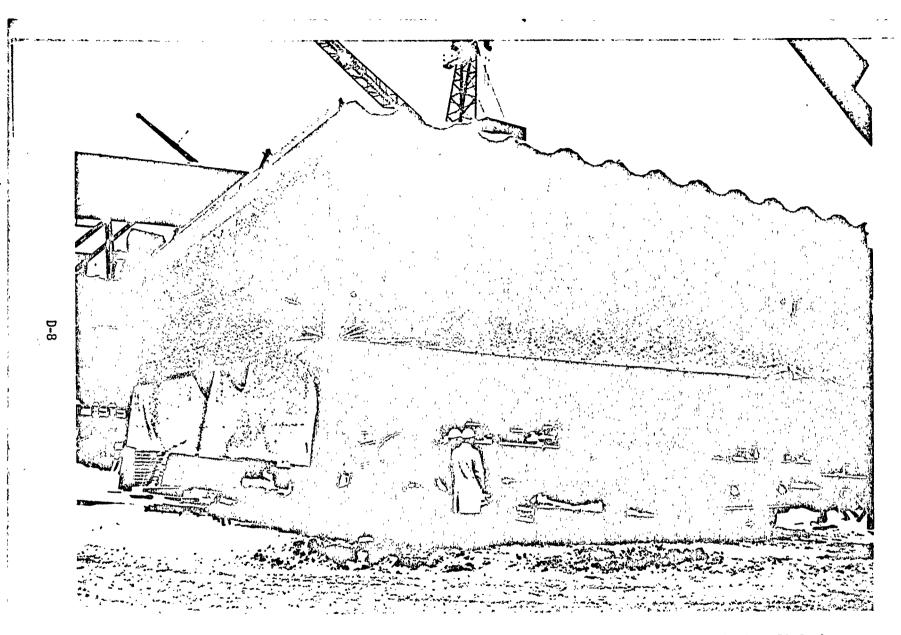


Figure D-7 - Temporary weather protective shelter. These portable structures measure 40 ft x 50 ft in plan with roof heights varying from 12-30 ft. The roof grid is assembled from cold rolled beams and supported on pipe columns. The roof cover is large corrugation metal sheeting. Removable rubberized canvas sidewalls provide additional protection. The shelter encloses sufficient volume to protect a variety of welding, blasting, painting and storage activities. Courtesy of Bath Iron Works Corporation, Bath, Maine.

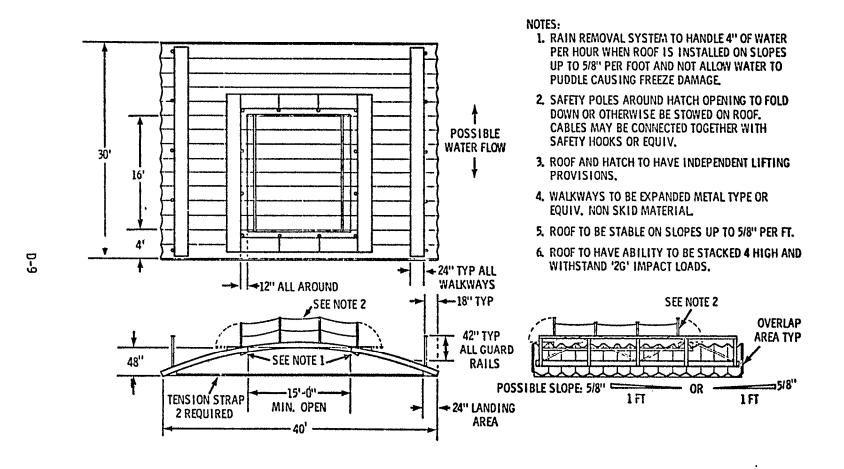


Figure D-8 - Design for a Portable, Trussless Cover with Hatch for Hull Construction - Newport News Shipbuilding and Dry Dock Company.

#### APPENDIX E

#### MODULAR WEATHER PROTECTION PANELS

#### HOARDING PANELS

#### Typical Design Criteria

#### 1. Diffusion of Light

Hoarding panels should be such that no auxiliary light is required during the normal daylight.

#### 2. Resistance to Wind

Closure system should be such that it could stand the high winds during the winter months (up to 70 mph).

#### 3. Strength of Panels

Enclosures should be such that they could support the load of the different panel sections when installed one on top of the other. When used as the roof, they should also be able to support the snow load.

## 4. Loss of Heat

The closure should be such that the heat loss is at a minimum.

## 5. <u>Versatility</u>

Closures should be such that they could be adapted to numerous configurations, re: stand alone structures, structural steel requirements, etc.

#### Design Specifications

To meet the above criteria, one contractor assembled hoarding panels in an 8'-0" x 16'-0" size, which were constructed of 2 x 4 spruce frame with 2 x 4 studs at 2'-8" on center. Reinforced woven polyethylene was applied on the frame and was held in place by 1 x 2 lumber strips all over the frame and studs. Design of the hoarding panel is shown in Figure E-1.

Figure E-1 - Design of Hoarding Panels

E-2

For the fabrication of the hoarding panels, a jig was made which permitted panels to be made in different sizes: 8' x 16', 6'x 16', 4' X 16', 2' X 16'.

To minimize heat loss, two layers of polyethlene can be used, if necessary, with air gap up to a maximum of one inch between the two layers.

#### Erection

Hoarding panels are secured together by a tie and wedge system. Panels are then nailed to small wooden frames built around the steel building frame as shown in Figure E-2.

For the construction of structures inside a main building, hoarding panels are attached to one another to forma closure.

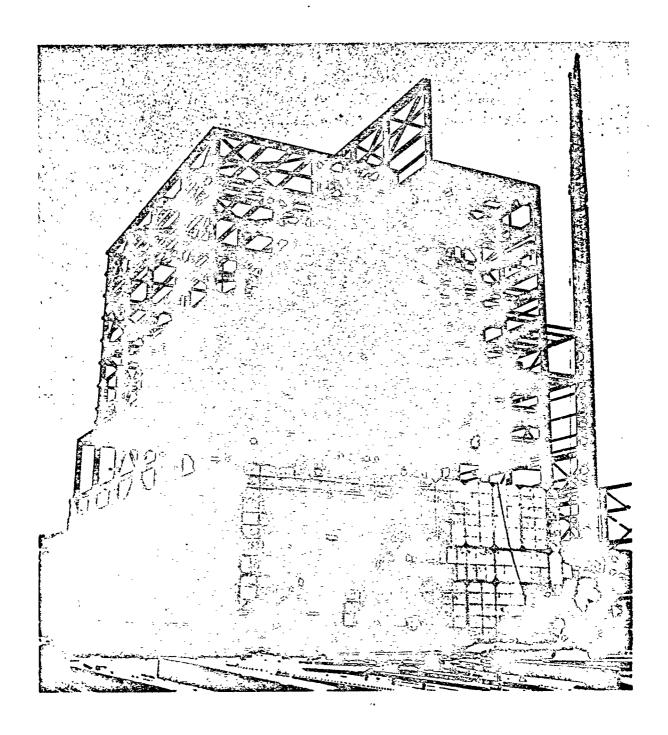
#### Cost of Hoarding Panels

A cost studies indicated that it is more economical to fabricate panels on the job site rather than purchase or rent them from others. Total cost of the hoarding panels is about \$0.40/sq\$ ft with a cost breakdown as follows:

| Material          | \$0.09 Sq ft |
|-------------------|--------------|
| Manufacture Labor | 0.44 "       |
| Erection Labor    | 0.19 "       |
| Dismantle Labor   | 0.08 "       |
| Total             | \$0.40 Sq ft |

Average cost of one panel, 8x 16 ft= \$48.00.

Figure E-3 illustrates portable welder's shelter used in civil construction works.



 $\frac{ \mbox{FIGURE E-2}}{\mbox{Enclosure.}} \mbox{- Hoarding Panels Attached to Building Frame to Form Weather} \label{eq:bulker}$ 

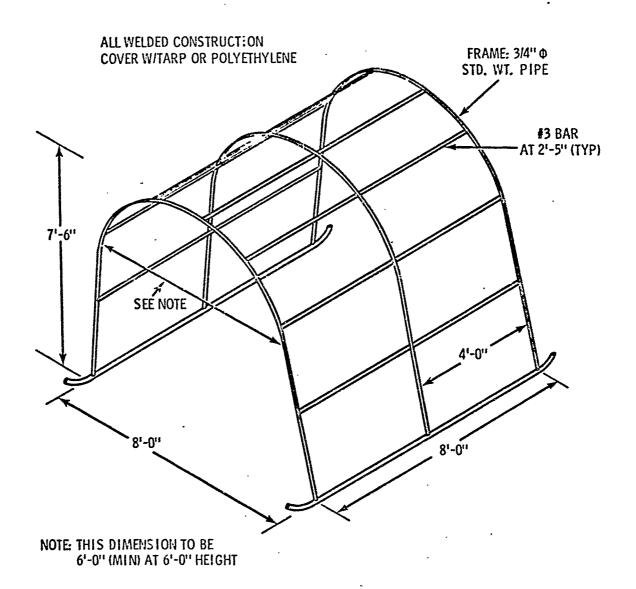


Figure E-3 - Portable Welder's Shelter

#### APPENDIX F

#### DESCRIPTION OF AIR-SUPPORTED SHELTER

A large, most unique shelter used on a civil works project in Canada was an "air shelter" or, as it is commonly called, a "bubble". It is an air supported structure, a strong. flexible, balloon-like envelope, supported and stabilized by maintaining a small pressure differential within the envelope. The air supported shelter is a dynamic structure, as contrasted with a static pile of bricks, mortar of timbers, and is the ultimate in structural efficiency. There is no redundancy of structural material in the pretensioned shell and the apparent simplicity of the shelter belies the actual complexity of the design of all its components. The shell must tolerate and resist all the normal loadings experienced by any other type of structure. It does so with a shell measuring only a few hundredths of an inch thick.

Physical characteristics of the shell material, seam design, loading around the doorways, and the pressurization system must be carefully chosen and controlled to ensure satisfactory, life and usefulness.

The structure was 100' wide, 200' long, and 50' high, with ends that were almost 'square". It covered an area of almost 20,000 sq.ft., the surface area of the shell Was 35,000 sq.ft. The fabric was guaranteed for eight years.

The bubble used a' vinyl-coated nylon with a 2x 2 basket weave, having a tensile strength of  $400 \times 400$  lb/in. The material was described as off-white which admitted sufficient light during the daytime for all types of work. Inside, the shell appeared to be an unusual orange-yellow color.

The joints were heat sealed to develop the full-strength of the fabric.

The envelope was supplied in three sections which were joined by a single interlocking peg system which was readily assembled or disassembled without special tools.

The sectionalizing permitted the individual packages to be kept to a reasonable size to handle and, also gave flexibility to the ultimate size of the shelter by adding or subtracting additional center sections when required.

Sandbags were installed in the ballast skirt, approximately six cubic feet of sand per foot of periphery, to hold the shell down and solid anchors were provided for the attachment of cables to isolate and redistribute the load around the doorways.

Two Buffalo-Forge, Model 600A, 3 H.P. centrifugal blowers, each having a free delivery of 14,000 cfm provided sufficient pressure for normal operation and the other was used for unusual conditions as well as beings standby unit. The inflation pressure was just less than one. inch of water, which resulted in a pressure of approximately 5 lb/sq.ft.

Automatic pressure controls operated the second blower when the internal pressure dropped because of excessive leakage through open doors or damage to the shelter or because of failure of the primary blower.

A plywood airlock, twenty feet wide, twenty feet high and thirty feet long with full opening access doors was used to permit the passage of all materials, trucks, and cranes. Small doors were installed in the airlock for personnel ingress or egress to avoid using the main doors and two additional emergency exits were also provided in the sides of the shelter.

The inlet air to the blowers was heated by six Herman-Nelson oil-fired heaters which were enclosed in a temporary shelter. The maximum output of the heaters was 1-1/2 million BTU/hr. The thin shell does not provide very good insulation qualities and the overall heat transfer coefficient is approximately 1.2BTU/hr/°F/sq.ft. which is similar to single glazing.

The introduction of the heat through the blowers gives good distribution, and as the mass of the structure is low, the internal temperature can be increased rapidly.

The delivered cost of the shelter was just over \$50,000 \$2.50/sq.ft.

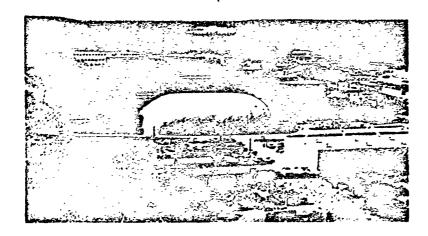
The weight of the supliment was 8706 pounds and occupied a volume of 720 cu. ft.

The shelter was first erected in early February over the excavation for the foundation of the Final Extraction Plant. The temperature ranged from 20° above zero to 22° below zero. The erection was completed within two working days by a crew of sixteen men. No real problems arose despite the complication of raising the shelter over the large excavation. The structure was completely dismantled, at the end of its useful period, in four hours.

The shelter possesses several advantages over the more conventional types of hoarding, such as:

- The interior is completely free of posts, trusses, cables, or other supporting members, this allows for more flexibility of operation and construction.
- 2) The blowers provide a natural circulating media for heat, which is provided by any type of heater located outside the working area. This saves space and also reduces the fire hazards.
- 3) The skin is translucent and little additional illumination is required during daylight hours. This factor can be a major item for more conventional types of shelter.
- 4) The structure can be reused, as requird, with no loss of material, as many times as necessary. While the original cost is higher than other types of hoarding, even only a second reuse would be economical. The disadvantages of the structure must also be considered:
- 1) Limited working area and height inside the shelter. This is not too serious for small, low buildings, but the work must proceed slower than outside. The handling of material and equipment through the airlock has to be planned and coordinated.
- 2) The loss of air pressure, for any reason, could be disastrous. All sharp projections on rebar, forms, etc., were covered with a plywood cap to avoid damage to the skin, should the shelter collapse. In good weather, little damage should result, however in a storm (which also

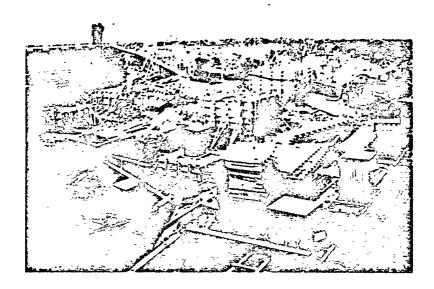
increases the possibility of power failure) the structure could be completely destroyed.



 $\frac{\text{Figure F-l}}{\text{access air}}$  - View of the 100' x 200' 50' high air shelter. A large vehicle



Figure F-2 - Concrete form work in progress inside the air shelter. Note the height of the columns, the wooden caps on top of the reinforcing steel to protect the skin in case of a loss in pressure. Also note the excellent natural light.



 $\frac{\text{Figure F-3}}{\text{the base of the "bubble" over the excavation.}}$  The workers in the upper left are standing in front of a small man-made access way.

#### APPENDIX G

#### INFORMATION SOURCES

Information on the effects of weather on outdoor worker productivity and methods to provide weather protection was sought through letter contacts with the following:

### Trade Associations

- 1. Associated Builders and Contractors
- 2. Associated General Contractors of America
- 3. Building Research Advisory Board
- 4. Building Research Institute
- 5. American Concrete Institute
- 6. American Society of Concrete Constructors

#### Construction Firms

- 1. American Dredging Company
- 2. The Austin Company
- 3. Bow Valley Industries, Ltd.
- 4. Bovis Corp., Ltd.
- 5. Dravo Corp.
- 6. Dravo of Canada, Ltd.
- 7. Fluor Corporation
- 8. General Construction Company
- 9. J. A. Jones Construction Company
- 10. Kaiser Industries Corp.
- 11. M. W. Kellogg (Div. of Pullman, Inc.)
- 12. Michigan Wisconsin Pipe Line Company
- 13. Morrison-Knudsen Company, Inc.
- 14. Guy F. Atkinson Company
- 15. Blaw-Knox Company
- 16. C. F. Braun and Company
- 17. Chemical Construction Corp.-
- 18. Hoffman Construction Company

## Page 2

- 19. Whitehead Kales Company
- 20. Genstar, Ltd.
- 21. Bechtel Corp.
- 22. ITT Levitt and Sons, Inc.
- 23. Pullman, Inc.
- 24. Ocean Drilling and Exploration Company
- 25. Ocean Service and Engineering, Inc..
- 26. The Ralph M. Parsons Company
- 27. Pacific Car and Foundry Co.

### Research Organizations

- 1. Cold Regions Research and Engineering Laboratory
- 2. Environmental Protection Systems Division
- 3. Fordham University
- 4. National Bureau of Economic Research
- 5. Naval Artic Research Laboratory
- 6. Rand Corporation
- 7. Stevens Institute of Technology
- 8. U.S. Department of Commerce
- 9. University of Illinois
- 10. University of Michigan
- 11. Department of the Army, Construction Engineering Research Laboratory

REPORT OF THE STUDY FOR DETERMINING THE STATE-OF-ART OF THE USE OF WEATHER PROTECTION IN THE JAPANESE SHIPBUILDING AND HEAVY EQUIPMENT INDUSTRIES.

to
Battelle Pacific Northwest
Leboratories

May, 1973

Mitsubishi Research Institute 1-1, Yurakucho, Chiyodaku Tokyo, Japan

#### **Preface**

This is the Final Report on the Study for Determining the State-of-the-Art of the Use of Weather Protection in the Japanese Shipbuilding and Heavy Equipment Industries, based on the Special Agreement B-654, signed on 31st, October 1972, between the Battelle Pacific Northwest Laboratories and Mitsubishi Research Institute.

The study has been carried out according to the principles and definitions stated in the Research Proposal dated 15th November 1972, made by The MRI on the subject above stated. The Draft Report of MRI, dated 27th March 1973, was reviewed by BNW and succeeding comments were meet and incorporated into the Final Report.

Japanese experience on the weather protection for outdoor works are unique and has a history of nearly two decades in many shipyards. Weather Protection facilities in these shipyards are one of the cause of productivity improvement in Japanese shipbuilding industries, competiting in the world market with foreign shipbuilders.

It would be the first time to describe the state-of-the-art of the usc of and the cost-effectiveness of the weather protection devices in Japan in a comprehensive way for foreign people. who have the interest on it.

We hope this Report will be good for the use for the sponsors in U.S.

#### May 1973

S.Ikeda, General Manager

T. Miyakawa, Senior Transportation Economist

Research and Development Department Mitsubishi Research Institute, Tokyo, Japan.

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### 1. The method of study and other explanations

First we have surveyed the usage of weather protection facilities among 25 major Japanese shipyards to get overall picture. Then, we have selected four shipyards, located at places with a wide weather variation and represent different type of workshop layouts, i.e. one from northern region, one from central reagion and two from western region of Japan. We have asked for these four shipyards necessary data for weather protection devices used and carried out enquete survey to engineers at workshops to get data for productivity gains. Photographs were taken on the protection facilities studied during these enquete surveys on the spot.

As for the heavy construction industry we have selected one large steel construction site located contral region of Japan. We add brief survey of crane and wharf protection during extreme climatic conditions, the data for which were obtained simultaneously during the survey on the spot.

This study was carried out by us with close cooperations of engineers in the Shipbuilding Division of Mitsubishi Heavy Industries Ltd.

2 Selection of Shipards and a Large-scale Construction site to be Investigated

Pattelle Northwest are requesting to obtain the informations on shipyards, having a range of typical climatic conditions. We set two criteria for the selection of shipyards. The first is the criteria by the climatic conditions and the second is the one concerning the layout of the shipyards.

2.1. The Criteria by the climatic conditions.

The climatic conditions concerning out-door heavy construction works in Japan can be devided into following three types ( for detailed explanation on each climate see comments p.9 seq.)

- 1) Eastern Japan-Pacific Coast
- 2) Western Japan-Pacific Coast
- 3) Northern Japan

Whereas the difference in climate between Eastern Pacific Cost and Western Pacific Coast are not so clear except the duration of rainy months during summer, this difference on rainy weather would be significant in considering the out-door working conditions. The climate in Northern Japan differs clearly from the other parts of the country. Despite the relatively low latitude ( for example Sapporo, the capital of Hokkaido is at 35°N), the climate there has the same characteristics like Northern Europe, in higher latitude. Thus we need, at least, three types of shipyard that are locating in each of one climatic conditions mentioned aboved.

### 2.2. The criteria concerning the layout of shipyard.

In Japan there are 45 major shipyards that have at least one shipbuilding berth over 5,000 gross tonnage. Among these, 23 shipyards have been building the major part of new ships. These 23 large shipyards that have at least one building berth over 30,000 gross tonnage, can be divided into 3 groups in terms of the date of their establishment.

First group of shipyards arc old ones that were established before or during the World War II and some of them even dated from one hundred years ago. The layout and the construction flow of these old shipyards have been modernized and renewed as possible within the limited land use after the War, especially during the Suez Crisis shipbuilding boom, (1956-58), and the second boom after 1963.

The second group of shipyards are completely new giant shipyards that are established upon the reclaimed land, and its layout were designed to achieve the most effective construction. These shipyards were erected mainly after 1965. Whole of them have building docks that can build super tankers over 100,000 gross tonnage.

The third group is the most newly established and the largest shipyards. They have large building decks in which tankers up to one million dwt can be built. They began their operation around 1970.

The types of weather protection devices used among these shipyards depend on the differences of the duration of operations since shipyard's establishment and subsequent modernization and their final layouts.

2.3 The differences of the use of weather protection devices among the type of shipyards.

In Japanese shipbuilding industry, the means to prevent the fluctuation of productivity in the outdoor welding and assembling works due to the variation of weather, have been improved significantly during these decade.

In the most old conventional type of shipyards, the outdoor works in hull construction yard were changed and arranged to fit into the large welding and black assembling factory during the later half of 1950's. In the case of Nagasaki shipyard ( Mitsubishi Heavy Industries), these improvements were carried out through following process.

- (1) change of the flew of sheets
- (2) modernization of sheet bending and cutting process
- (3) enlargement of welding spaces
- (4) increase of crane capacities
- (5) construction of huge roof overwelding and small block assembling yard
- (6) integration of welding work and small-block assembling work

At the end of covered assembling factory, hull blocks, usually SO to 80 metric tons in average, were lifted up and down directly onto the adjacent building berths by the giant gantry cranes. Thus the most parts of hull construction stages were covered by the roofs except final assembling processes that were carried out on the building berths. These improvement, which included the change of factory layout partly, was completed by the end of 1957, when the ratio of outdoor works was reduced to only 14 percent to the whole hull construction works. The layout of building berths were changed again substantially during 1965-68 to enlarge building capacity at Nagasaki. These improvement consisted of the integration and increase of width of old berths, replacement of old gantry cranes to giant goliath cranes and construction of new building docks. The crane capacities were increased from 50 tens to 120 tons and thus the maximum size of blocks to be supplied from the assembling factory reached up to 120 tons. However major flow of hull blocks remained, in principle, the same as before.

These "indoorization" of outdoor welding and assembling works were carried out, in general, through similar processes in other major shippards on the Pacific Coast during 1955-1965.

The plannings and constructions of the new shipyards in the second group began around 1960 among the largest shipbuilding companies. In this case, some of the Swedish examples of advanced shipbuilding technology and novel ideas incorporated into the layout of ships within shipyards, e.g. those at the Arendal Shipyard of Gotaverken A/B, had a considerable influence upon the planning of new larger shipyards in Japan. In these new generation of shipyards, the most part of outdoor works were "indoorized" from the beginning, having large welding and block-assembling shops. For example, in Yokohama Shipyard of Ishikawajima-Harima Heavy Industries Co., Ltd., there are five indoor welding and block-assembling shops, each 853 feet long and 115 ft. wide. Hull block over 100 tons can be assembled in these shops. The outdoor works remains only at the final assembling stage on the uncovered building dock.

This New Yokohama shipyard of IHI began its operation 1968.

In the third group of new shipyard, even the large building dock is covered partly by the roof. For example, in Koyagi Shipyard of Mitsubishi Heavy Industries, the maximum size of a hull block which can be assembled within assemble shops arc 600 tons. Over the buildingdock, that is 3182 ft. long and 328 ft. wide, there are two sets of travelling roofs each 164 ft-long and 328 ft. wide. Thus, the works in the final stage of ship-construction are partly "indoorized". This newest shipyard has just begun its operation in this year.

#### 2.4. The Selection of shipyard

We select three large shipyards each located in different climatic conditions from layout type 1, that is Shipyard W from Eastern Japan, Shipyard X from Western Japan and Shipyard V at Northern Japan. For the method used in the indoor welding assembling works in the type 2 shipyards are the same to those are used in the type 2, we do select no shipyard from the layout type 2, However we add Shipyard Y from layout type 3. (cf. Table 1),

Although we will survey the use of weather protection facilities in these four shipyards in deptth, we supplement the result with further informations on other shipyards, if we find significant exceptional examples to the fact surveyed.

Table 2-1 Classification of Shipyards. (1) (2)

| Type of Layout     | Туре І.  | Newly Built lar                   | rge Shipyard |  |  |  |  |
|--------------------|--|-----------------------------------|--------------|--|--|--|--|
| Climatic Condition | Old but modernised   | Type II.                          | Type III.    |  |  |  |  |
| Eastern<br>Japan   | IHI-Tokyo,<br>IHI-Nacoya,<br>MHI-Yokohama<br>NKK-Tsurumi<br>Sumitomo   | Mitsui-Chiba<br>IIII-Yokohama     | NKK-Tsu      |  |  |  |  |
| Western<br>Japan   | IHI-Kure IHI-Aioi MHI-Nagasaki MHI-kobe MII-Hiroshima Kawasaki-Kobe Mitsui-Tamano Hitachi-Innoshima Osaka Sasebo | Kawasaki-Sakaide<br>Hitachi-Sakai | MHI/Koyagi   |  |  |  |  |
| Northern<br>Japan  | Hakodote<br>Hitachi-Maizuru  | 3                                 |              |  |  |  |  |

Note (1) Major 23 shipyards are listed first by the name of company and then of shipyard, i.e. IHI-Tokyo means Ishikawajima-Harima Heavy Industries, Tokyo Shipyards.

(2) Abbreviation of the names of companies,

MiI: Mitsubishi-Heavy-Industries

NKK: Nippon Kokan Company

Table 2-2. Shipyard to be studied in Depth.

Total S

To the same of

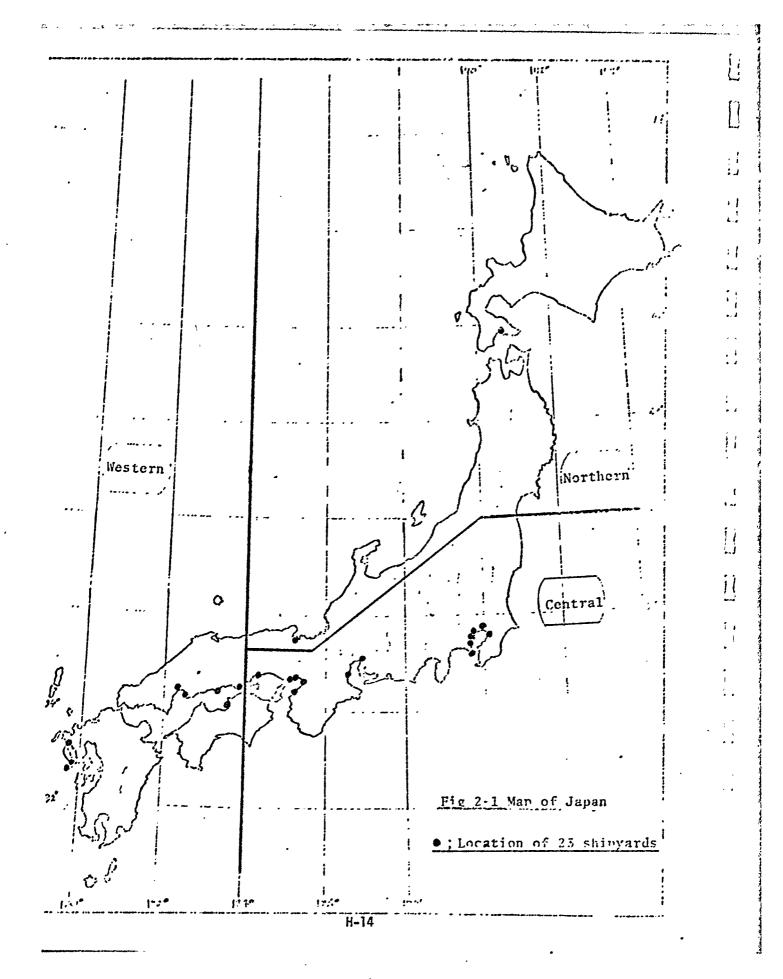
To the same

No.

All Control

| region                              | name                     | shipbuilding capacity        |
|-------------------------------------|--------------------------|------------------------------|
| northern                            | shipyard V               | 43.700 G.T.                  |
| central                             | shipyard W               | 106.000 G.T.                 |
| Western                             | shipyard X<br>shipyard Y | 170.000 G.T.<br>250.000 G.T. |
| Large-scale<br>construction<br>shop | workshop Z               |                              |

A rough distribution of shipyards under study is shown in the figure 1.



#### 3.1. Two Patterns in Climate

Japan consists of islands, facing eastwards to the Pacific Ocean and westwards to the Sea of Japan. Japan also has a latitudial span of 21, from 24°N to 454. llence, there are-two different climatic conditions in Japan. The first, which we call "climatic pattern of emote Nippon", forward side of Japan, i.e. Pacific Coast, except northern Tohoku, North eastern region of Honshu, and Hokkaido, has a similar chracter of weather It is hot and moist in summer and relatively warm and dry in winter. In June and first half of July we have usually the rainy season due to the monsoon from the Asian Continent. But in winter, we have relatively stable weather. It is fine and rarely rains or snow.

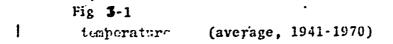
The second pattern that we call "climatic pattern of Ura Nippon", back side of Japan, i.e. regions along Sea of Japan and llokkaido. The weather in summer is not so different from "Omote Nippon", but in winter there are many snowy days. It is cold and dark from November to March. From December through February the temperature is below freezing point in Hokkaido. In this region, "the rainy season in June and July" is not so distinct. We explain these differences in details constracting with the number of the days of rain and snow and temperature and precipitation at four cities.

#### 3.2. Temperature

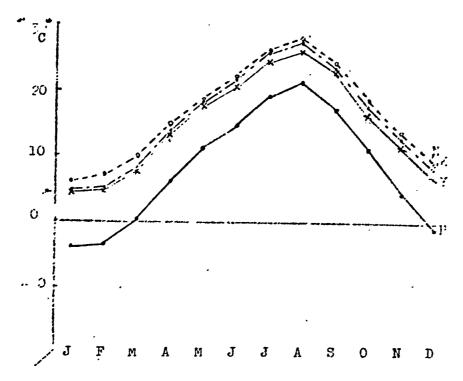
In temperature significant difference can be observed between Hakodate (Hokkaido) and other three cities in Honshu. In Hakodate average temperature through year is under 10°C and during winter, monthly average are below freezing point.

| month                   | Hakodate                     | Yokohama                     | Kobe                         | Nagasaki                     |
|-------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1<br>2<br>12<br>average | -3.9<br>-3.5<br>-1.1<br>-2.1 | 4.4<br>4.8<br>7.0<br>6.0     | 4.5<br>4.8<br>7.4<br>6.2     | 6.2<br>7.1<br>8.9<br>8.1     |
| 7<br>8<br>9<br>average  | 19.3<br>21.5<br>17.2<br>17.5 | 24.6<br>26.1<br>22.6<br>24.4 | 25.8<br>27.3<br>23.6<br>25.6 | 26.4<br>27.6<br>24.3<br>26.1 |

(Obsevation data: 1941-70)



1 ; 1,1



H: Hakodate Y: Yokohama K: Kobe N: Nagasaki

# 3.3 Precipitation and Wind

Monthly change in precipitations at four cities are shown in Fig 2. The peak due to the monsoon is in June except in Hakodate. The second peak in September are usually due to the typhocus. The largest precipitation is observed at Nagasaki. (cf. Table 1)

Table 3-1 Precipitations

|  | average prec<br>per month       | ipitation                            | precipitation per<br>per year |                                      |  |  |  |
|--|---------------------------------|--------------------------------------|-------------------------------|--------------------------------------|--|--|--|
|  | millimeters                     | (inches)                             | millimeters                   | (inches)                             |  |  |  |
| Hakodate<br>Yokohama<br>Kobe<br>Nagasaki | 95.3<br>136.0<br>113.9<br>164.7 | (3.75)<br>(5.35)<br>(4.48)<br>(6.48) | 1143<br>1632<br>1367<br>1976  | (45.0)<br>(64.3)<br>(53.8)<br>(77.8) |  |  |  |

Table 3-2 Days of Rain and Snow

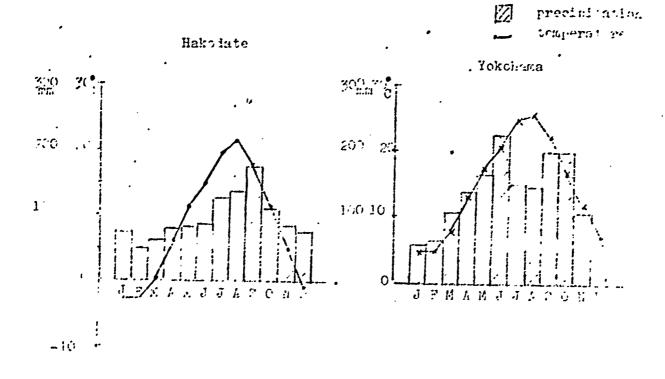
| Month<br>Place | J         | F          | М        | A | М | J   | J | A | S  | 0 | N   | D        |
|----------------|-----------|------------|----------|---|---|-----|---|---|----|---|-----|----------|
| Hakodate       | 11<br>(9) | 11<br>(10) | 9<br>(7) | 3 | 4 | . 4 | 4 | 3 | 4  | 6 | 6   | 11       |
| Yokohama       | (1)       | 4 (1)      | 4        | 5 | 4 | - 6 | 3 | 3 | 4  | 6 | (3) | (9)<br>  |
| Kope           | (1)       | 4<br>(2)   | 4        | 3 | 4 | 6   | 4 | 2 | -5 | 5 | 3   | 3        |
| Nagasaki       | 5<br>(3)  | 5<br>(1)   | 5<br>(1) | 4 | 5 | 7   | 5 | 2 | 4  | 3 | 2   | 5<br>(1) |

(Observation Data: 1945-52)

Note: Figures in brackets show the days of snowfall.

Fig. 3-2

Frecipitation and Temperature



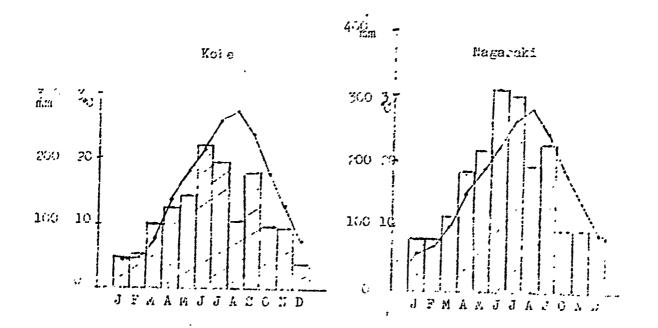


Table 3-3
The amount of snowfall (Depth of snowfall of each month is designated by number of days in each category)

| month    | Categories of        | 11 | 12 | 1  | 2  | 3   | 4 | total |
|----------|----------------------|----|----|----|----|-----|---|-------|
| region   | depth of snow (inch) |    |    |    |    |     |   |       |
|          | under 3.94           | 0  | 0  | 2  | 1  | 0   | 0 | 4     |
| Western  | over 3.94            | 0  | 0  | 0  | 0  | 0_  | 0 | 0     |
|          | over 7.87            | 0  | 0  | 0  | 0  | 0   | ۵ | 0     |
|          | over 19.69           | 0  | 0  | 0  | 0  | 0   | 0 | 0     |
|          | under 3.94           | 0  | 0  | 1  | 3  | 1   | 0 | 5     |
| ļ        | over 3.94            | 0  | 0  | 0  | 1  | 0   | 0 | 1     |
| Central  | over 7.87            | 0  | 0  | 0  | 1. | 0   | 0 | 1     |
|          | over 19.69           | 0  | 0  | 0  | 0  | 0   | 0 | 0     |
|          | under 3.94           | 6  | 14 | 7  | 5  | 10_ | 2 | 45    |
| _        | over 3.94            | 1  | 9  | 24 | 22 | 11  | 0 | 67    |
| Northern | over 7.87            | 0  | 4  | 14 | 16 | 7   | 0 | 41    |
|          | over 19.69           | 0  | 0  | 0  | 0  | 1   | 0 | 1     |

( Values above are averages between 1941 and 1960 )

Table 3-4
Temperature (in centigrade) (during the work hours)

| month<br>region | 1    | 2    | 3    | 4   | 5          | 6    | 7         | 8    | 9    | 10   | 11   | 12   |
|-----------------|------|------|------|-----|------------|------|-----------|------|------|------|------|------|
| Western         | 6.2  | 7.1  | 10.2 | 14. | 718.5      | 21.9 | 26.4<br>i | 27.6 | 24.3 | 18.6 | 13.8 | 8.9  |
| Central         | 4.4  | 4.8  | 7.5  | 12. | 717.1<br>! | 20.5 | 24.6      | 26.1 | 22.6 | 16.5 | 11.5 | 7.0  |
| Northern        | -3.9 | -3.5 | 0    | 6.  | 111.0      | 14.8 | 10.3      | 21.5 | 17.2 | 11.3 | 4.6  | -1.1 |

( Above values are averages between 1941 and 1970. )

Table 3-5 . Wind Velocity (during the work hours)

| month  | [.            | 1  | 2  | 3  | 4  | 5  | 6 | 7 | 8 | 9   | 10  | 11 | 12 |
|--------|---------------|----|----|----|----|----|---|---|---|-----|-----|----|----|
| region | i             |    |    |    |    |    |   |   |   |     |     |    |    |
| West-  | 22.4          | 8  | 7  | 9  | 7  | 6  | 7 | 7 | 3 | 4   | . 3 | 3  | 5_ |
|        | over 33.6     | ì  | 1  | 2  | 2  | 1  | 2 | 2 | 1 | 1   | 1   | 0  | 1  |
| Cent-  | 22.4          | 12 | 15 | 16 | 16 | 14 | 9 | 8 | 7 | 8   | 12  | 11 | 12 |
| 1 721  | over<br>33.6  | 3  | 4  | 4  | 4  | 2  | 1 | 1 | 1 | 2   | 2   | 2  | 3  |
| North  | 22.4<br>-33,6 | 15 | 14 | 16 | 16 | 14 | 7 | 4 | 3 | 7   | 10  | 11 | 13 |
| ern    | over<br>33.6  | 3  | 3  | 2  | 2  | 2  | 0 | 1 | 0 | 1 - | 1   | 1  | 2  |

( Above values are averages between 1949 and 1960 )

Table 3-6
The number of days of high discomfort index (during the work hours )

| month                         | Jı  | ine |    | Ju   | 1y   |     | Aug          | ust  |     | s    | epte | mber |
|-------------------------------|-----|-----|----|------|------|-----|--------------|------|-----|------|------|------|
| Discomfort<br>index<br>region | 75  | 80  | 85 | 75   | 80   | 85  | 75           | 80   | 85  | 75   | 80   | 85   |
| Western                       | 9.0 | 0   | 0  | 30.0 | 14.4 | 0.4 | <b>30.</b> 8 | 18.2 | 1.2 | 19.4 | 4.8  | 0    |
| C ntral                       | 8,4 | 1.2 | 0  | 24.4 | 8.4  | 0   | 27.2         | 17.2 | 0   | 13.8 | 4.4  | 0.2  |
| Northern                      | 0   | 0   | 0  | 1.6  | 0    | 0   | 6.0          | 0    | 0   | 0.4  | 0    | 0    |

( Above values are averages between 1956 and 1960 )

#### note:

We feel rather discomfort when the index shows over 70 and very discomfort when it shows over 80.  $_{H-20}$ 

Table 3-7

The number of days with outdoor temperatures below zero at the shipyard V.

The time of measurement: 9.00A.M., 12.00A.M., 3.00P.M. Measurment was made at above three time points and the average was taken of the three values.

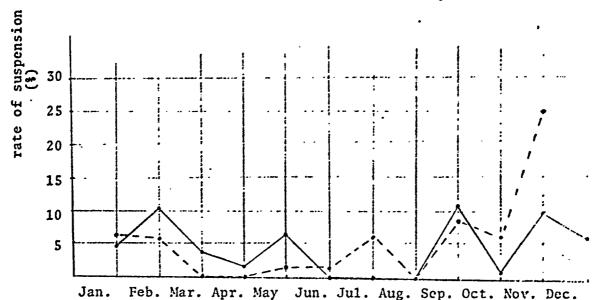
|           |       | The number of days with temperatures below zero |       |       |     |      |  |  |
|-----------|-------|---|-------|-------|-----|------|--|--|
| month     | 28.4F | 24.8F   | 21.2F | 17.6F | 14F |      |  |  |
| Nov. 1969 | 3     | 0   | 1     | 0     | 0   | 4    |  |  |
| Dec. 1969 | 9     | 5   | 3     | 0     | 0   | 17   |  |  |
| Jan. 1970 | 8     | 3   | 2     | 2     | 1   | 16 · |  |  |
| Feb. 1970 | 10    | 6   | 3     | 1     | 0   | 20   |  |  |
| Mar. 1970 | 4     | 7   | 1     | 1     | 0   | 11   |  |  |
| Nov. 1970 | 2     | 0   | 0     | 1     | 0   | 3    |  |  |
| Dec. 1970 | 5     | 2   | 1     | 0     | 0   | 8    |  |  |
| Jan. 1971 | 5     | 5   | 3     | 1     | 0   | 14   |  |  |
| Feb. 1971 | 7     | 2   | 3     | 0     | 2   | 14   |  |  |
| Mar. 1971 | 5     | 9   | 0     | 0     | 0   | 5    |  |  |
| Nov. 1971 | 1     | 0   | 0     | 0     | 0   | 1    |  |  |
| Dec. 1971 | 3     | 2   | 0     | 0     | 0   | 5    |  |  |
| Jan. 1972 | 10    | 4   | 2     | 0     | 0   | 16   |  |  |
| Feb. 1972 | 7 .   | 2   | 1     | 1     | 0   | 11   |  |  |
| Mar. 1972 | 4     | 1   | 0     | 0     | 0   | 5    |  |  |

Table 3-8
The record of wind velocity in recent times at the shipyard V

| month     | the number<br>of days of<br>operation | of days | the number of days warning index issued against craoperation | remarks<br>ne                                    |
|-----------|---------------------------------------|---------|--|--|
| Jan. 1971 | 22                                    | 1.0     | 3.0  |  |
| Feb. 1971 | 23                                    | 2.5     | 1.0  |  |
| Mar. 1971 | 27                                    | 1.0     | 3.0  |  |
| Apr. 1971 | 23                                    | 0.5     | 5.0  | Warning is issued                                |
| May 1971  | 21                                    | 1.5     | 3.0  | against crane                                    |
| Jun. 1971 | 26                                    | 0       | 0  | operation when wind                              |
| July 1971 | 26                                    | 0       | 0.5  | velocity reaches                                 |
| Aug. 1971 | 25                                    | 0       | 2.5  | 33.6 to 40.3                                     |
| Sep. 1971 | 22                                    | 2.5     | 4.0  | miles per hour.                                  |
| Oct. 1971 | 26                                    | 0.5     | 4.5  |  |
| Nov. 1971 | 25                                    | 2.5     | 4.5  | Crane operation is stopped when wind             |
| Dec. 1971 | 25                                    | 1.5     | 2.5  | velocity is more<br>than 40.3 miles per<br>hour. |
| Jan. 1972 | 23                                    | 1.5     | 4.0  |  |
| Feb. 1972 | 25                                    | 1.5     | 3.5  |  |
| Mar. 1972 | 25                                    | 0       | 1.5  |  |
| Apr. 1972 | 21                                    | 0       | 2.5  | :<br>•   |
| May 1972  | 22                                    | 0.5     | 2.5  | 1  |
| Jun. 1972 | 25                                    | 0.5     | 4.0  |  |
| Jul. 1972 | 25                                    | 1.5     | 2.0  |  |
| Aug. 1972 | 26                                    | 0       | 2.0  |  |
| Sep. 1972 | 24                                    | 2.0     | 2.0  |  |
| Oct. 1972 | 24                                    | 1.5     | 4.5  | ;  |
| Nov. 1972 | 24                                    | 6.0     | 2.0  |  |
| Dec. 1972 | -                                     | -       | -  | :  |
|           | 4                                     |         | <br>   |  |

: }

Fig. 3-3.
The monthly rate of suspension of crane operation



#### month

- note: 1) The solid line designates the curve for 1971, while the dotted line designates the curve for 1972.
- note: 2) The average rate for 1971.....5.7% The average rate for 1972.....4.6%
- note: 3) Monthly rate of suspension of crane operation is defined here as the ratio of number of days when crane operations were stopped to the number of days of operation (cf. Table 3-\$ in the previous page).

# 4. Actual Condition. of Protection Facilities in Japan

There are four type of weather protection facilities, adopted for outdoorworks in shipyards and heavy construction industries, i.e. (1) roofs, (2) other facilities in workshops, (3) special devices for cranes and (4) those for wharfs.

#### 4.1. Roofs

Covering with roofs is one method to provide protection from wind, rain, snow and heat. There are four types of roofing and their specifications are described roughly in the Table 4-1.

Table 4-1. Type of Roofing

| Type .   | Specification  |
|--|--|
| Pornanent  | Steel frame roof covered with galva-<br>nixed from sheet                                 |
| ouilding, fully<br>closed                              | Steel frame roof covered with long procoated iron sheet                                  |
| Permanent build-<br>ing with traveling                 | Steel frame roof covered with gal-<br>vanized iron sneet or long precoated<br>iron sheet |
| :<br>Proof   | Steel frame roof covered with slate  |
| Fermanent build-<br>ing with roof,<br>not fully closed | Steel frame roof covered with galva-<br>nized iron sheet                                 |
| Simple traveling                                       | Light gage steel frame roof covered with galvanized iron sheet.                          |
| roor .   | Lightweight steel tube roof covered with eslon sheet                                     |

Table 4-2, Covered rate of assembling yard in major shipyards in Japan mainly as of 1970.

| Region  | Shipyard   | Cove  | red rate | e (%) | Remarks                          |
|---------|------------|-------|----------|-------|----------------------------------|
| · 4     |            | total | type 1   | type2 |                                  |
| North-  | I,         | 56    | 42       | ] 4   |                                  |
| ern     | A          | 51    | 51       | 0     | type 1 100%,<br>as of April 1972 |
|         | В          | 52    | 17       | 35    |                                  |
|         | N.         | 47    | 29       | 18    | {type 1, 378                     |
| 1       | С          | .84   | 76       | 8     | 11 type 2. 33%                   |
|         | D          | 100   | 100      | 0     | total 70%,<br>as of April '72    |
|         | Е          | 59    | 42       | . 17  |                                  |
|         | F          | 34    | 0        | 34    |                                  |
| •       | G          | 56    | 25       | 31    | {type 1, 495                     |
|         | H          | i 68  | 36       | 32    | 11 type 2. 214                   |
| Central | I          | 96    | 96       | 0     | total 70%,<br>as of April '72    |
| Japan   | J .        | - 34  | 34       | 0     | Control of the second            |
|         | К          | 27    | 16       | 11    |                                  |
|         | L          | 49    | . 7      | 42    |                                  |
|         | M          | 61    | 61       | 0     |                                  |
|         | N          | 62    | 0        | 62    |                                  |
|         | 0          | 90    | 90       | 0     | · .                              |
| 1       | P          | 60    | 49       | 11    |                                  |
| Ì       | Q          | 100   | 100      | 0     |                                  |
| estern  | R          | 87    | 87       | 0     |                                  |
| Japan   | · <b>S</b> | • 72  | 61       | 11    |                                  |
| į       | T          | 55    | 20       | 35    |                                  |
|         | , <b>X</b> | 67    | 64       | 3     |                                  |
|         | Y          | 100   | 100      | 0     | as of April '72                  |

Note:

covered rate (1) of assembling yard (1)

Square meter of indoorized assembling surface

Total square meter of assembling surface

(2) Type 1; covered by fixed roof, type 2: covered by travelling roof.

Among four production stages in new construction work, Steel Fabrication stages are wholly indoorized. The vital parts of Block Assembly stage are covered by roofs in the most shipyards. The covered rate of workshop is outlined below.

Block Assembly Shop: Covered ratios by roofs range from 51 to 100% in shipyards.

Pre-Erection Shop, Dock and Builking Berth: Almost all shipyards have no protection facilities, except for several new shipyards provided with roofs of a covered ratio of about 10%. This may also apply to constructional steel works. Painting and Coating Shop: Traveling and fixed roofs are used in roofed shipyards and constructional steel works, with covered ratios ranging from 60 to 100%.

The data of the roofs actually installed at four shipyards surveyed in depth, are shown in the Table 1-5 in the Appendix 1 and their photograph as No. 1-12 in the Appendix 2.

The fiscal 1970 survey on covered ratios in block assembly shops Of Japan's principal shipyards (Table 4-2 on previous page.) gives the following covered ratios: (1) 27 - 87% for shipyards built prior to 1960; (2) 51 - 99% for those built from 1961 to 1970; and (3) 100% for those built from 1971 up to now. According to the survey made this time in 1972, covered ratios of block assembly shops in shipyards in (2) have increased to 70 - 100%. This means that introduction of flow production systems like coveyor lines to promote automation and labor saving in block assembling has necessitated roofing. Particularly, all of newly constructed, sophisticated shipyards In the central and western parts are fully roofed regardless of their siting and weather conditions.

#### 4.2. Other Protection Tools

### 4.2.1. Needs for personal protection tools

Conditions for which needs for personal protection arise in winter and summer are as follows:

Winter: In the northern part, leather windbreakers and trousers—are supplied to all outdoor welders for protection from cold while in the central and western parts outfits for protection from cold are lent to several thousand outdoor workers. Each workshop has heating devices installed as required to allow workers to warm themselves. However, no measures for protection from cold are taken in workshop which are not covered completely.

Summer: Since the maximum temperature in the year (monthly average) is 70.7°F, most comfortable to the human body, in the northern part, no protection from heat is provided there. In the central and western parts indirect methods such as fans and coolers and direct methods like cool suits are taken.

# 4.2.2. Specifications of protection tool for personal use.

There are five main items in protection tool, i.e. ventilating fan, cooler/heater, water cooler, clothing and material to make shadow.

Applications of such protection tools and equipment are listed below.

Table 4-3 Protection Tools and Equipment

|                                    | Protection Tools  | and Equipment   |
|------------------------------------|---|---|
| Item                               | Location  | Specification   |
| Ventilating fan                    | Block assembly shop Pre-erection shop Building berth and dock Painting and coating shop | Commercially available motoroperated ventilating fans 5 - 30 KW                           |
| Cooler and eater                   | do.   | Inboard cooler with<br>the same performance<br>as commercially<br>available type<br>33 KW |
|                                    |   | Gas and kerosine<br>stoves are used as<br>heaters   |
|                                    |   | Coke stove are used as heater   |
| %ater<br>cooler                    | do.   | Commercially available types are used   |
| Outfit for protection against cold | Outdoor block assembly shop, building berth and dock in welding                         | Coat and vest for pro   |
|                                    |   | Leather windbreaker and trousers and pocket warmer  |

<sup>-</sup>cont'd-

# -cont'd-

| Net for protection against heat | Building berth and dock Pre-erection shop | Made of nylon and sizeds 269 to 1076 sq. ft.   |
|---------------------------------|---|--|
| Cool suit                       | Pre-erection shop Building berth end dock | Compressed air is fed into bag in vest to cool |

#### 4.2.3. Use of protection tools among shipyards

We surveyed the state of the arts of the use of protection tools for personal use among 25 major shipyards in Japan, using the data made by Nihon Zosen Kogyokai (Shipbuilders Association of Japan). The data were revised by us through direct interview or questionning to get up-to date picture in Jan. 1972. Percentages in the following Tables denote the share of the number of shipyards in which particular tools adopted to the total number of shipyard surveyed, otherwise mentioned.

Diffusion of use of Protection devices for variation of temperature in the major Shipyards, in Japan as of January 1972 is as follows.

# A. Heating

Table 4.4. Adopted Types by shipyard (25 shipyards)

| Shops   | Steel<br>Fabrication        | Assembly                         | Dock and Build-<br>ing Berth      |
|---|-----------------------------|----------------------------------|-----------------------------------|
| Steam heating<br>Warm air blower<br>Gas Stoves<br>Electric heater<br>Coal stoves<br>Oil heater etc<br>nothing | 0<br>0<br>8<br>1<br>0<br>15 | 0<br>0<br>5<br>0<br>6<br>10<br>4 | 0<br>0<br>3<br>0<br>1<br>11<br>11 |

Table 4-5. Wearings

| percentage of adoption among 24 shipyards |
|---|
| 83%                                       |
| 42\$                                      |
| 12%                                       |
| 4%  |
| 4 %                                       |
| 4 %                                       |
|   |

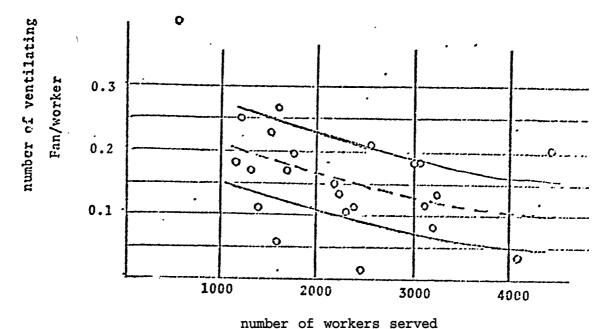
Table 4-6. Standard and system of Supply

| For those who work outdoor wholeday                                   | 37% |
|---|-----|
| For workers at building berth and dock during over-time work at night | 25% |
| For outdoor crane operators at night                                  | 4 % |
| For all outdoor workers   | 46% |
| Lending system  | 71% |
| Supply as personal effects  | 178 |

# Ventilation Fan

Ventilation Fans are used widely among shipyards, of which two standard types are shown as photographs 13 and 14 in the Appendix 2. The correlation of number of ventilating fans installed and the number of workers served are shown in Figure 4-1.

Figure 4-1.Number of ventilation Fan installed

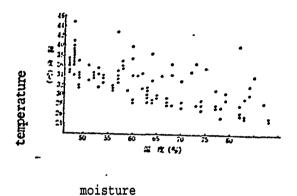


#### Spot Coller Unit

In some shipyard, Spot Cooler Unit, which is shown as photograph 16 in the Appendix 2, arc used to blow cool air through ducts into the shop or into the tank block of-ships on the dock. The complete encolsure of ways do arise other kinds of extreme environments. These arc high temperature, moisture, noise and dust. For example, in welding and fitting works in large hull blocks on the docks in summer, people sometimes have to work in as high temperature as 104F and in high moisture

over 80 percent. These hot and moist environment are caused by the radiation heats both from the equipments themselves people using, i.e. gas cutters, welding tools etc., and steel sheets hot up by direct sunshine. We show an example of high temperature and moisture observed in the hull construction works in Japan.

Figure 4-2. Temperature and moisture in the holds and tanks on the dock.



source: Shipbuilding Association of Japan Working Environment Committee.

These temperatures and moistures are usually extremely high in the holds and tanks directly under the deckplates and inside of side shells in summer. To protect welders and strain removers who are working under such an extreame conditions, Spot Cooler Unit are available in several shipyards. (cf. Figure 4-3). The effects of this device at the shipyard W in the Central Japan and the shipyard X in the Western Japan in the summer 1972 are shown in the Table 4-5. Temperature decrease was 37.4°F in average, moisture decrease 3-5% and discomfort index was lowered to 80.

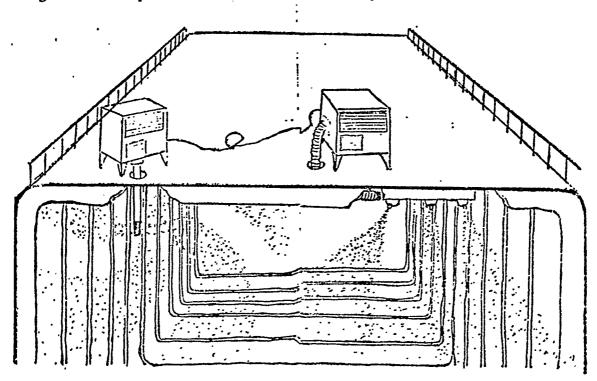
Table 4-7. The effects of Spot Cooler Unit in the Tanks and Holds.

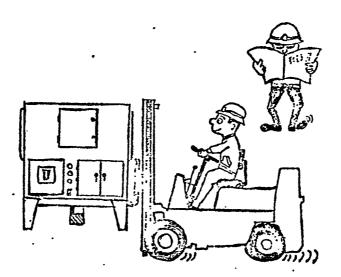
Ovserved: middle of June-middle of September 1972. (Shipyard W in Cemtral Japan)

middle of June-middle of October, 1972. (Shipyard X in Western Japan)

| item    | tempo                 | erature | °F               |           | humi                  | dity | ક્ષ                  |           | đ:                    | iscomfo               | rt index | ¢      |
|---------|-----------------------|---------|------------------|-----------|-----------------------|------|----------------------|-----------|-----------------------|-----------------------|----------|--------|
| egion   | air on<br>the<br>deck |         | (2)air<br>cooler | (1) - (2) | air on<br>the<br>deck | air  | (4)<br>air<br>cooler | (3) - (4) | air on<br>the<br>deck | (S)no<br>air<br>coole | cooler   | (5)-(6 |
| Central | 93.2                  | 95.0    | 89.6             | 5.4       | 47                    | 47   | 44                   | 3         | 84                    | 85                    | 80       | 5      |
| Western | 89.6                  | 100.4   | 91.4             | 9.0       | 66                    | 47   | 42                   | 5         | 82.5                  | . 88                  | 81.5     | 6.5    |

Figure 4-3. Spot Cooler Unit on the deck plate





# Other devices

In all 23 shipyards surveyed, sunnet are used to make shadow to protect workers under direct sunshine on the outdoor working shops (cf. photograph 26 in the Appendix 2.)

In some shipyards dry ice is supplied to the outdoor workers to prevent the heat, especially to cool their heads.

They put the packed dry ice in the bag of felt and set it in the helmet. They change it. twice a day, that is, in the morning and in the afternoon. However the use of dry ice has been suspended recently in many shipyards.

The cool suits is shown as photograph 19 in the Appendix 2.

Table 4-8. Other devices

| -                                  | Percentage of adoption among 23 shipyards surveyed |
|------------------------------------|--|
| Sunnet                             | 100%   |
| Supplying dry-ice for personal use | 31%  |
| Vortextube and cool-suits          | 52 %   |

#### 4.3. Cranes

To prevent cranes from speeding and overturning due to wind force, all outdoor cranes are equipped with clamping devices regardless of their size. (Installation of this device is required by regulations of the Japanese Government.) There are four types of crane protection method, of which photographs attached in the Appendix 2, as follows.

```
Type I. Rail clamping (photos. No. 20)

Type 2. Hooking (photos. No. 21.22.)

Type 3. Pin drop (photos. No. 23.24.)

Type 4. Guy wire (photos. No.25)
```

Though different depending on type of crane, these devices may be roughly divided as listed below.

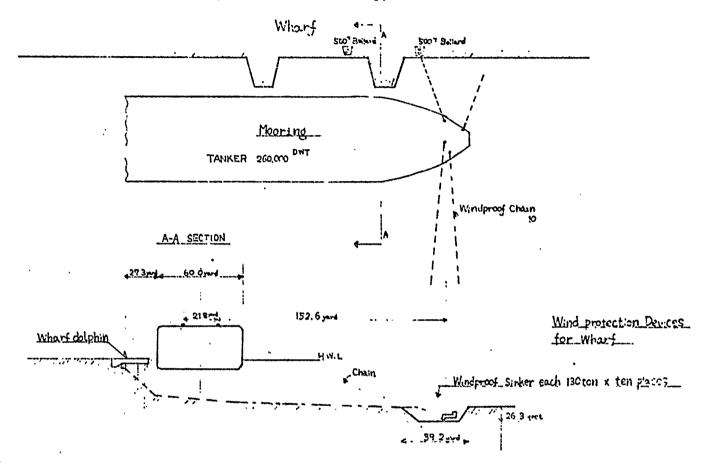
Table 4-9 Crane protection methods

| Description             | Specification   |
|-------------------------|---|
| Rail clamping<br>System | Crane rail is clamped with steel clamp near crane saddle  |
| Hooking system          | Steel hook provided on underside of crane saddle is fitted into eye provided outside or inside of crane rail to clamp crane         |
| Pin (Drop-in)<br>system | Steel bar or strip pin equipped on outside of crane saddle is put in hole provided in foundation outside of crane rail to fix crane |
| Guy wire system         | Steel wire a steel turnbuckle is used to fix crane to foundation from outside of crane saddle                                       |

#### 4.4 Wharf

Almost all shipyards have no particular provisions against strong wind, except for some newly built shipyards in which windproof sinkers are equipped, provided there are ample open sea in front of wharf. An example of the windproof sinker at Shipyard Y is shown as Figure 4-1. Ten chains fixed at the bottom of open sea can hold a mooring ship with other ten chains on wharf side in the case of strong winds.

Figure 4-4. Windproof sinker at Shipyard Y.



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# 5. Relationship of Weather Variation to Productivity in Japan

#### 5.1 Background of the survey

We defined, here, productivity as man-hour efficiency, i.e, man-hours consumed per unit volume of construction. This productivity measure is generally used, as basic index for daily and monthly production control in. Japanese shipyards. The productivity is influenced by equipment, personnel composition, management organization and construction method; of which latter two factors are based on the former two. Weather conditions have also influences on the productivity as a whole. This makes it difficult to single out precise relationship of weather variation to productivity change.

We have tryed to find statistical correlations between man-hours consumed in particular workshops and weather variations during certain time span. Here, productivity measured mainly by man-hours, is a function of weather variations, method of production and management and two factors for production, i.e. equipments and labour. However, man-hours consumed per unit volume constructed differ ship by ship due to their type and size. If we took the man-hour data on the same type and size of ships in longer periods, say four and five years, the production methods were improved gradually during these years. Thus we could not find any precise correlation statistically between weather variation and man-hours consumed.

When we have carried out surveys in depth at four shipyards selected, we have asked for over fifty supervisory personnel at various managerial levels who have long experiences in production work, on their opinions on the effect of weather variations on productivity. Replying to this question, some one relies on man-hours data and others on different data they are using according to their types of workshop. We asked for them to express their empirical obsevations on the effect of weather variations in terms of percentages.

#### 5. 2 Degree of Effect of Weather Change

The degree of effects of weather change on productivity, based on the empirical observation thus collected, is shown in Table S-1. In this table, the monthly degree of effects on productivity are shown as percentages of monthly production in each region compared with the best production efficiency observed from the past experience. This best efficiency is for the production activity of shipyard as a whole, not for the outside work only. Although the effects of weather variation are naturally the lagest on outside works, the production efficiency in roofed Block Assembly Shop has to be reduced, if there occur slow down due to weather variation in succeeding working stage, i. e. Pre-Errection

The most shipyards in Japan are usually located at relatively narrow site along old ports, for example

Nagasaki port is older than United States itself, i,e. it had been receiving foreign traders since 17th century.

When Commodore Perry asked for Tokugawa Shogunate Government to open several Japanese ports for U. S. merchant marines 120 years ago, Yokohama, Kobe and Hakodate were in his list of ports to open doors to him. In old shipyards located at such historically old ports, there are scarcely ample spaces between workshops for storing stock and members to adjust the difference of production efficiencies if any, among workshops. The slow down of production at

Pre-Errection and Dock/Building Berth inevitably affects the production pace of Block Assembly Shop. The effect of weather variation should not be considered separately for outside work only. Thus the figures shown in the Table 4-9 denote the effects of weather change observed as a whole for each shipyard, based on the experiences and opinions of fifty managers and supervisor interviewed.

At the shipyard in northern region, monthly productivities arc reduced to 85% to those in best conditions during winter, from November to March. These reduction are mainly caused by low temperatures and snows. The work dots not stop in the cold days below 0°C, however it is impossible to estimate the reduction of efficiency due to cold temperature. Further, snow removal on uncovered surface needs another costs. Based on the data of the past few years, the costs of snow removing works arc as follows.

For total surface \$  $362/100yd^2$  of which forassembly \$  $162/100yd^2$  of which forwelding work \$  $200/100yd^2$ 

Table 5-1
Degree of Effect of Weather Change on Productivity by Region
in Percent

| Month    |                   |                |     |     |      |     |     |     |    |     |     |                | ennual  |
|----------|-------------------|----------------|-----|-----|------|-----|-----|-----|----|-----|-----|----------------|---------|
| -Region  | 1                 | 2              | 3   | 4   | 5    | 6   | 7   | 8   | 9  | 10  | 11. | 15             | averago |
| Northern | 85                | 85             | 85  | 90  | 90   | 95  | 100 | 100 | 95 | 90  | 85  | 85             | 90      |
| Central  | 95                | 95             | 95  | 100 | 100  | 100 | 85  | 85  | 85 | 100 | 100 | 95             | 95      |
| :/estern | 95_ <sub>97</sub> | 95 <b>_</b> 97 | 100 | 100 | 1.00 | 90  | ٤5  | 85  | 85 | 100 | 100 | 95 <b>_</b> 97 | 95      |

Note: 100.% denotes the best contitions in each region

Table 5-2: Seasonal Division by region

| Month    | Ton         | Fob   | <br>            | 35000 | T                 | T               |      |               |             |       | Dec. |
|----------|-------------|-------|-----------------|-------|-------------------|-----------------|------|---------------|-------------|-------|------|
| -Region  | ઇસા!        | reo   | ирт.            | erey. | Jun.              | aut.            | Aug. | sap.          | 001         | NOV.  | Dec. |
| Forthern | #int        | er    | <br><b>&gt;</b> |       | · <del>&lt;</del> | Sur             | mer  | $\rightarrow$ | <b>←</b>    | Wint. | er   |
| Central  | ./int       | ;er } |                 | •     |                   | <del>( , </del> | umme | r             | <b></b>     | ۷/غ   | nter |
| Western  | <u>Zint</u> | ;er)  |                 | ,     | <del></del>       | Sun             | mer  |               | <del></del> | Wi    | nter |

In the Shipyard W in Central region, the effect of weather variation, are usually the largest in summer, expecially due to the high temperature and moisture ( of. Table 3-5) and partly due to rain. Monthly productivities during summer arc reduced to 85% to the best efficiencies.

In the shippard X in Western region weather conditions and its effects on productivity arc almost the same as the Central region, except precipitations during summer months.

The effect of weather variations to the best production efficiencies, considered in annual average percentage, are 10% at shipyard in Northern region and 5% at shipyard W and X in the Central and Western regions.

#### 5-3 The Secondary Cost Effect

There is no direct correlation between accidents rate and extreme environment in Japanese shipyards. Here accident rate is defined as the frequency of accident, for which worker has to absent himself from work, to one million working hours. The frequency observed at shipyard W and X in Central and Western regions in shown as Table 5-3. Accident rates are rather high in a fine and comfartable day like spring afternoon. People ususally seem to be more cautious to protect themselves in the extreme working conditions.

Table  $_{5-3}$  Accident frequency at Shipyard W and X 1972.

| Month                 | J    | F    | М | A         | М    | ۲, | J. | A | S | 0 | N | D    |
|-----------------------|------|------|---|-----------|------|----|----|---|---|---|---|------|
| Accident<br>Frequency | 6.35 | 5.01 |   | 7<br>5.20 | 2.35 | 0  | 0  | 0 | 0 | 0 | 0 | 2.80 |
| Rainy days            | 3    | 4    | 4 | 5         | 4    | 6  | 3  | 3 | 4 | 6 | 4 | 2    |

Note; Accident Frequency = Accident x 10 Total working hours

6. Improvement in Productivity after Adoption of Protection Facilities.

### 6.1. Roofs .

As described above, block assembly shops arc only workshops that allow measurement of effect through the adoption of roofs. The results of survey on block assembly shops are given in the Appendix I-Collection of Data, "The results of surveys on roof installment, Table-1-4," and in Table-5, "Effects through Indoorization in major shipyards as of 1970".

Roofing a block assembly shop promises an effect of about 20 to 30% thanks to: (1) Ability to continue work despite rain; (2) shortening of time required for arranging assembly blocks due to improved facilities; and (3) improvement in working environment due to uniformly maintained temperature.

Effect of covering is great in the northern part in winter because it can prevent reduction in efficiency arising from stopping of cranes due to strong winds, snow removing work due to low temperatures.

Covering of pre-erection shops and building docks and berths have been rarely practiced in Japan despite its great effect expected, except newly built giant shipyard like shipyard Y in western region. However, we can not obtain any stable data there at present, because the operation has just begun there in 1972.

#### 6.2. Protection Tools and Facilities

As a direct method protection tools are supplied to cope with bad working environment. According to the results of the questionnaire, this, coupled with improvement in moral of workers, has an effect of about 5% for equipment standards in Table 6 to 9 in Collection of Data.

The estimation of 58 increase in efficiency is based upon

the opinions of experts questioned, for it is further difficult to single out the effect of the adoption of particular protecion tool, say cool suits or portable body warmer on the productivity. These tools, it seems, have a more direct effect upon the motivation to work as whole.

## 6.3. Crane Clamping Devices

A Japanese crane construction standard provides that devices to prevent a crane from speeding and overturning be installed to the crane. It is impossible to calculate the effect on protection units.

6.4 Additional Works Arising from Unfavorable Working Environment and Resultant Reduction in Efficiency

Additional works required in Japan are the following direct and indirect types:

- (1) Wind: e.g., crane clamping
- (2) Rein: e.g., rain protection (temporary awning installation), drying, draining
- (3) Snow: e.g., snow removing
- (4) Heat: e.g., net and cooler installion
- (5) Cold : e.g., heating

Among these works, heating is measurable. This heating work attendent on welding invloves the heating of portions of high tension steel plate and sheet to be welded with a gas burner, etc. to compensate poor welding conditions at low temperature.

According to Table "Results of Survey on Additional Works" in Collection of Data compiling the results of the survey, these heating works reduce efficiency by about 20 % with ordinary welding speed taken as 100 %. The term "heating work" used here does not mean removel of moisture on nor drying a portion to be welded but raising low steel plate temperature to that optimum for welding, that is 300-400F.

Water removal cost in the case of heavy rain can not be extimated seperately.

Table 6-1. Additional Work for welding in low temperature

|            | Heating Method   | Investment               | Decrease of productivity measured by man-hours (1)    |  |
|------------|--|--------------------------|---|--|
| Shipyard X | In welding works on docks and-<br>building berths, worker heat<br>welding points at first<br>through gas-burner heater &<br>then weld immediately.   | \$ 380<br>/ 5<br>heaters | 20% reduction<br>compared to<br>normal weldig<br>work |  |
| Workshop Z | Gas-burner method  | \$ 38<br>/ heater        | 20%   |  |
| Shipyard V | During winter (from November to March) no welding-work in the night (6.00p.m8.00p.m.)  In the winter day time, stop welding works, if temperature is getting low under 23°F  Using gas-burner heater |                          | approximatel:   |  |

- 7. Examples of Productivity Increase through Adoption of Roofs.
- 7.1 On the Job Compositions in the Workshop affected by Weather Protection Devices

The organization of production in the Japanese shipyards has been changed drastically, in recent years, due to the adoption of flow production system. In previous days, workers were allocated and organized by their trades to each workshop. However it became difficult to control workers on production flow and keep good efficiency by such a production organization based on trades. Today, in the most large shipyard in Japan, the production arc reorganized on the stage unit through construction processes and workers who belong to different trades arc mixed up in to a working unit. In the case of Shipyard W in Central region, the composition of trades (jobs) in each production stage is shown in Table 7-1.

Table 7-1 The Composition of Jobs at Shipyard W. (1)

| rabrication | Block            | pre-            | Errection                       |
|-------------|------------------|-----------------|---------------------------------|
|             | Assembly         | Errection (4)   | (on Dock and<br>Building Berth) |
| х           | x                | x               |                                 |
| х           | x                | x               | x .                             |
| X           | х                | x               | x :                             |
| х           | х                | Y               | x                               |
| х           |                  |                 | X                               |
|             |                  |                 | X                               |
|             |                  |                 | v                               |
|             |                  | •               | X                               |
|             |                  |                 | X<br>X                          |
|             | x<br>x<br>x<br>x | X x x x X X X X | Assembly Errection (4)  X       |

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notes:

- (1) X denotes major trades in each stage and x denotes minor trades in it.
  - (2) Fabrication includes gas-cutting, bending and scale removing.
  - (3) including gas cutting, scale removing.
  - (4) Pre-Erection. In this stage, which is between Block Assembly and Errection in some shippard, a larger Block is assembled by uniting two or more small blocks into one. The aim of Pre-Errection stage is to complement the limit of indoorized Block Assembly workshop where larger Blocks can not be assembled due to relatively narrow working surface.

In the Shipyard X there are three major section in the Hull Construction Department, i. e. Hull Fabrication, Block Assembly and Erection (including Pre-Erection stage), and three in the Outfitting Department (Table 7-2). Necessary jobs for Hull Construction Dept. are fifteen, of which welding and maintenance jobs appears in every section, hull assembly, crane operation and rigging, pneumatic service and power jobs appears in two sections. Further the workers who belong to the same job do not make one group in the Section but scattered among working Hull Fabrication Section consists of about 450 workers, which are divided into three Sub-Section (Kakari). One Sub-Section, then, consists of ten Group (Han). Each Group, the smallest working unit, has a forman and fifteen to twenty workers. These working unit themselves, consist of several crafts, i. e. welders, gas cutters, platers, riggers and pneumatic serviceman etc.

Such a mixed composition of multiple jobs in the working organization, will be one of the remarkable chracteristics of Japanese shipyard. All necessary informations to control production processes are based on these mixed working organizations and not on jobs.

Table 7-2 Composition of major job by working section at Shipyard X as of 1972

| Department                               | Hull |          | ruc-<br>_tion | Out | fitt | ing |
|--|------|----------|---------------|-----|------|-----|
| Section                                  | 1    | 2        | ·3            | 4   | 5    | 6   |
| Job                                      | Í    |          |               |     |      |     |
| Hull Fabrication                         | х    |          |               |     |      |     |
| Hull Assembly                            | x    | x        | •             |     |      |     |
| Plater                                   |      |          | х             |     |      |     |
| Welding                                  | x    | x        | х             |     | x    |     |
| Crane Operating & Rigging                |      | x        | х             | х   |      |     |
| Pneumatic Service                        |      | ×        | x             |     |      |     |
| Power                                    | x    |          | х             |     |      |     |
| Maintenance                              | x    | x        | х             | x   | x    |     |
| Slipway Service                          |      |          | х             |     |      |     |
| Inner Fitting                            |      |          |               | x   |      |     |
| Interior Fitting for Living-<br>-Quarter | ·    |          |               |     | x    |     |
| Outer Fitting                            | 1    |          |               |     |      | x   |
| Painting                                 |      | 1        |               |     |      |     |
|  | 1    | <u> </u> |               |     |      | x   |

Note: Section 1: Hull Fabrication

2: Block Assembly

3: Erection

4: Inner Fitting

5: Super Structure

" 6: Hold

Further, there is a trend to multiple workmanship in the smallest working unit.

Every worker has been trained in and has, at least, one qualified skill necessary for shipbuilding works. However, in recent years, there is a remarkable trend to have multiple skills or qualifications among worker. For example, welders in Hull Construction Department usually have other related skill, i. e. qualification as plater. Platers, in turn, can have gas cutters skill.

7.2 Available Measures on Efficiency for This Study

The measures on efficiency that are used as produce
tion management indexes, daily or monthly, in each Department, depend naturally on the type of working organizations.

In the shippard surveyed, man-hours per ton of constructed ship and/or volume of steels fabricated per month are used as measure on efficiency.

Data that show differences of efficiencies by trades do not exist, because of multi-trades working unit already mentioned.

Any physical measure like welding lengths per man per shift can not be obtained unless one carry out special observation beside the production line. It is impossible for us to do such special observations within limited term and thus we have to relied upon available existing informations on efficiencies.

## 7.3 Example A.

We have obtained during our survey man-hours statistics at particular workshop, i.e. Block Assembly Shop at Shipyard X. In this shop the surface was uncovered in 1968, where roofs were installed in 1970. We calculated the productivity increase using these man-hours data as a clue.

Table 7-3..Areas covered under roof ( 1970 )

| Block Assembly shop | (1) Total Area<br>sq. ft. | (2) Covered sq. ft. | (3) Covered ratio. (2)/(1)x100 |  |
|---------------------|---------------------------|---------------------|--------------------------------|--|
| A                   | 41,980                    | 26,910              | 64%                            |  |
| В                   | 11,840                    | 7,104               | 60%                            |  |
| C                   | C 16,146                  |                     | , 63%                          |  |
| Total               | 69,966                    | 44,240              | 63%                            |  |

Table 7-4 Productivity measures recorded, in 1968, in the term of man-hours per square meteres of Block Assembly shops listed bellow.

| Block<br>Assembly<br>shop | man-hours<br>consumed on<br>the area(H/Y) | of which<br>welding<br>man-hours | ·  | number of<br>workers in<br>average(man) |
|---------------------------|---|----------------------------------|----|---|
| A                         | 136,800                                   | 84,820                           | 62 | 50                                      |
| В                         | 86,400                                    | 47,520                           | 55 | 30                                      |
| C                         | 172,800                                   | 96,770                           | 56 | 70                                      |
| Total ·                   | 396,000                                   | 229,110                          | 58 | 150                                     |

note: These man-hours were consumed on the uncovered area in 1968 where rocfs were installed in 1970. Therefore, 396,000 hours are corresponding to the covered 44,240 ft<sup>2</sup> in 1970 in Block Assembly Shops A.B.C.

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| •  |   | days or hours<br>affected per worker | total loss time<br>( hours ) | remarks   |
|----|---|--------------------------------------|------------------------------|---|
| 1) | Fully idle days   | 22 days                              | 42,420                       | The days, precipitation is over int/H at 08:30 a.m. and all workers are ordered to back home.                                       |
| 2) | Interruption of welding works only  | 86 hours                             | 12,242                       | The days, precipitation became over   |
| 3) | Interrution of all works  | 88 hours                             | 12,242                       | The days, precipitation became over occupill after beginning of operation.  |
| 4) | Reduction of efficiencies due to the drizzling rains and interruption listed above in related works | 50 hours                             | 9,356                        | In drizzling rains, that are under occupation, all works can be continued. However there occur efficiency reduction in some degree. |
|    | Total   |                                      | 64,018                       |   |

In 1970, the uncovered area above mentioned in this Block Assembly Shop was covered by roofs and thus they could eliminate the loss times due **to** the rain that amounted to 64,018 hours in 1968. The loss rate of working hours in 1968 can be obtained by a ratio of total loss times to total man-hours at that year on the particular area in Block Assembly Shop. This was 16% annually, i.e.

loss time ratio= Total loss times x 100%
Total man-hours

64,018 x=16.2% 396,000

We can read approximately this loss time ratio as productivity increase ratio by the adoption of roofs over these particular area of Block Assembly Shop. because that when roofs were installed over the area, the production methods there were changed drastically. The most significant change must be taken place in the type of cranes, i.e. from jib type to overhead travelling one and consequently in their handling and lifting capacities. This leads to other changes in supplying and handling procedures of sheets and pieces on the production lines, in distribution and location of tools, e.g. those for cutting and welding and total number of workers on the area. Therefore even if we obtain the productivity figures for 1970 at the same workshop, we should not compare this figure with those of 1968 to estimate the effects due to the installation of roofs. The above estimated gains of 16.2% can be considered as the most conservatively calculated figure based on the conditions that there is no change except roofs in the production methods.

#### 7- 4. Example B.

As we already described in Section 2.3, the "indoorization" process had begun in some Japanese Shipyard as early as on later half of 1950's. At that time, the engineers in Shipyard IV estimated the productivity gains if they installed roofs over Block Assembly Shop. The basis of estimation and the result are as follows. The estimation had been made on the data of seven months from April to October 1957. The estimation was based on the production volume per hours and production reduction due to rain was calculated 23.6% (Wr/Wf x 100).

In this case the differences of man-hours consumed due to the different size and type of ships were assumed to have no significant effect upon production volume. It was assumed, too, the necessary man-powers were always supplied to the workshop to keep the marginal production capacities.

The introduction of roof over this workshop eliminated the reduction of production due to rain. However we have to add further gains, i.e. reduction of piece stock for rain and changes in crane capacity and production methods.

This old estimation can be used as standard and classical calculation on the effect of rains.

### Basis of estimation

(A) Reduction of Prodction due to rain

Wr=K X R

here K=

H-(R+E)

Wr=Reduction of Production due to rain

R=Loss time due to rain

W=Production Volume

K=Production Volume per hour in net working hours

H=Total working hours E=Loss time due to labour dispute

H is defined as

H=Hw-Hh+'H'h

here

Hw=Total working days x normal working hour per day Hh=Total holidays x normal working hour per day

H'h=Total working days in holiday x normal working hour per day

n= Operation ratio in holiday

 $= \frac{m}{H''} \cdot \frac{1}{M}$ 

here m=Total workers who work in holiday

M=Average of workers in weekday

H"=Total working days in holiday

R is defined as

R=Rw-Rh+ηR'h

here

Rw=Total rainy hours in normal working hours

Rh=Total rainy hours in holiday

R'h=Total rainy hours in working hours in holiday

E is defined as

E=Ed+Ei

here Ed=Direct loss time due to labour dispute Ei=Indirect loss time due to labour dispute

(B) Reduction of Production due to labour dispute (We)

We= $K \times E$ 

(C) Operation capacity of Block Assembly Shop (Wf)

#### Wf=W+Wr+We

here wf is defined as normal production volume on Block Assembly Shop if there occur no rainy days and Iabour disputes

(D) Normal working hours was nine hours per day, i.e. 8.00am-noon, 1.00pm-6.00pm.

hin 7-6 Effects of rains to Block Assembly Shop

Observed at Shipyard W during 7 months (April to October) 1957.

| tonth     | Total working<br>hours ( h ) | loss time due<br>to rains (h)<br>(R) | loss time due<br>to labor dis-<br>pute ( h ) (E) | Volume of prod<br>per month<br>( tons )(%) | per hour (t) | Losses due to<br>rains ( t)<br>(Nr) | losses due to<br>labor dispute<br>( t ) | Full capacity when Nr=0 Re=0(t) [wi) |
|-----------|------------------------------|--------------------------------------|--|--|--------------|-------------------------------------|---|--------------------------------------|
| April     | 243.0                        | 53.5                                 | 0  | 5641                                       | 29.7         | 1590                                | 0                                       | 7231                                 |
| ::y       | 248.4                        | 69.0                                 | 0  | 5427                                       | 30.2         | 2080                                | 0                                       | 7507                                 |
| June      | 235.8                        | 62.2                                 | 0  | . 50\$6                                    | 29.1         | 1805                                | 0                                       | 631.1                                |
| July      | 239.0                        | 73.9                                 | 38.5   | 3662                                       | 28.9         | 2140                                | 1115.0                                  | 6917                                 |
| .'ugust   | 243.4                        | 21.0                                 | 0  | 6042                                       | 27.2         | 572                                 | . 0                                     | 6614                                 |
| September | 241.6                        | 96.5                                 | 0  | 4074                                       | 28.2         | 2720                                | 0                                       | 6794                                 |
| Catober   | 249.9                        | 25.3                                 | 14   | 6118 -                                     | 29.2         | 740                                 | 406.0                                   | 6853                                 |
| .iverage  | 243.0                        | 57.3                                 | 7.5  | 5145.7                                     | 28.9         | 1655.0                              | 217.0                                   | 7017.7                               |

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8. Weather Protection Devices ,in the Heavy Equipment Industries.

#### 8-1. Description of Workshop Z

As we have already described in our Research Proposal, we restrict the scope of heavy-equipment and construction industries to be studied to the works which are carried out within the same enterprises with shipyards as a field of their diversified operation.

We have selected a large scale construction shop, workshop Z, that is located beside shippard W in central region of Japan. Weather variations in Workshop Z is the same with that of shippard W. (cf. 3. seq.)

The products in this workshop Z are steel bridge, highway structure, water sluice gate, hydraulic pipe, parking facilities and steel frame for building etc.

#### 8-2. Weather protection devices adopted.

The surface of this workshop Z is not covered by roofs, exports a part of paint shop, that has a floor space of 30,030 ft<sup>2</sup> of which 3,305 ft<sup>2</sup>,i.e. 11% of space is now covered by roof ( the data of which are given in Table 4, Collection of Data.) Protection devices adopted other than roof are 1) heater,

2) Sunnet, 3) Water cooler and 4) Winter Cloth.

heating devices that were introduced since 1968, were small portable gas-stoves to heat workers in the closed section of steel structure on the ground (cf. Table-7, Collection of Data and photograph No. 15). Sunnet were used since 1957 to shade workers from direct sunshine during summer. At present nets are made of nylon and have different size according to the places to be used. Water cooler that is shown in photograph No.17, commercially available ordinary one to serve workers on work surface in summer. Winter cloth (photograph 18) are supplied for rent, without fee, for every workers

during winter. The cranes on this work surface have same clamping devices as those of shippards and the types and costs are shown in the Table-11 and 12, Collection of Data.

## 8.3. Their effects on productivity...

The use of protection devices are limitted to rather simple ones like portable stoves, water-coolers and winter cloth. Thus, their effects on productivity can not be singled out and, it seems, have good effect on the moral of workers in some degree.

In this workshop, preheating of welding points are usually done by gas-burner method in low temperature. These additional works for welding usually reduce the productivity measured by man-hours by about 20%. (cf. Table. 6-1. in the Report).

9 The distribution of shipbuilding costs in Japan

#### 9-1 The method of estimation

The shipbuilding cost usually differ from the type and size of ship and from the conditions on which shippard operates. Although tankers are the largest single type of ships that are constructed in Japan, there are wide variety of ships constructed among 25 major shippards here, and it is impossible to get average figures on the shipbuilding costs. Another difficulty arises from the fact that the field of business of the most shipbuilding enterprises? have been diversified significantly in recent years, and distort cost figures appeared in company's annual financial statements.

Consequently, we select two shipbuilding companies whose manufacturing activities concentrate on shipbuilding and especially on single type of ship, so as to get relatively stable and reliable cost pictures. The figures base on the financial statement of these companies.

#### 9-2. The distribution of shipbuilding costs

The shipbuilding company A has only a large shipyard in western region, according to climate classification used in this report, and the sales of shipbuilding department accounts for 82% of the annual company sales in 1971. The three fourth of shipbuilding sales comes from new construction and one fourth comes from reparting. The main product here is large tanker of 200,000 dwt.

The shipbuilding company B has also one major shippard in northern region and the share of shipbuilding accounts for 88% of total annual sales in 1971. New construction was 94% of total shipbuilding sales in this year. The main

product in this company is small bulk-carriers from 25,000 tons to 28,000 tons in deadweight.

As for the cost items, Raw Material is including subcontractors and purchasing, Overhead is including the cost for capital components and salaries in general and administrative departments.

The distribution of costs in 1971 are shown in the Table 7-1, Raw Materials item accounts for about the half and Labour cost for slightly under 20%, whereas the Overhead is over 30%.

Table 9-1. The Distribution of Shipbuilding Costs compared with other Manufacturing Industries in Japan. 1971 (%)

|       |                     | ·       |                    |   |
|-------|---------------------|---------|--------------------|---|
| otal  | Overhead<br>charges | Labours | Raw Mate-<br>rials | Cost items Shipyards Industries   |
| 100.0 | 30.9                | ]9.8    | 49.1               | Shipbuilding Co. A  |
| 100.0 | 33.6                | 15.8    | 50.4               | Shipbuilding Co. B  |
| 100.0 | 22.8                | 16.9    | 60.3               | . Machinery Industry (except electrical)  |
| 100.0 | 27.1                | 21.1    | 51.8               | Electrical Machinery<br>for Industrial Use                                      |
| 100.0 | 22.8                | 16.9    | 60.3               | Railway lacomotives   |
|       | 22.8                | 21.1    | 51.8               | Machinery Industry (except electrical)  Electrical Machinery for Industrial Use |

SOURCE: Mitsubishi Research Institute, Kigyo keiei no Bunseki (Financial Analysis of Japanese Corporations),
No. 38, Dee, 1972.

Appendix H-1

Collection of Data

#### Appendix H-1.

Collection of Data
Explanatory Note to Table of Protection Facilities

(1) The results of survey on rool installment Table-1. Work environment with roofs Type of workshop: No.1.

Table-2 do: No.2.
Table-3 do: No.3
Table-4 do: No.4

- (2) Table-5 Effects through "Indoorization" in major shippards as of 1970.
- (3) The results of survey on protection facilities and devices Table-6 Work environment-heat and cold protection facilities, Type of workshop: No.1.

Table-7 do: No.2
Table-8 do: NO.3
Tab2e-9 do: No.4

(4) The results of survey on czane protection Table-10 Protective equipment exclusively for cranes,

Type of crane No.2
Table-11 do: No.3
Table-12 do: No.4

# Explanatory Note to Table of . Protection facilities

| Items                          | Definitions  | Remarks   |
|--------------------------------|--|---|
| 1. Type of Workshop            | <ol> <li>Block Assembly</li> <li>Pre-Erection (Grand Assembly)</li> <li>Erection</li> <li>Coating</li> </ol>   | on dock or building berth                               |
| 2. Type of Roof                | <ol> <li>Permanent building, wholly closed</li> <li>", with travelling roof</li> <li>Permanent building with roof, not wholly closed.</li> <li>Travelling roof</li> </ol>  |   |
| 3. Covered Area                | 1. Covered ratio of Block Assemble Square meter of indoorized as Square meter of total of as:  2. Covered ratio of Pre-Erection Square meter of indoorized as Square meter of total pre-ex  3. Covered ratio of Building Ber Square meter of covered area Square meter of Building ber | Shop= pre-crection surface rection surface th and Dock= |
| 4. Type of Acquisition (Roof)  | 1. Owened 2. Rental  | •   |
| 5. Capital<br>Costs<br>( Roof) | Building Construction Cost+ Civil Engineering Cost and - Cost for Auxiliary Facilities   |   |

# . Explanatory Note (continued)

|  | <del></del>                       |  |         |
|--|-----------------------------------|--|---------|
|  | Items                             | Definitions  | Remarks |
| 6.   | Operating<br>Cost                 | Yearly maintenance cost  for particular covered area   |         |
| 7.   | Type of<br>Protection<br>Devices. | 1. Ventilating Fan. 2. Air Conditioner & Stoves 3. Water Cooler 4. Winter Cloth 5. Sunnet 6. Cool Suits.     | ·       |
| 8.   | Type of<br>Utili-<br>zation       | <ol> <li>Supplied as standard equipment<br/>to workers</li> <li>Lended when need arises</li> </ol>           |         |
| 9.   | Capital<br>Cost<br>(Devices)      | Costs to introduce or purchase the devices   |         |
| 10.  | Operating<br>(Devices)            | Yearly replacement costs   | •       |
| 11.  | Type of cranes                    | <ol> <li>Overhead traveling crane</li> <li>Bridge crane</li> <li>Jib crane</li> <li>Goliath crane</li> </ol> |         |
| 12.  | Crane capacity                    | Lifting capacity .   |         |
| 13.  | Type of workshop                  | same as Item 1.  |         |
| 14.  | Type of protection methods.       | <ol> <li>Rail clamping</li> <li>Hooking</li> <li>Pin drop</li> <li>Guy wire</li> </ol>                       |         |
| <u>.                                    </u> | Operating costs                   | Yearly main-tenance costs for particular protection method   |         |

(1) The results of enquete on roof installment
Table 1. Work environment with roofs
Type of workshop: No.1

| Shipyard | Floor space<br>of work <sub>2</sub><br>shop,ft | Covered ft2       | £8,£1.84)  | Tresita | TEGUL Elever                 | Carital<br>Costs<br>S per ft <sup>2</sup> | Operating<br>Sper/year | Peacriptic<br>Code<br>number of<br>photos | and facilities specification of structures     |
|----------|--|-------------------|------------|---------|------------------------------|---|------------------------|---|--|
| ¥        | 39,611   | 35,305            | 89         | 1       |                              | •   |                        | 1.2.                                      | steel structure,<br>ralvanised iron .<br>sheet |
| ×        | 85,357<br>143,697                              | 85,357<br>143,697 | 100<br>100 | 1:3     |                              | 14.55<br>14.12                            | 6,004<br>10,260        | 1:2:3.                                    | *; *   |
| Y        | 775,600  | 775,600           | 100        | 1       |                              | 11.72                                     |                        | 1.2                                       | steel structure,<br>colored itom sheet         |
| W        | 27,986   | 27,986            | 100        | 2       |                              | 15,88                                     |                        | 4.5.6.                                    | steel structure,<br>long colored iron<br>sheet |
| ٧        | 25,833   | 25,833            | 100        | 2       | 1                            | 14.12                                     |                        | 4,5.6.                                    | steel structure,<br>slated roof,               |
| X        | 37,027   | 37,027            | 1,00       | 2       |                              | 8.82                                      | 2,622                  | 4.5.6.                                    | steel structure,<br>galva ised iron<br>sheet   |
| Y        | 62,107   | 62,107            | 100        | 2       |                              | 15.42                                     |                        | 4.5.6.                                    | steel structure,<br>colored iron sheet         |
| ¥        | 91,008   | 59,944            | 66         | •       | ,                            | 3.53                                      |                        | 7.8.                                      | Eslon(Corrugated vinylchloride residence)      |
| ¥        | 62,377   | 12,378            | 20         | •       |                              | 12.36                                     |                        | 7.8,                                      | steel structure,<br>selvanized from<br>sheet,  |
| x        | 52,635   | 20,666            | 40         |         | 1.                           | 2.12                                      | 1,444                  | 7.0                                       | steel structure,<br>galvanized iron<br>sheet,  |
| Ŷ        | -  | -                 |            | ·       |                              |   |                        |   | readily movable<br>bounet roof                 |
| tetal    | 1,403,238                                      | 1,285,905         | 92         |         | ise in produc<br>30 percent. | fivity by co                              | vering in t            | Pe. cases and                             | unts to  |

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table 2. Nork environment with roofs
Type of wrokshop: No.2

| Shipyard | Floor space<br>of workshop |                 | Covered rate | Type of covering | Type of acquisition | ' '   | costs<br>\$ per year | Description of facilities |  |  |
|----------|----------------------------|-----------------|--------------|------------------|---------------------|-------|----------------------|---------------------------|--|--|
|          | ft <sup>2</sup>            | ft <sup>2</sup> | (\$)         |                  |                     |       |                      | number                    | specifi-<br>cation of<br>structure           |  |
| Y        | 447,503                    | 97,682          | 21           |                  | 1                   | 15.42 | •                    |                           | steel<br>structure,<br>colored<br>iron sheet |  |
|          | ·                          |                 |              |                  |                     |       |                      |                           |  |  |
| total    | 447,508                    | 9,075           | 21           |                  |                     |       |                      |                           | •  |  |

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table 3. . Mork environment with roofs Thpe of wrokshop: No. 3

| Shipyard | Floor space<br>of workshop | space           | Covered rate | Type of covering | Type of acquisition |        | Operating costs | Description of facilities |  |  |
|----------|----------------------------|-----------------|--------------|------------------|---------------------|--------|-----------------|---------------------------|--|--|
|          | ft <sup>2</sup>            | ft <sup>2</sup> | (8).         | (\$)             |                     |        | \$ per year     | number                    | specifi<br>cation of<br>structure          |  |
| Υ.       | 1,130,206                  | 107,640         | . 10         | 4                | 1                   | .25.60 | :               | 7.8<br>·                  | steel<br>structure<br>colored<br>iron shee |  |
| ٠        |                            |                 |              |                  | •••                 |        |                 |                           |  |  |
| total    | 1,113,206                  | 107,640         | 10           |                  |                     |        |                 |                           |  |  |

table 4. Nork environment with roofs
Thps of wrokshop: No.4.

| [ | Shipyard | Floor space of workshop | Covered space   | Covered<br>rate<br>(%) | Type of covering | Type of acquisition                     |              | Operating costs \$ per year | Description of facilities |   |  |
|---|----------|-------------------------|-----------------|------------------------|------------------|---|--------------|-----------------------------|---------------------------|---|--|
|   |          | ft <sup>2</sup>         | ft <sup>2</sup> |                        | 1,               |   | <b>,</b> ,,, |                             |                           | specifi<br>cation of<br>structure               |  |
|   | Υ.       | 80, 730                 | 80,730          | 100                    | 1                |   | 9.00         |                             |                           | steel<br>structure,<br>colored<br>iron sheet    |  |
| • | X        | 35,520                  | 35,520          | 100                    | 2                | <b>1</b> .                              | 15.88        | 2,508                       | !.                        | steel<br>structure,<br>galvarized<br>iron sheet |  |
| - | Z        | , 30,000                | 3,300           | 11 .                   | . 2              | • | 30.18        | 1,140 .                     | 9. 10                     | 11 11   |  |
| _ | W        | 30,250 ·                | 21,530          | 71                     | 4                |   | 8.93         | - •                         | 11. 12                    | 19  |  |
| - | total    | 176,500                 | 141,080         | 80                     |                  | <u> </u>                                | •            |                             | ļ                         | ·   |  |

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#### (2) Table 5.

Effects through "Indoorization" in major shipyards as of 1970.

| Region  | Shipyard | Increase of floor use rate (1) (1) | Reduction of manhours(%)        | Remarks  |
|---------|----------|------------------------------------|---------------------------------|--|
| North-  | v ·      | 40 .                               | 20                              |  |
| ern     | E        | 10-15                              | 5(only for<br>outdoor<br>works) |  |
|         | W        | 30                                 | 15                              |  |
|         | L        | 20 -25                             | 15                              |  |
| Central | K        | 20                                 | . 15                            |  |
| ~       | J        | in somedegre                       | ec 10                           | plus improved<br>ment in<br>working<br>environment |
|         | 0.       | 20                                 | 15 6                            | increase in  |
| Yana    | P ,      | 100(in final<br>assembli           | 30                              | safety and quality through                         |
| Western | x        | 10                                 | 10                              | improvement in working conditions.                 |

- Note: (1) ratio of fabricated steel in tons persquare meters of assembling yards. This ratio does not directly correspond to the annual increase rate of production capacity. By increasing floor use rate at particular workshop, additional works could be done, if other poduction factors, especially manpowers, were provided to carry out this additional works. Empirically, annual increase of production capacity rather corresponds to the rate of reduction of man-hour consumed.
  - (2) man-hours per tons of ships constructed.

Source: Nihon Zosen Kogyokai (Shipbuilders' Association of Japan)

(5) The results of survey on protection facilities and devices

Table 6. Work environment-heat and cold protection facilities

Type of workshop: No. 1

| orkshop          | Type of                       | Standard  | Type of    | Capit  | al Costs                 | •                                   | Operati | on Costs                 | 1            | specifi-                                 |         |
|------------------|-------------------------------|---|------------|--|--------------------------|-------------------------------------|---------|--------------------------|--------------|--|---------|
| -                | protection<br>facili-<br>ties | of equip<br>ment<br>(number<br>of units<br>per<br>person) | tion       | number of facili- ties (number of unit per person) | unit /<br>(<br>./unit)   | total<br>cost<br>(\$)               | nuaber  | cost per<br>unit<br>(\$) |              | carion<br>Code<br>number<br>of<br>photos | renarks |
| X<br>Y<br>X      | 1                             | 0.25<br>0.20<br>0.42                                      | 1          | 0.248<br>0.195<br>0.420                            | 357.2<br>407.0<br>-357.2 | 52151.2<br>52320.0<br>46793.2       | -       | √357.2<br>38.0           | 9.11<br>6.70 | 13.14<br>13.15<br>13.14                  |         |
| ÿ                | 2 2                           | 0.02  | <u>·1</u>  | 0.022<br>0.193                                     | . 60:8                   | 2158:4                              | 0.022   | 11.4                     | 0.25         | 13                                       |         |
| X<br>Y<br>W<br>y | 3                             | 0.04<br>0.03<br>0.03<br>0.08                              | 1          | 0.036<br>0.027<br>0.048<br>0.008                   | 190<br>247<br>190<br>171 | 3590.0<br>5187.0<br>2850.0<br>342   | 0.003   | 19.0                     | 2,65<br>0.91 | 15<br>17<br>17<br>17<br>17               |         |
| ,,               | 4.                            | 0.01 .  | 1          | 0.013<br>1.000                                     | 13.3                     | 133.0<br>2660.0                     | -       |                          | •            | 16<br>18<br>18                           |         |
| - × -            |                               | 0.02<br>0.03<br>0.14<br>0.08                              | - <u>i</u> | 0.017<br>0.032<br>0.136<br>0.077                   | •· 38                    | 159.6<br>-159.6<br>3040.0<br>1824.0 | 0.014   | 38.0                     | •            | 19                                       |         |
| 16               |                               | 0   | 1          | )  |                          | •                                   | ٠       | ••                       | •            | 19                                       |         |

(3) The results of surveyon protection facilities and devices

Table .7. Work environment-heat and cold protection facilities

Type of workshop: No.2

| works       | ihop | Type of protection facilities | Standard of equip ment (number of units per person) | acquisi<br>tion | number                  | unit<br>(\$/unit)         | total<br>cost<br>(\$) | number of supple- [mented] | (\$'unit)      | cost:-<br>per<br>unit<br>(\$/ | Code<br>number   | remarks |
|-------------|------|-------------------------------|---|-----------------|-------------------------|---------------------------|-----------------------|----------------------------|----------------|-------------------------------|------------------|---------|
| Y           |      | 1                             | 0.14<br>0.19  | 1               | 0.143<br>0.194          | 357.2<br>368.6            | 12160                 | 0.014                      | 357.2          | 2.33                          | 13.14<br>· 13.14 |         |
| X<br>X<br>Z |      | 3                             | 0.05<br>0.02<br>0.08                                | 1               | 0.050<br>0.024<br>0.083 | 190.0                     |                       | 0.042                      | 72.2           | 0.95<br>1.20                  | 15<br>17         |         |
| Z           |      | -4<br>-5                      | 0.07<br>1.00<br>0.04                                | 1 2 .           | 0.071                   | .13.3                     | 159.0<br>490          | 0.233                      | 11.4           | 2.65                          | 17<br>18<br>18   |         |
|             |      | 6                             | 0.27  | 1               | 0.048<br>0.267<br>0.236 | -15-96<br>-15-96<br>-38-0 | 509.2                 | 0.005<br>0.033<br>0.029    | 15.96<br>15.96 | 1.09                          | 19               |         |

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(3) The results of enquete on protection facilities and devices

Table 8. Work environment-heat and cold protection facilities

Type of workshop: No.3

|      | Corkshop    | Type of | Standard  | Type of | Capit  | al Costs                   |                          |   | on Costs         | \                                 | specifi-                                 |         |
|------|-------------|---------|---|---------|--|----------------------------|--------------------------|---|------------------|-----------------------------------|--|---------|
| н_75 |             | tion    | of equip<br>ment<br>(number<br>of units<br>per<br>person) | !tion   | number of facili- ties (number of unit per person) | unit<br>( \$<br>/unit)     | cost<br>( \$             | number of supple- imented facili- ties (number of units per | ( \$             | cost per unit (\$ / person/ year) | cation<br>Code<br>number<br>of<br>photos | remarks |
| -    | х           |         | 0.28  |         | 0 250  | 754 %                      | 00700                    | person)   |                  |                                   |  |         |
|      | Y<br>W      | 1       | 0.17<br>0.30  | _       | 0.278<br>0.168<br>0.302                            | 357.2<br>541.9.<br>357.2   | 89300<br>109440<br>57152 | 0.028   | 357,2<br>-<br>38 | 9.94<br>3.58                      | 14<br>14<br>14                           |         |
|      | Х<br>       | 2       | $\frac{0.51}{0.02}$                                       |         | 0.310  | 342.0_                     | 40356_                   |   |                  | -                                 | 14                                       |         |
|      | W<br>V      | 2 cools | 0.02<br>er0.02<br>0.05                                    | 2.      |  | 11400.0<br>11400.0<br>38.0 | 159600<br>91200<br>760   | -   | •                | -                                 | 16<br>· 16<br>15                         |         |
|      | X<br>Y<br>W | 3       | 0.03<br>0.02<br>0.03                                      | 1       | 0.026<br>0.023                                     | 190<br>247                 | 4370.<br>6916            | -   | 190              | 0.42                              | 17                                       |         |
|      | ,;<br>Y     |         | 0.02  | 1       | 0.026<br>0.016                                     | 190<br>_114                | 684                      |   | 19               | 0.50                              | 17<br>17                                 |         |
|      | W<br>V      | 4       | 0.10<br>0.57<br>1.00                                      | 1       | 0.008<br>0.566<br>1.000                            | 13.3<br>8.7<br>19          | 1569.<br>2622<br>2869    | 4 -   |                  |                                   | 18<br>18<br>18                           |         |
|      | X<br>i;     | 5       | 0.33<br>0.77  | 1       | 0.334<br>0.774                                     | 15.96<br>15.96             | 4788                     | 0.033   | 15.96            | 0.53                              | -  |         |
|      | X<br>X      | 6       | 0.61  |         | 0.612<br>0.057                                     | 38<br>45.6                 | 20900<br>1369            |   |                  | 2.33                              | ] 9<br>19                                | •       |

(3) The results of survey. on protection facilities and devices

Table 9. Work encironment-heat and cold protection facilities

Type of workshop: No.4

| Workshop              | protection<br>facili- | Standard of equip ment (number of units per person) | Type of acquisi tion | number<br>of<br>facili-<br>ties                    | cost per<br>unit<br>(\$ /unit) | cost<br>(\$)  | number<br>of<br>supple-<br>mented | (\$./unit) | cost<br>per<br>unit<br>( c / | specifi-<br>cation<br>Code<br>number<br>of<br>photos | remarks |
|-----------------------|-----------------------|---|----------------------|--|--------------------------------|---|-----------------------------------|------------|------------------------------|--|---------|
| Y<br>W<br>W<br>Y<br>Y | 1<br>2<br>3 .         | 3.14<br>0.80<br>0.20<br>0.06<br>0.05<br>3.00        | 1<br>1<br>1          | 3.140<br>0.800<br>0.200<br>0.060<br>0.050<br>3.000 | 050                            | 65,888.<br>15,200<br>9,120.<br>741.<br>190<br>4,560 | ! <u>-</u>                        | 190        | 9.5                          | 13.14<br>13.14<br>15.<br>17<br>17<br>19              |         |

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(4) the results of survey: on crane protection

Table. 10Protective equipment exclusively for cranes
Type of crane: No. 7.

| Workshop | Capacity<br>of crane | Place of equip- | Type of protective equipment | Total of capital | Operating costs ( \$ per year) | Protective code number of photos | equipment<br> specification<br> of structure |
|----------|----------------------|-----------------|------------------------------|------------------|--------------------------------|----------------------------------|--|
| 1        | 31T                  |                 | 1                            | 775.2            | 26.6                           | 20                               | steel  |
| W .      | 40T                  | 1               | 1.3.                         | 615.6            | 26.6                           | 20.23.24                         | *1   |
| <u> </u> | 10T                  |                 | . 3                          |                  | 26.6                           | 23.24                            | 11   |
|          | -                    |                 |                              |                  |                                |                                  |  |

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| Workshop | Capacity of crane                         | Place of<br>equip-<br>ment | Type of protective equipment | Total of capital                   | Operating costs ( \$ per year) | Protective code number of photos                | equipment<br>specification<br>of structure |
|----------|---|----------------------------|------------------------------|------------------------------------|--------------------------------|---|--|
| w _      | 80T/40T<br>40T/15T<br>20T/10T<br>125T/25T | 3<br>1<br>- 3              | 1.3.4.<br>1.3.4.<br>1.4.     | 2,2°3.4<br>2,247.8<br>965.2        | 83.6<br>                       | 20.23.24<br>20.23.24.25<br>20.23.24.25<br>20.25 | steel                                      |
| Х        | 103<br>103                                | 1                          | 2                            | 7,220<br>5,700<br>836<br>9,120     | -                              | 21.22<br>21.22                                  | 11<br>11                                   |
| W        | 6T/3T                                     | 3                          | 2.4.                         | 836                                | ن.197                          | 21.22.25  | 11   |
| Y        | 1007/507<br>357/107<br>207/107<br>107/57  | 2<br>3<br>2<br>3           | 3                            | 9,120<br>13,490<br>9,120<br>13,300 | 494.0<br>190.0<br>133          | 23.24   | 11<br>11<br>11                             |
| W        | 901/45T<br>801/35T<br>10T                 | 3<br>1. 3                  | 3                            | 14,440<br>11,488                   | .83.6                          | 11 11<br>11 11<br>11 11                         | 11<br>11<br>11                             |
| 2 .      | 20T/7.5T<br>15T/7.5T                      | 2                          | 3                            | 608<br>608                         | 60.8                           | 11 11<br>11 11 .                                | 11   |
| v .      | 80T<br>50T<br>40T<br>45T<br>25T           | 3                          | 3                            | -                                  |                                | 11 11<br>11 11<br>11 11<br>11 11<br>11 11       | 11<br>11<br>11<br>11<br>11                 |
| 1        | TOT                                       | 1                          |                              | -                                  | -                              | ,, 11   | 11   |

(3) the results of survey on crane protection

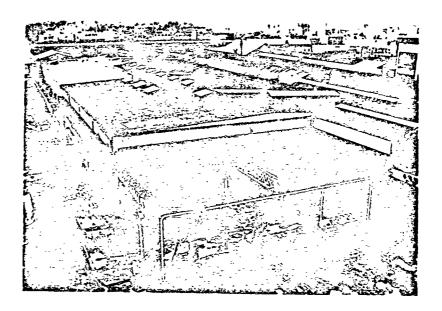
Table 12 Protective equipment exclusively for cranes
Type of crane: No.4

|      | Workshop | Capacity<br>of crane | Place of equip-ment | Type of protective equipment | Total of capital cost | Operating costs ( \$ per, year) |                | pment<br>cification<br>structure |
|------|----------|----------------------|---------------------|------------------------------|-----------------------|---------------------------------|----------------|----------------------------------|
| =    | <u>Y</u> | 600T                 | 3                   | 1.2.3.                       |                       | 912                             | 20.21 22 23 24 | steel                            |
| н-79 |          | 20T                  | 2                   |                              | 4,180                 | -                               | 21.22          | 11                               |
| _    | X        | 3001                 |                     | 2                            | 23,560                | -                               | tı             | fi                               |
|      |          | 120T                 | 3                   |                              | 9,652                 | -                               | 11             | 11                               |
|      |          | 80T                  | 7                   | •                            | 8,170                 | •                               | 11             | 11                               |
|      | Z        | 20T                  | 2                   | 4                            | 1,026                 | ., 49.4                         | 25             | 11                               |
|      |          |                      |                     |                              |                       |                                 |                |                                  |

#### Appendix H-2

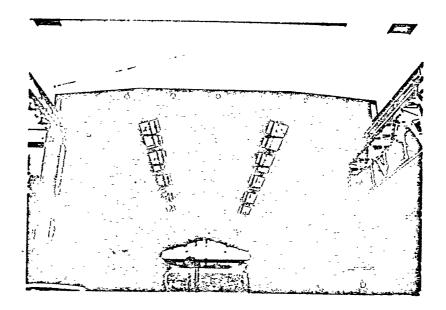
Photographed of Facilities and Devices.

( Each number under pictures denote code number in the Tables in Appendix H-1, all pictures were taken during our survey on December and January 1973.)

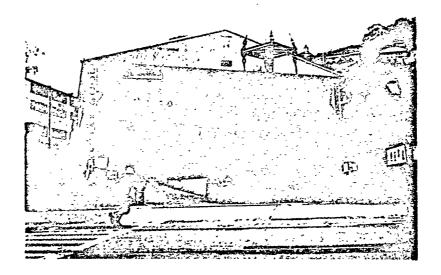


1. Roofed Block Assembly shop at Shipyard W in the Central region of Japan. Type of roof: permanent building, wholly closed.

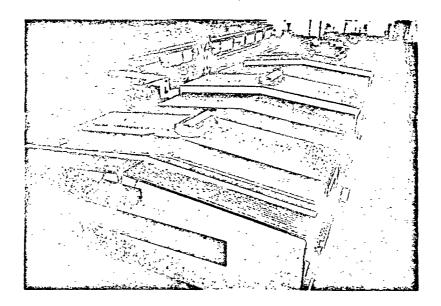
11



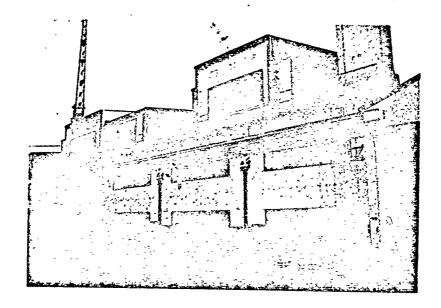
 Roofed Block Assembly shop at Shippard X in the Western region. Type of roof: same to 1.



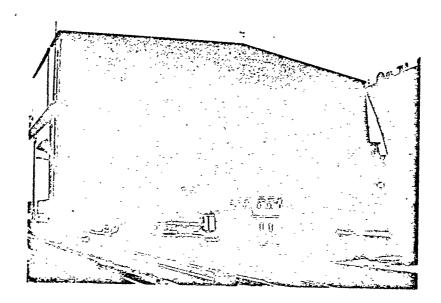
3. An assembled block is carried out from roofed Block Assembly shop at Shipyard X.



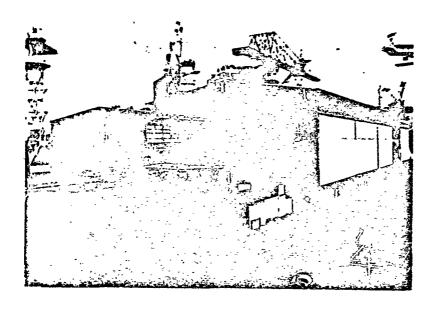
4. Block Assembly shop with travelling roof at Shipyard X. Type of roof: permanent building, wholly closed, with travelling roof.



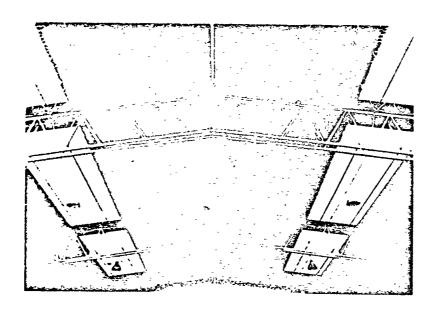
 Block Assembly shop with travelling roof at Shipyard X. Type of roof: permanent building, wholly closed, with travelling roof.



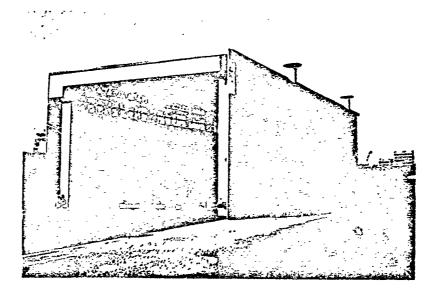
6. Block Assembly shop with travelling roof at Shipyard W.



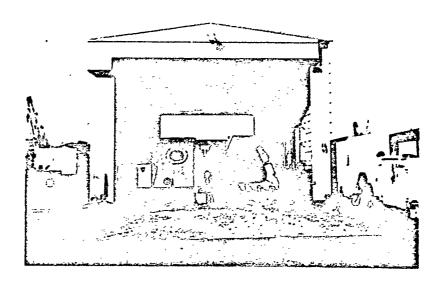
7. Block Assembly shop with travelling roof at Shipyard W. Type of roof: wholly travelling roof.



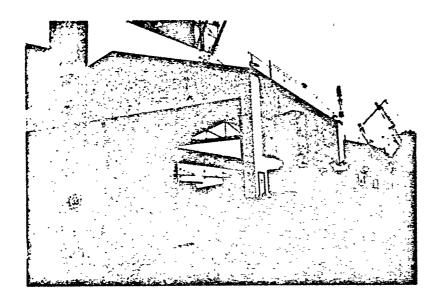
8. Block Assembly shop with travelling roof at Shipyard W. Type of roof:  $\neg$  wholly travelling roof.



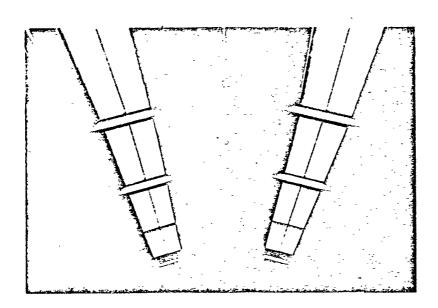
 Painting/Coating shop at Shipyard X in the Western region. Type of roof: permanent building, wholly closed, with travelling roof.



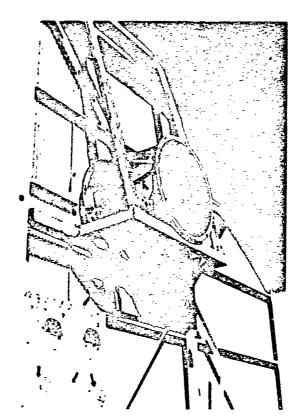
Painting/Coating shop at Shipyard X in the Western region.
 Type of roof: permanent building, wholly closed, with travelling roof.



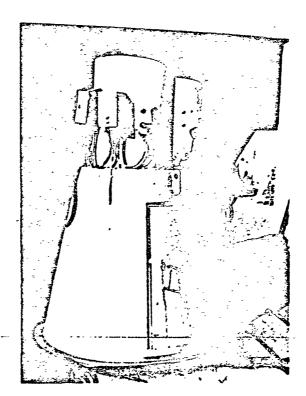
 Painting/Coating shop at Shipyard W. Type of roof: Travelling roof.



12. Painting/Coating shop at Shipyard W. Type of roof: Travelling roof.

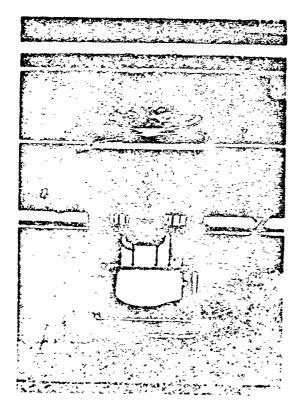


13. Ventilating Fan.



14. Ventilating Fan.

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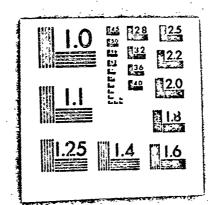
15. Gas Store.

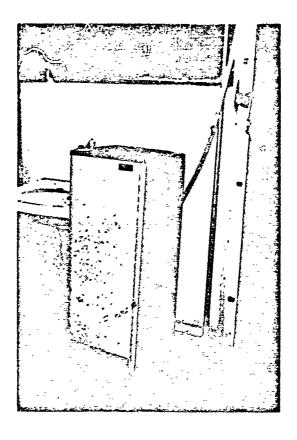


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16. Air Conditionning Unit on the dock.

# 30F3 00M-75 10933





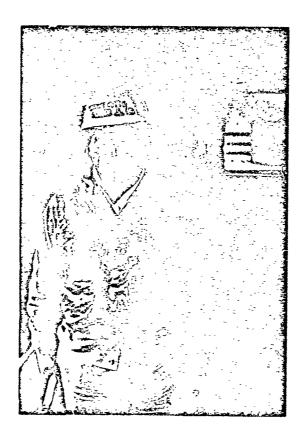
]

17. Water Cooler.



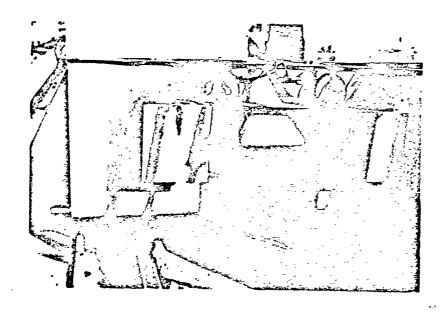
18. Winter Clo...

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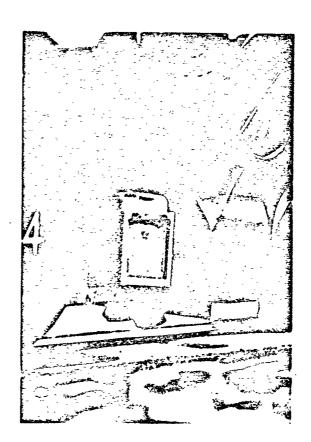


 $I_{\ell}^{i}$ 

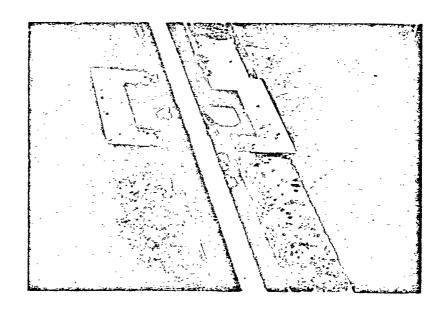
19. A foreman wearing Cool Suits.



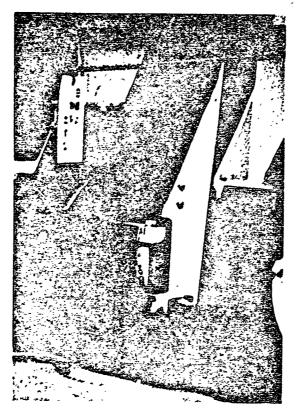
20. Rail clamping device for Bridge crane. H-90



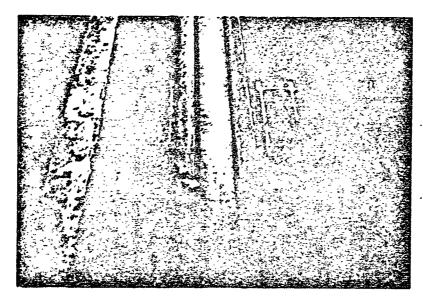
21. Hooking device for Goliath crane.



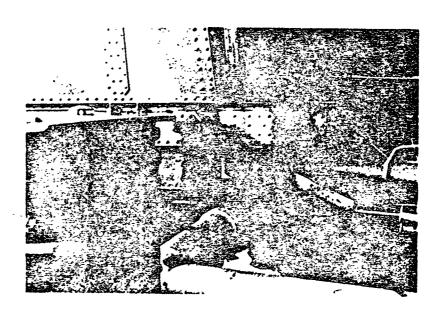
22. Hooking device for Goliath crane. H-91



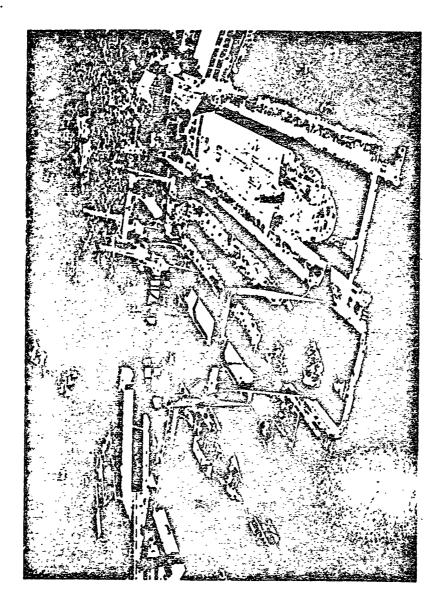
23. Pin drop device for Bridge crane.



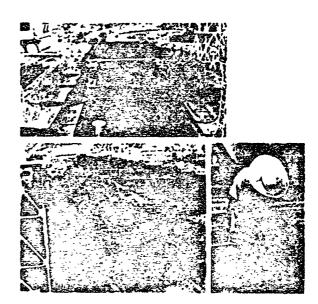
24. Pin drop device for Bridge crane.



25. Guy wire for Jib crane.



26. Goliath cranes at Shipyard X, each has carrying capacity 300 tons.



27. Sunnets over upper deck on the dock. H-95

#### APPENDIX I

## STATE-OF-THE-ART IN HEATHER PROTECTION FACILITIES IN THE EUROPEAN SHIPBUILDING INDUSTRY

Battelle-Frankfurt Laboratories, Frankfurt, Germany conducted a study, "Heather Protection Facilities at European Shipyard", under a subcontract to Battelle-Northwest a part of this study. That report is reproduced here.

The report includes estimates of increases of productivity and actual increases of productivity for working with weather protection facilities along with capital and operating costs of several structures.

Reference is madeon Page 12 of the report to English summaries of articles written in German. These are attached following the appendix section of the report. Photographs of movable "halls" and a hoarding panel system used in Germany are included at the end of the report.

#### Weather Protection Facilities

#### at European Shipyards

#### February 1973

#### A. <u>Introduction</u>

It is the intention of this report to describe the different types of weather protection facilities used at European yards and to demonstrate the improvements in worlcing productivity and costs.

Literature reviews could only urnish a small part of the information required for the study- SO special questionnaires were sent out to selected European shipyards and in addition, some German shipyards were contacted by telephone.

ortuxmtely the results of these activities were not sufficient because most of the shipyards were not willing to cooperate-

Therefore the following information, especially the quantitative figures, can not be representative for the European shipbuilding industry.

Nevertheless, the figures delivered by questionnaires of two German, one Dutch and one Swedish shippard, have been included in this report to give at least an order of magnitude. The report arrangement, which has been proposed by BNW, has been taken over as far as possible.

- B. <u>Designs</u>, costs and effects of weather protection <u>facilities</u>
  - Permanent and portable weather Protection facilities used at European shipyards

#### 1.1 Facility designs

The following weather protection facilities of different types and dimensions and for several. shipbuilding activities are in use:

- halls with fixed roof

construction: steel or reinforced concrete with

overhead travelling cranes

used for: marking, burnings welding. erecting

of panels and sections

- halls with traversing roof

construction: steel or reinforced concretc with

overhead traveling cranes or other

cranes. working from outside through

the open roof

used for:

marking, burning, wolding, erecting

of panels and sections

movable halls

construction: steel frame; steel- or other

material-plating

moved by:

vehicle, workmen

used for:

marking, burning, welding, erecting

of panels and sections, assembling

sheds

construction: steel

used for:

sandblasting, painting, storage,

general purpose

shacks

construction: wood

used for:

storage, general purpose

portable roofs

construction:

steel frame with corrugated plate

moved by:

crane

used for:

marking, burning, welding, painting

tarpaulin shelters, tents

used for:

burning, welding, painting, storage,

general purpose

weather protection clethes

used against: rain, wind, ice, snow, coldness

### 1.2. Capital and operation related costs

The capital and operation related costs of some weather protection facilities are specified in table 1.

Fo. better comparison, the costs are given in US dollars per square foot of floor area, too.

Table 1: Capital costs and operation related costs of some weather protection facilities

| type of weather                                   | floor area | capital          |                      | operati | on rela                   | ted cost              | ts per                   | year                    |                |         |
|---|------------|------------------|----------------------|---------|---------------------------|-----------------------|--------------------------|-------------------------|----------------|---------|
| rot etion<br>acility                              | sq. ft.    | related<br>US \$ | us \$<br>per sq. ft. | _       | main-<br>tenance<br>US \$ | hea-<br>ting<br>US \$ | illu-<br>minat.<br>US \$ | insu-<br>rance<br>US \$ | total<br>US \$ | US \$ 5 |
| hall with<br>fixed roof                           | 15,000     | 95,000           | 6.33                 | 2,400   | 1,250                     | 2,400                 | 500                      | 329                     | 6,870          | 0.46    |
| hall with<br>craversing roof                      | 14,500     | 170,000          | 11.72                | 2,500   | 1,750                     | 2,400                 | 450                      | 520                     | 7,620          | 0.53 +  |
| movable hall                                      | 3,200      | 10,000           | 3-13                 | 930     | 310                       | -                     | 160                      | 125                     | 1,525          | 0.48    |
| portible roof                                     | 900        | 1,500            | 1.67                 | 130     | 40                        | -                     | -                        | -                       | 170            | 0.19 E  |
| weather protection<br>clothes (for 50<br>workmen) | -          | 1,550            | -                    | 160     | -                         | -                     | -                        | -                       | 160            | •       |

NOTE: The above costs are for individual buildings and are not necessarily representative of capital and operating costs for buildings.

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2. Methods and procedures of weather protection for personnel and material in the European heavy construction industry. Improvements in productivity and costs.

A special analysis of this branch has not been made, because many of the European shippards build not only ships, but also docks, heavy steel constructions, apparatus, machines, etc.

Thus the conditions for the use of weather protection facilities are nearly the same.

- 3. Effects of weather protection facilities on productivity and costs in the European shipbuilding industry.
- Advantages and disadvantages in the use of weather protection facilities -

#### 3.1 Advantages

- better working conditions
- better working quality
- no interruption of work by adverse weather conditions
- lower uncertainty in work planning
- no schedule delays
- increase of working efficiency
- lower production costs

- no removal of rain water, snow, -ice
- less or no removal of dirt, dust, rust
- less or no preheating (when welding high tensile steel or painting)
- longer life span of shipbuilding tools and apparatus
- lower accident rate
- lower sickness rate
- possibility of working without daylight
- possibility of welding high tensile steels
- possibility of sand blasting
- possibility of using automatic devices

  (e.g. submerged arc welding or gas-shielded arc welding)
- better possibility of control

#### 3.2 Disadvantages

- narrow working space
- low height of crane hook (in halls with overhead travelling cranes)
- draft
- more heat
- more noise
- more welding and burning gases in the air
- more dust in the air during cleaning work
- 4. Increases of worker productivity obtained in the
  European shipbuilding industry by the use of weather
  protection.

#### 4.1 Productivity per shift and worker

|   |           | without weather protection facilities in adverse weather conditions (snow, ice, rain, storm) | with Weather<br>protection<br>facilities |
|---|-----------|--|--|
|   |           | linear ft.   | linear ft.                               |
| welding   | manual    | 65   | 120                                      |
|   | automatic | 240  | 430                                      |
|   |           |  |  |
| burning   | manual    | 180  | 360                                      |
|   | automatic |  | 570                                      |
|   |           |  |  |
|   |           | Sq. ft.  | Sq. ft.                                  |
| painting (incl<br>liminary work<br>derusting etc. | such as   |  |  |
|   | manual    | 220  | 480                                      |
| with spray  | gun       | 380  | 760                                      |

The shippards took the above figures from their production records.

Since thin plates afford a larger, and thick plates a smaller welding and burning productivity measured in linear ft. an average plate thickness has been assumed.

Figures for welding were assumed to be one run of welding.

Figures for painting were assumed for one coat film of the average thickness.

The significant difference between working productivities with and without weather protection facilities will of course decrease if better weather conditions are anticipated (see 4.2).

#### 4.2. Productivity.per year

(basis for productivity without weather protection facilities = 100)

|                                    | without weather protection facilities | with weather protection facilities |
|------------------------------------|---------------------------------------|------------------------------------|
| marking                            | 100                                   | 150                                |
| burning                            | 100                                   | 165                                |
| assembling includixxg tack welding | 100                                   | 140                                |
| welding                            | 100                                   | 165                                |
| painting including preliminary wor | k 100                                 | 170                                |
| other shipbuilding activities      | 100                                   | 135                                |

The above figures have been estimated by the shipyards.

# 5. Additional work requirements and costs in European shipbuilding caused by environmental extremes

removal of

- - dirt
- - dust
- -- scale
- - rust
- - rainwater
- -- snow
- - ice
- proheating for
  - -- welding
  - -- painting

more loss and repairing and maintenance of shipbuilding tools and apparatus

more 10ss of materials, e.g. welding electrodes and welding wire

- arrangement of safety devices to prevent damage by wind, storm, etc.
- 6. Secondary cost effects on worker productivity resulting from environmental extremes
- 6.1 Accident rates

(basis for accident rate without weather protection facilities = 100)

|                     | without weather protection facilities | with weather protection facilities |
|---------------------|---------------------------------------|------------------------------------|
| in summer           | 100                                   | 95                                 |
| in winter           | 100                                   | 75                                 |
| throughout the year | 100                                   | 85                                 |

#### 6.2 Sickness rates

(basis for sickness rate without weather protection facilities = 100)

|                     | without weather protection facilities | with weather protection facilities |
|---------------------|---------------------------------------|------------------------------------|
| in summer           | 100                                   | 95                                 |
| in winter           | 100                                   | 75                                 |
| throughout the year | 100                                   | 85                                 |

The above figures have been estimated by the shipyards.

#### C. Conclusion

Shipbuilding in Europe is shifting to an increasing extent from non-protected open-air space to weather protected areas.

Weather protected facilities ensure improvements in working productivity and working conditions.

Especially small and middle sized shippards with adverse climate conditions, e.g. Amels, IHC-Smit and Linz shippards (see literature), have erected and put into operation halls

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for shipbuilding activities, which had been done in open air space before. In some cases even building docks and slip way areas have been covered by weather protection devices.

Most of the larger shippards in Northwest Europe however, could not, or only partly, realize this idea of total inside shipbuilding up to now, because the capital costs for such great halls, covering the whole building areas, are too high in relation to the attainable output. The shippards, in many cases, also have not got enough orders to justify such investments.

#### D. Literature about Weather Protection

- 1. "Überdachtes Baudock bei der Amels-Werft in Makkum"- HANSA 1971, Nr. 21. p. 2096 -
- 2. "Binnenschiffbau in der Halle"
  - Schiff und Hafen 1972, Nr. 4, p. 247 249
- 3. "Überdachte Helling bei IHC Smit"
  - HANSA 1972, Nr. 24, p. 2270 2271
- 4. 'Reconstruction of Öresundsvarvet"
  - Schiff und Hafen, 1970, Nr. 11, p. 1038 1040

Copies of these articles are attached, additional English summaries of articles 1, 2, and 3.

## Überdachte Helling bei IHC Smit - Hansa 1972, No. 24, p. 2270 - 2271

Roofed Building Slip at IHC Smit Shippard (Netherlands) (English Summary)

The former shippards L. Smit and J. + K. Smit, Kinderdijk, have been united to one shippard within the IHC-Group since 1967.

The different situated local workshops require a reorganization of the entire shippard and also the way of production. Shipbuilding should be accomplished without the influence of adverse weather conditions and rationalized to a high degree so that personnel savings can be obtained. Workmen are no longer willing to do shipbuilding work at unprotected and narrow places.

The new shipbuilding hall, existing of three naves, was finished in October 1972. Consequently the whole steel shipbuilding up to launching can be accomplished inside the Hall.

The third nave covers the building slip, which has a bulk-heading against the outside water in form of a pontoon. Ships with the dimensions of 459.2 ft. x 75.4 ft. can be built on the building slip.

The dimensions of the hall are 551.0 ft. x 167.3 ft. x 111.5 ft.

Ventilation is obtained through two ventilation channels, respectively 14 exhaustors, which are fixed within the roof. The hall can be heated by infra-red heating devices.

V-61.847 101-71 101-76 Volkers Reg. (2)

## Überdachtes Baudock bei der Amels-Werft in Makkum

- Harsa 1971, No. 21, p. 2096

#### Roofed Building Dock at Amels Shipyard, Makkum (Netherlands)

In 1968 Makkum Shipyard started a large program of modernization. The first part of this program was completed in November 1971.

The main investments are a roofed building dock with the dimensions of 393.6 ft. x 62.3 ft. x 23.0 ft. and a hall of 413.3 ft. x 121.4 ft. x 93.5 ft. Thus, all shipbuilding works can be accomplished without the influence of adverse weather conditions. The dock floor is situated 15.4 ft. below the outside water level, so even ships which are nearly fully fitted out, can be floated up inside the hall.

The hooks of the overhead travelling hall cranes are 72.2 ft. above the floor of the hall, respectively 95.1 ft. above the floor of the building dock.

At both ends of the hall there are sliding doors with a clear width of 60.7 ft. installed. The doors are driven electrically and tele-controlled.

Above the sliding doors, which reach up to the crane track, there are wing doors installed. When these wing doors are opened, the overhead travelling cranes can roll out of the hall on crane tracks nearly 45.9 ft.

The hall is illuminated by 125 mercury vapour lamps of 1000 watt each and through plastic windows of 21.3 ft. breadth in the walls. Ventilators are installed within the roof of the hall. The hall can be heated in the winter.

It is planned to lengthen the building dock 262.4 ft. and the hall 426.4 ft.

V-61.847 101-71 101-76 Volkers Reg. (2)

#### Binnenschiffbau in der Halle

- Schiff und Hafen 1972, No. 4, p. 247 - 249

#### Building of River Vessels inside Halls

(English Summary)

On March 11, 1972, the Linz Shipyard (Austria) put into service a new shipbuilding hall (see plan, Hall No. IV).

There were several reasons for building the hall and altering the conventional procedure of shipbuilding:

- Shipbuilding should be accomplished without the influence of adverse weather conditions. It is very difficult to obtain qualified workmen who are willing to do the hard shipbuilding job in unprotected open air space.
- Increasing building costs should be stopped as far as possible by more productivity.
- There should be no uncertainty in work planning, which is very often the result of adverse weather conditions.
- Better quality of work should be achieved.
- The conditions of competition should be improved.

Technical data of the shipbuilding hall:

Dimensions:

Length: 328.0 ft; breadth: 114.8 ft; height: 78.7 ft.

Cranes: Two overhead travelling cranes of 40/10 t each, one crane of 10 t. Height of crane hook: 46.6 ft.

Sliding doors:

Dimensions:

west doors: 39.4 ft. x : 3.8 ft; 39.4 ft. x 51.2 ft.

east door: 23.0 ft. x 52.5 ft.

Heating: 20 air heating devices of 353,149 cu. ft./hour.

The dimensions of the halls allow to build two river vessels of European type (Europa-Type) (278.8 ft. x 31.2 ft.) side by side.

The ships are completely outfitted in the hall and then brought out by rail cars.

<u>V-61.847</u> 101-71 101-76 Volkers (Reg. 2)

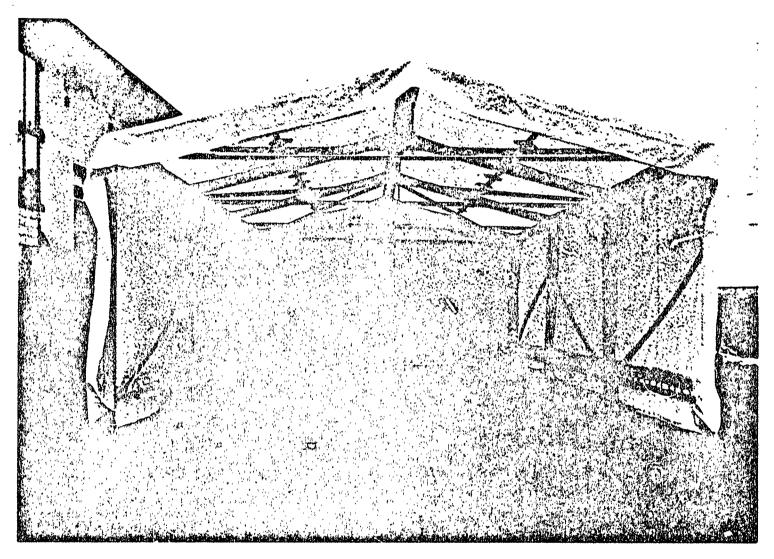


Figure I-l - Lightweight canvas-covered portable shelter supported on rubber tired wheels. These unique wheeled buildings are manufactured by Josef Wirtz and Co. GmbH in Germany and have seen use in European shipyards.

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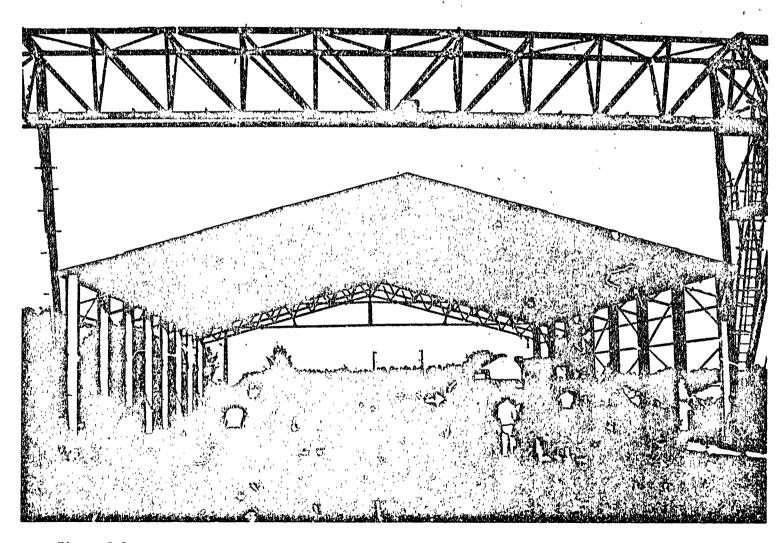


Figure I-2 - A movable hall, supported on wheels. These wheeled buildings may have sheet metal or canvas sides or ends, or be open as shown. They are manufactured by Josef Wirtz and Co. GmbH, Germany and have been used in European Shipyards and construction industry.

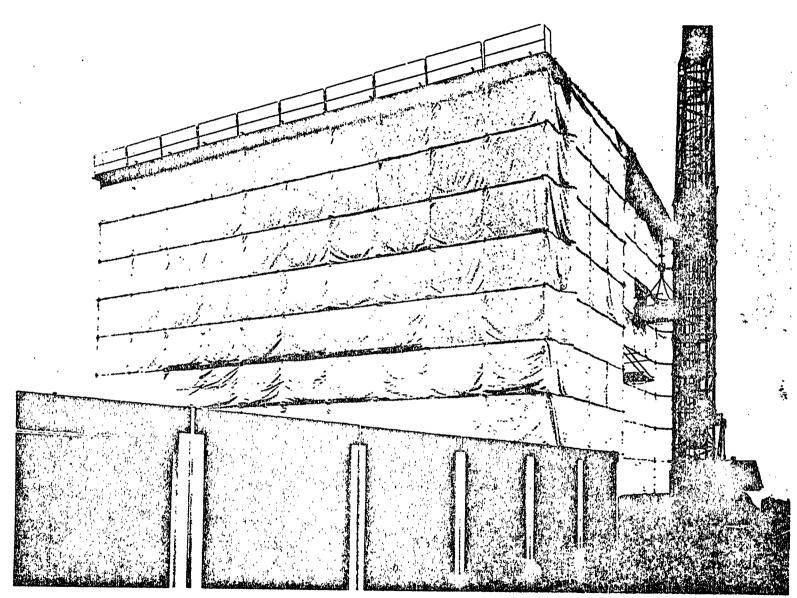


Figure I-3 - An example of the use of hoarding panels for weather protection in heavy construction in Germany. Note the access for materials delivery. These are called CENO plastic tilts and Carl Nolte, Germany is the patentee of this particular system. The fabric is reinforced PVC and is translucent.

#### APPENDIX J

#### DESCRIPTION OF THE STANDARD SHIPYARD

#### General

The productivity models were applied to a hypothetical "Standard" shipyard to obtain estimates of the cost effectiveness of various categories of weather protective structures. The purpose of the standard shipyard was to provide a yardstick against which anticipated benefits of this and other R&D programs could be measured. The standard shipyard description was provided by J. J. McMullen Associates as a part of a study on "Ship i'roductivity - Determination of Task Priorities." It describes both a "standard" shipyard and a "standard" ship.

The standard ship is a "Panamax" type of tanker with an overall length of 820 feet, a breadth of 105 ft, a depth of 60 ft and a displacement of 91,250 tons. Other particulars of the ship and its construction which are pertinent to this study are shown in tables in the following sections.

It should be pointed out that the "standard" shipyard is entirely synthetic having been created from a number of basic production requirements constrained by a number of typical environmental factors; although it is intended to be a standard United States shipyard, rather than a foreign one, any resemblance to any other shipyard, whether existing or defunct, is purely coincidental. It should be kept in mind that it is a tool for comparative analyses and is not intended to be an "optimum" shipyard.

The descriptions of the standard ship and the shipyard which follow are extracted from the J. J. McMullen Associates report.

#### The Standard Ship

The principal particulars of the standard ship, a "Panamax" tanker, are given in Table J-1. It is a traditionally high quality, subsidized construction vessel built to American Bureau of Shipping rules and conforming to all the usual requirements for U.S. flag operation.

A simplified breakdown of construction cost is presented in Table J-2 and expanded in Table J-3. Both of these exhibits display the elements of cost as percentages of the total: Table 5 converts the detailed data of Table J-3 to dollars, assuming that the total price for one ship in a continuous series is \$26,750,000 in mid-1973.

The weight breakdown of the seven steel classifications has been derived separately and is shown in Table J-5.

#### The Standard Shipyard

In formulating the standard shippard, it was assumed that the standard shippard, although built before World War II, has modernized its facilities to the fullest extent possible given its geographical and structural limitations.

It was also assumed that the shippard has an annual steel throughput of approximately 40,000 tons, equivalent to three standard ships a year.

| I.       |   | Table J-1                  |                   |
|----------|---|----------------------------|-------------------|
|          | DESIGN FEATURES OF  | A STANDARD 75,000 DWT T    | ANKER             |
| ll L     | ength Overall<br>ength B.P.<br>readth                             | 780' -                     | 0 #<br>0 #<br>0 # |
| IT D     | epth<br>craft, full load  | —                          | 0"                |
| ∐ 0<br>M | teel weight, tons<br>outfit weight, tons<br>achinery weight, tons | 13,500<br>1,750<br>1,000   |                   |
| l) p     | ightship, tons<br>eadweight, tons<br>isplacement, tons            | 16,250<br>75,000<br>91,250 |                   |
| ∐ s      | achinery<br>HP<br>ropellers                                       | Geared steam 20,000        | turbine           |
| S<br>B   | peed, design, knots<br>unkers, tons<br>adurance, miles            | 16<br>5,000<br>15,000      |                   |
|          | umps<br>ump size, GPM   | 6,500                      |                   |
| A<br>C   | argo tanks<br>ccommodation<br>lassification<br>egistry            | 7<br>Aft<br>ABS            |                   |
|          | rew   | us<br>30                   |                   |
|          |   |                            |                   |

#### TOTAL PRICE BREAKDOWN

#### (Simplified)

| •                 | / 26.31 % |
|-------------------|-----------|
| Direct Material   | 50.00     |
| Total Direct Cost | 76.31     |
| Indirect          | 5.26      |
| Engineering       | 2.63      |
| Construction Cost | 84.20     |
| overhead •        | 15.80     |
| Total Cost        | 100.00    |
| Profit            | 12.63     |
| Total Price       | 112.63 %  |

Table J-3

# TOTAL PRICE BREAKDOWN (Detailed)

| DESCRIPTION                      | MATERIAL 8  | LABOR         |
|----------------------------------|-------------|---------------|
| Shell Plating                    | - 5.31      | 4.25          |
| Bulkheads and Pillars            | 4.56        | 3.08          |
| Frames                           | 6.64        | 5.14          |
| Deck Plating and Beams           | 4.24        | 2.05          |
| Superstructure                   | •55         | 1.55          |
| Foundations                      | .14         | .85           |
| Castings                         | .70         | .21           |
| Total Steel                      | 22.14       | 17.13         |
| Masts and Rigging                | .09         | . 05          |
| Hatch Covers and Beams           | to en e-    |               |
| Anchors, Cables and Hawsers      | <b>.7</b> 5 | .03           |
| Hull Attachments and Joinerwork  | 3.05        | .71           |
| Generators and Distribution      | 2.15        | .97           |
| Reefer and Air Conditioning      | .30         | .07           |
| Deck Auxiliaries                 | 2.15        | .19           |
| Navigation and Steward's Outfit  | . 45        | .16           |
| Hull Plumbing                    | 3.65        | 1.86          |
| Ventilation                      | . 40        | . 47          |
| Paint                            | 2.51        | 2.35          |
| Total Outfit                     | 15.50       | 6.86          |
| Main Engine and Shafting         | 5.08        | .23           |
| Boilers, Fuel and Steam Systems  | 4.76        | 1.51          |
| Pumps and Compressors            | 1.56        | .07           |
| Engineroom Outfit                | .96         | .51           |
| Total Machinery Total Labc-      | . 12.36     | 2.32          |
| Total Labe-<br>Total Material    | •           | 26.31         |
| Total Material Total Direct Cost |             | 50.50         |
| Indirect                         | •           | 76.31<br>5.26 |
| Engineering                      |             | 2.63          |
| Construction Cost                |             | 84.20         |
| Depreciation                     | 2.11        | 04.20         |
| Fringe Benefits                  | 6.32        |               |
| Other                            | 7.37        |               |
| Total Overhead                   |             | 15.80         |
| Total Cost                       | -           | 100.00        |
| Profit                           |             | 12.63         |
| Total Pr                         | ice         | 112.63        |

Table J-4

#### TOTAL PRICE BREAKDOWN

| DESCRIPTION  Shell Plating Bulkheads and Pillars Frames | MATERIAL<br>\$<br>1,262,500<br>1,085,000<br>1,577,500 | LABOR<br>\$<br>1,010,000<br>732,500<br>1,220,000 |
|---|---|--|
| Deck Plating and Beams                                  | 1,007,500   | 487,500  |
| Superstructure  | 130,000   | 367,500  |
| Foundations   | 32,500  | 202,500  |
| Castings  | 165,000   | 50,000   |
| Total Steel   | 5,260,000   | 4,070,000  |
| Mast and Rigging  | 22,500  | 12,500   |
| Hatch Covers and Be.ms<br>Anchors, Cables and Hawsers   | 177,500   | 7,500  |
| Hull Attachments and Joinerwork                         | 725,000   | 167,500  |
| Generators and Distribution                             | 510,000   | 230,000  |
| Reefer and Air Conditioning                             | 70,000  | 17,500   |
| Deck Auxiliaries  | 510,000   | 45,000   |
| Navigation and Steward's Outfit                         | 107,500   | 37,500   |
| Hull Plumbing   | 867,500   | 442,500  |
| Ventilation   | 95,000  | 112,500  |
| Paint   | 595,000   | 557,500  |
| Total Outfit  | 3,680,000   | 1,630,000  |
| Main Engine and Shafting                                | 1,207,500   | 55,000   |
| Boilers, Fuel and Steam Systems                         | 1,130,000   | 357,500  |
| Pumps and Compressors                                   | 370,000   | 17,500   |
| Engineroom Outfit                                       | 227,500   | 120,000  |
| Total Machinery   | 2,935,000   | 550,000  |
| Total Labor   | . •   | 6,250,000  |
| Total Material  | -   | <b>21,875,000</b>                                |
| Total Direct Cost                                       | •   | 18,125,000                                       |
| Indirect<br>Engineering                                 |   | 1,250,000<br>625,000                             |
| Construction Cost                                       |   | 20,000,000                                       |
| Depreciation Constitution Cost                          | 509,000   | 20,000, 000                                      |
| Fringe Benefits   | 1,500,000   |  |
| Other   | 1,750,000   |  |
| Total Overhead  |   | 3,750,000  |
| Total cost  |   | <b>2</b> 3,750,000                               |
| Profit  |   | 3,000,000  |
|   |   |  |
| Total Pri   | .ce \$  | 26,750,000                                       |

Table J-5

#### STEELWEIGHT BREAKDOWN

|                        | Tons   |
|------------------------|--------|
| Shell plating          | 3,375  |
| Bulkheads and pillars  | 2,862  |
| Frames                 | 3,888  |
| Deck plating and beams | 2,660  |
| Superstructure         | 500    |
| Foundations            | 108    |
| Castings               | 107    |
|                        | 13,500 |

The direct labor requirements of this rate of production are given in Table J-6. The direct labor costs in dollars from Table J-4 have been converted into manhours using an average rate of \$4.60, the projected average hourly rate for the United States shipbuilding industry at mid-1973, and the results have been multiplied by three to reflect the assumed output of three ships a year. In the second column, these manhours have been expressed as a percentage of total direct labor manhours—and in the third column they have been divided by 2000 to arrive at the equivalent number of direct labor employees required. The total in this column shows an average direct labor requirement of 2038 workers.

The required direct labor workforce shown in Table J-6 is presented again in Table J-7 in such a way as to demonstrate the distribution of manpower both by function and work location.

It was further assumed that the standard shippard is engaged in merchant ship construction only and all, naval and repair work is contained within a separate and distinct organization.

Although virtually all United States shipyards are involved simultaneously in both merchant and naval shipbuilding and ship-repairing, the impacts of cost reduction tasks on commercial ship costs can only be effectively evaluated if those costs are isolated from the shipyard's other activities. The implication of this assumption for the definition of the standard shipyard is that the labor force is perfectly balanced and fully occupied, a condition that can only be true in a shipyard building a single Product, a standard ship, since variations in product mix inevitably result in variations in labor function requirements.

Table J-6

LABOR REQUIREMENTS

| CLASSIFICATION                              | Annual Direct<br>Labor<br>Hanhours | of Total<br>Direct<br>Labor | Equivalent<br>f of<br>Men |
|---|------------------------------------|-----------------------------|---------------------------|
| Shell Plating                               | 658,700                            | 16.2                        | 200                       |
| Bulkheads and Pillars                       | 477,700                            | 11.7                        | 329                       |
| Frames                                      | 795,600                            | 19.5                        | 239                       |
| Deck Plating and Beams                      | 317,900                            | 7.8                         | 398                       |
| Superstructure                              | 239,700                            | 5.9                         | 159                       |
| Foundations                                 | 132,100                            | 3.2                         | 120                       |
| Castings                                    | 32,600                             | .8                          | 66                        |
| Total Steel                                 | 2,654,300                          | 65.1                        | 16                        |
|   |                                    | 03.1                        | 1,327                     |
| Masts and Rigging<br>Hatch Covers and Beams | 8,200                              | .2                          | 4                         |
| Anchors, Cables and Hawsers                 | 4.000                              | ·                           |                           |
| Hull Attachments and JoinerWork             | 4,900                              | .1                          | 3                         |
| Generators and Distribution                 | 109,200                            | 2.7 ·                       | 55                        |
| Reefer and Air Conditioning                 | 150,000                            | 3.7                         | 75                        |
| Deck Auxiliaries                            | 11,400                             | •3                          | .6                        |
| Navigation and Stewards Outfit              | 29,300                             | .7                          | 15                        |
| Hull Plumbing                               | 24,400                             | · _•6                       | 12                        |
| Ventilation                                 | 208,600                            | 7.1                         | 144                       |
| Paint                                       | 73,400                             | 1.8                         | 37                        |
| Total Outfit                                | 363,600                            | 8.9                         | 182                       |
| Total Outrie                                | 1,063,000                          | 26.1                        | 532                       |
| Main Engine and Shafting                    |                                    |                             |                           |
|   | 35,900                             | <b>.9</b> ·                 | 18                        |
| Boilers, Fuel and Steam Systems             | 233,100                            | 5.7                         | 116                       |
| Pumps and Compressors                       | 11,400                             | .3                          | 6                         |
| Engineroom Outfit                           | <u>78,300</u>                      | 1.9                         | 39                        |
| Total Machinery                             | 358,700                            | 8.8                         | 179                       |
| TOTAL                                       | 4,076,000                          | 100.0                       | 2,038                     |

Table J-7
DIRECT LABOR DISTRIBUTION

| Location Function    | Steel Fabrication & Related Shops | Steel<br>Assemby Shops<br>and Areas | Departmental<br>Shops | Machinery<br>Assembly<br>Shops | Shipway | Outfitting<br>Wharf | Totals    |
|----------------------|-----------------------------------|-------------------------------------|-----------------------|--------------------------------|---------|---------------------|-----------|
| Steelwork            | 200                               | 400                                 | CON 1755 SAM          | 7                              | 700     | 20                  | 1327      |
| Electrical           |                                   | 10                                  | 8                     | 2                              | 35      | 20                  | <b>75</b> |
| Piping<br>Sheetmetal | 4                                 | 20 .                                | 74                    | 8                              | 24      | 14                  | 144       |
| Sileetilletai        |                                   | 1.0                                 | 14                    | 2                              | 20      | 4                   | . 50 .    |
| Joinerwork           | dan kali kab                      |                                     | 10 .                  |                                | 15      | 20                  | 45        |
| painting             | 4                                 | 40                                  | . 4                   |                                | .110    | 24                  | 1.82      |
| Machinery            | 000 cm 000                        | 20                                  | 12 .                  | 40                             | 48      | 59                  | 179 .     |
| Other .              | ***                               | ***                                 | . 4.                  |                                | 20      | 12                  | 36        |
| otals                | 208                               | 500                                 | 126                   | 59                             | 972,    | 173                 | 2038      |

J-10

The support workforce required by a standard shipyard with a direct labor workforce of 2038 was defined as 458 additional employees (for a total of 2496).

This proportion represents the position of the standard shipyard as an approximately average yard in the spectrum of United States shipbuilding. Indirect, engineering and overheads, which include the cost of the support workforce are shown in Table J-8.

#### Facilities and Production Processes in the Standard Shipyard

Steel arrives"by rail and is unloaded and sorted by a gantry magnet crane in a stockyard of about 60,000 square feet, employing a horizontal storage and having a capacity for one shipset of steel. The standard plate size is 45 feet by 10 feet, although the maximum could be 48 by 12. This standard size is directly related to the design of the standard ship, 45 feet being one half of the tank length, and hence to the panel construction method.

The steel is fed by convejor, via a surface preparation line involving the usual cleaning, mangling, blasting, painting and drying processes, into a fabrication shop of about 40,000 square ieet, divided into four bays, equipped for sections, flat panel material, shaped panel material and the remainder. The fabrication shop is equipped with the conventional cold forming machinery, template-controlled, and automatic burning machinery, optically-controlled. There is no numerical control. An overhead crane of 15 tons spans each bay.

### Table J-8 INDIRECT, ENGINEERING AND OVERHEAD COSTS

#### (MARAD GROUPINGS)

|  | • of Costs | Cost in \$.              | Equivalent<br>f of Men |
|--|------------|--------------------------|------------------------|
| Indirect Costs Insurance and bond premia, fees for classification and testing, royalties of a general nature.  Drycocking, launching trials and delivery costs,  | .26        | \$ 187,500;              |                        |
| including supplies, catering, trials personnel, pilots. tugs, calibration, etc. Miscellaneous labor for ship cleaning, toolrooms,  | 79         | 562,500                  |                        |
| watchmen, materials handling, supervision, industrial engineering functions. Sundry other items, including travel, temporary   | 2.63       | \$1,875,000              | . 200                  |
| services, weather protection, fire prevention, gasfree-ing and analysis, photography.  | 1.58       | \$1,125,000:             | 20                     |
| Engineering Costs  Drawings, calculations, yard liaison, purchase requisitions, tests, microfilming, model testing, outside professional services.   | 5.26       | \$3,750,000              |                        |
|  | 2.63       | \$1,875,000              | 80                     |
| Degreciation, insurance and taxes.   | 2.11       | \$1,500,000,             | •••                    |
| Maintenance and repair of all property, buildings, machinery and equipment, fixed or portable.  Wages and salaries of all other personnel, including management, departmental supervision, clerical staff, | 2.11       | \$1,500,000.             | 18.                    |
| maintenance personnel, crane operators, storekeepers, drivers, production planning, welfare services and administration.  Supplies of services and maintenance and adminis-                                | 2.63       | \$1,875,000.             | 100                    |
| trative requirements.  Fringe benefits, including vacation and holiday pay, bonuses, social security, life insurance, unemploy-  | 1.58       | \$1,125,000 <sub>1</sub> | •••                    |
| ment tax, workmen's compension, sick benefits, excused time, etc.  Miscellaneous other costs, including accidents,   | 6.32       | \$4,500,000              |                        |
| losses, welfare, travel, R and D, estimating, advertising, etc.  | 1.05       | \$ 750,000.              | 40                     |
| •  | 15.80      | \$11,250,000.            | 158                    |
| Total indirect, engineering and overhead:  | 23.69      | \$16,875,000             | 458                    |
|  |            |                          |                        |

The section and flat panel material bays lead into a flat panel assembly shop of about 20,000 square feet, featuring eight working areas, of 2,500 square feet each, for the construction of flat panels of plating with associated longitudinal and transverse framing, up to a maximum size of 48 feet by 30 feet, and averaging 60 tons each. Welding is semi-automatic, both of plate-butts and of stiffening, and material is moved and positioned using three overhead cranes, two of 75 tons and one of 15 tons. Average panel construction time is four to five days. The other two fabrication bays lead into a shaped panel assembly shop, also of about 20,000 square feet, where working areas are laid out as required for the more complex shaped panels. Welding is semi-automatic or manual and material is moved and positioned by means of similar cranage to the flat panel shop. Average panel construction time is eight to ten days.

All completed steel assemblies are moved outside to a paint shop where welds are cleaned and painted and then to storage areas or directly to the shipways: multi-wheel heavy-load transporters are used for these movements.

Machinery and outfit materials are received both by road and by rail and held in conventional warehousing and other storage areas until required. Machinery and outfit "work packages" are put together in-various shops, mostly of an earlier generation, and delivered to work stations by truck or forklift. "These packages are normally but not necessarily trade-oriented: they may include material for several different operations planned to take place in the same work place. Limited panel outfitting takes place in the

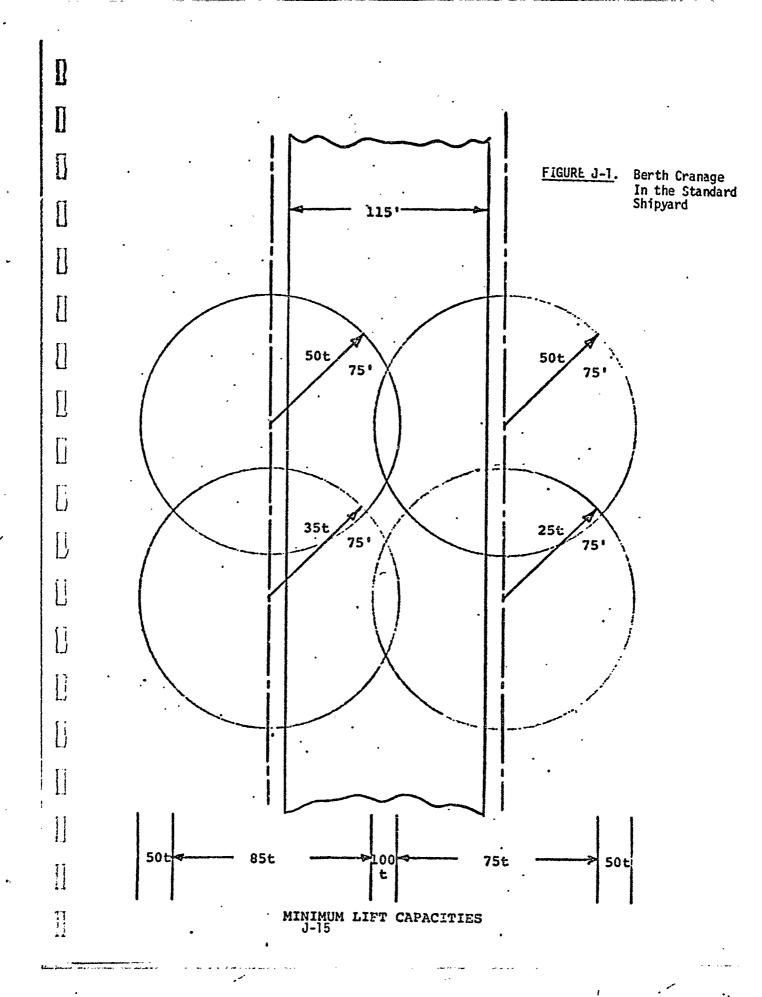
steel assembly shops, being confined to the fitting of attachments for piping, cable trays and ventilation ducting.

Ship erection is carried out on one of two shipways, starting with stern panels and working forward and upward. Each shipway is big enough for the standard ship with a working margin of five feet on each side and thirty feet on the length but no more. Each is served by four whirley cranes:

- two of 50 tons max. lift at 75 feet max. outreach
- one of 35 tons max. lift at 75 feet max. outreach
- one of 25 tons max. lift at 75 feet max. outreach

as shown in the sketch presented as Figure J-1. Average erection time is eight months at an average work rate of approximately on: panel per day.

After launching.aunching, each ship is moved to a single outfit wharf where its stay averages four months.



#### Outdoor Operations in the Standard Shipyard

The indoor operations and facilities and the outdoor shipways are described in the preceding pages.

The approximate uses and areas for outdoor operations which could be covered for weather protection were assumed to be in the ranges shown below:

#### Description

Steel stockyard operation

Machinery and outfit storage
areas for bulky items
of a non-weather-sensitive
nature

Cleaning and painting of welds on steel assemblies

Panel storage (or module assembly, if desired) with associated pre-outfitting (if not completed in the assembly shop) or further pre-outfitting following mudule assembly including fitting of as many of the following items as seems appropriate to the shipyard management:

pipes
valves and other pipefittngs
ventilation ducts
cable trays
cable runs
doors
manholes
skylights
hull openings

heating coils interior painting exterior painting machinery room outfit accommodation fitting to the extent that it is possible.

#### Area

60,000 sq.ft.
As required

10,000 Sq.ft. minimum 20,000 Sq.ft. minimum, up to 80,000 sq.ft.

#### DIRECT LABOR DISTRIBUTION IN THE STANDARDS SHIPYARD

The distribution of direct labor in the standard shippard by craft and location is shown in Tables J-9 through J-11 for steel work, machinery work and outfit work. This distribution was used in the productivity model.

Table J-9 DIRECT LABOR DISTRIBUTION FOR STEEL WORK

|      | Location<br>Function   | Steel<br>Fabrication &<br>Related Shops | Steel<br>Assembly Shops<br>& Areas | Departmental<br>Shops | Machinery<br>Assembly<br>Shops | Shipwaý                                     | Outfitting<br>Wharf | Totals |
|------|------------------------|---|------------------------------------|-----------------------|--------------------------------|---|---------------------|--------|
|      | Burners &<br>Welders   | a:60                                    | 160 a:80<br>b:80                   | -                     | a:4                            | 287 \begin{cases} b: 110 c: 177 \end{cases} | 30 {b:8<br>c:22     | 541    |
|      | Blasters &<br>Painters | 10 {a:5<br>b:5                          | b:10                               | · •                   | 0                              | 25 \begin{cases} b: 20 \c:5 \end{cases}     | 15 {b:7<br>c:8      | 60     |
| 1 10 | Fitters                | a:107                                   | 187 <b>a:87</b><br>b:100           | -                     | a:2                            | 285 b:113<br>c:172                          | 25 b:6<br>c:19      | 606    |
|      | Riggers                | 20 a:18<br>b:2                          | 40 {a:20<br>b:20                   | -                     | a:1                            | 39 b:14<br>c:25                             | 8 b:2<br>c:6        | 108    |
|      | Other Crafts           | a:3                                     | b:3                                | -                     | 0                              | b:4   | c:2                 | 12     |
|      | TOTALS                 | 200                                     | 400                                | -                     | 7                              | 640   | 80                  | 1327   |

a. In the shop
b. Outside not protected from weather
c. " but " by ship structure

Table J-10 DIRECT LABOR DISTRIBUTION FOR: MACHINERY WORK

| Location<br>Function | Steel<br>Fabrication &<br>Related Shops | Steel<br>Assembly Shops<br>& Areas | Departmental<br>Shops | Machinery<br>Assembly<br>Shops | Shipway  | Outfitting<br>Wharf | Totals |
|----------------------|---|------------------------------------|-----------------------|--------------------------------|----------|---------------------|--------|
| Burners & Welders    |   |                                    | ·                     |                                | b:1/c:1  | c:6                 | 8      |
| Blasters & Painters  |   |                                    |                       |                                | c:1      | c:3                 | 4      |
| Fitters              |   |                                    |                       |                                |          |                     |        |
| Riggers              |   |                                    |                       |                                | b:6/c:2  | c:4                 | 12     |
| Other:               |   |                                    |                       |                                |          |                     |        |
| Pipefitters          |   |                                    | a:15                  | ,                              | b:6/c:22 | c:40                | 83     |
| Electricians         |   |                                    | a:4                   |                                | c:12     | c:24                | 40     |
| Machinists           |   |                                    |                       | a:6                            | b:8/c:4  | c:6                 | 24     |
| Sheet Metal W        | krs.                                    |                                    | a:1                   |                                | c:2      | c:5                 | 8      |
| TOTALS               | -                                       | •                                  | 20                    | 6                              | 65       | 88                  | 179    |

<sup>a. In the shop
b. Outside not protected from weather
c. " but " by ship structure</sup> 

a. In the shop

b. Outside not protected from weather
c. "but "by ship stru by ship structure

#### APPENDIX K

#### ANALYSIS OF COSTS FOR THE STANDARD SHIPYARD

#### COSTS AFFECTED BY LABOR PRODUCTIVITY

Lower labor productivity and lost time can increase shipbuilding costs in several ways (Table K-1). The potential magnitude of these costs for the standard shippard are described and calculated in this section.

#### TABLE K-1. Increased Costs Caused by Lost Time or Lower Productivity

- A. Shipyard capacity not fully realized.
  - 1. Land is occupied longer than needed.
  - 2. Building space is occupied longer than needed.
  - Equipment and facilities not used to capacity.
  - 4. Inventory costs for work-in-process are higher.
  - 5. Overhead cost allocated over a reduced production.
  - 6. Extra capacity is required to meet peak operating rates.
- B. Unit labor costs increase.
  - 1. Payments for idle time not worked.
  - Lower output/man-hour.
  - 3. Reject and rework cost.
  - 4. Premium pay for call-in or overtime.

The cost distribution for the standard shipyard was shown in Table J-6 and Table J-8, Appendix J. The total annual costs for the standard shipyard are \$80,210,000. The overhead costs were distributed into material-related, labor-related, related to selling price, and fixed period costs as shown in Tables K-2 and K-3. The costs related to selling price in Table K-3 were redistributed proportionally to the other three. After this redistribution, the percentage breakdown of costs in the model shipyard were: labor-related, 37.4%; material-related, 54.2%; and fixed, 8.4%.

| Indirect Cost                  | % of Costs | Nature of Variability                                  |  |  |
|--------------------------------|------------|--|--|--|
| Insurance & Bond Premium, etc. | 0.26       | Fixed percentage of selling price                      |  |  |
| Drydocking, etc.               | 0.79       | Fixed percentage of selling price                      |  |  |
| Misc. Labor, etc.              | 2.63       | 1/2 Variable with direct labor cost - 1/2 fixed annual |  |  |
| Sundry Other Items, etc.       | 1.58       | 3/4 Fixed annual expense - 1/4 to direct labor         |  |  |
| Engineering Costs              | 2.63       | Fixed percentage of selling price                      |  |  |
| Overhead Costs                 | ,          |  |  |  |
| Depreciation, etc.             | 2.11       | Fixed annual expense (varies with capital investment)  |  |  |
| Maintenance, etc.              | 2.11       | Fixed annual expense (varies with capital investment)  |  |  |
| Wages, etc.                    | 2.63       | Fixed percentage of selling price                      |  |  |
| Supplies, etc.                 | 1.58       | Fixed percentage of selling price                      |  |  |
| Fringe Benefits, etc.          | 6.32       | Variable with direct labor cost                        |  |  |
| Misc. Other, etc.              | 1.05       | Fixed annual expense                                   |  |  |
| Profit                         | 12.63      | Fixed percentage of selling price                      |  |  |

TABLE K-3. Distribution of Annual Costs in the Standard Shipyard

Construction Schedule = 3 ships 1 year

| Expense                  | One Ship   | Three Ships | %%  |  |
|--------------------------|------------|-------------|-----|--|
| Direct Labor             | 6,250,000  | 18,750,000  | 24  |  |
| Labor Burden             | 1,910,000  | 5,730,000   | 7   |  |
| Direct Material          | 11,875,000 | 35,600,000  | 44  |  |
| Fixed Annual             | 1,840,000  | 5,520,000   | 7   |  |
| Related to Selling Price | 4,870,000  | 14,610,000  | 18  |  |
| 1                        | 26,675,000 | 80,210,000  | 100 |  |

Only the labor-related costs, 37.4% of the annual shipyard costs, vary directly with labor productivity. This percentage was used to determine the minimum cost savings achieved through productivity gains. The minimum cost does not include any extra provisions for hiring or training costs. The maximum cost savings are derived from the elimination of overtime premium pay and are calculated at 60% of the annual shipyard costs.

Intermediate cost savings would result from an increase in the production rate of the shipyard. Fixed costs per unit of production would be reduced. Interest expense on working capital would be reduced since the production schedule would be shortened. The calculation below of interest expense on working capital assumes reduction of four months covering 90% of the costs, since a large fraction of the costs, primarily for steel, are committed early in the shipbuilding schedule.

#### CALCULATIONS OF THE EFFECT OF LABOR PRODUCTIVITY ON SHIPBUILDING COSTS

Costs to regain lost productivity are calculated below for three different assumptions. The typical shipyard experience is probably a mixture of all these cases with some additional cost factors not specifically included here.

#### Maximum Cost Case

1. If the productivity deficit is made up by overtime - assuming minimum pay of time-and-one-half: then the increased cost to achieve the required output would be 1-1/2 times the straight time labor-related costs, or

$$0.374 \times \frac{1-\text{productivity}}{\text{productivity}} \times 1 \frac{1}{2} = 0.561 \times \frac{1-\text{productivity}}{\text{productivity}}$$

Since some premium pay would be at double time, we used 60% for the maximum cost case.

For example, if the average annual productivity in the shipyard was 90% (0.90), then the maximum annual cost for regaining this lost productivity through overtime would be:

$$0.60 \times \frac{1-0.90}{0.90} \times \$80,210,000 = \$5,350,000.$$

#### Minimum Cost Case

2. If the productivity deficit is made up with an increased work force, then the annual increased cost for straight time pay only would be, using the preceding example:

0.374 x 
$$\frac{1-\text{productivity}}{\text{productivity}}$$
 x \$80,210,000 = \$3,330,000.

#### Intermediate Cost Case

3. If the productivity deficit results in a longer schedule (reduced capacity), then the annual increased cost would be:

1-productivity productivity

(Fixed Cost)

b)  $.90 \times \frac{4}{12} \times 0.12 \times \frac{(1-\text{productivity})}{\text{productivity}} = .036 \times \frac{1-p}{p}$  (Interest on Working Capital)

assuming 90% of the costs are committed for four less months at 12% interest on working capital.

c) .374 x  $\frac{1-p}{p}$ 

(Straight Time Labor Cost)

d) tota1 = (.084 + .036 + .374) or  $0.492 \times \frac{1 - p}{p}$ 

and the total dollar cost using the preceding examples would be:

 $0.492 \times \frac{1 - 0.9}{0.9} \times $80,210,000 = $4,390,000$ 

# APPENDIX L LISTING OF THE COMPUTER PROGRAM FOR THE SHIPYARD PRODUCTIVITY MODEL U

#### APPENDIX L

#### COMPUTER PROGRAM FOR THE SHIPYARD PRODUCTIVITY MODEL

The Program is Written in Fortran V for the UNIVAC 1108.

#### DEFINITION OF VARIABLES USED IN COMPUTER PROGRAM

 $\Box$ 

TPRD

| •      | •  |
|--------|--|
| PRODET | RELATIVE PRODUCTIVITY FOR EFFECTIVE TEMPERATURE CATEGORIES   |
| PRODAT | RELATIVE PRODUCTIVITY FOR DRY BULB TEMPERATURE CATEGORIES  |
| PRODWS | RELATIVE PRODUCTIVITY FOR WIND CATEGORIES  |
| PRODPR | RELATIVE PRODUCTIVITY FOR PRECIPITATION CAGETORIES   |
| FGP    | RELATIVE PRODUCTIVITY FOR FOG CATEGORIES   |
| PRODSH | RELATIVE PRODUCTIVITY FOR SHADE CATEGORIES   |
| RTTIO  | RATIO CRAFTSMEN AT OTHER LOCATIONS TO OUTSIDE CRAFTSMEN OR SHOP  |
|        | CRAFTSMEN TO IN-SHIP CRAFTSMEN   |
| RAINPR | FRACTION SHIFT WORKED DURING PRECIPITATION PERIODS   |
| NAM    | SHIPYARD LOCATION  |
| DT     | DRY BULB TEMPERATURE CATEGORIES  |
| ET     | EFFECTIVE TEMPERATURE CATEGORIES   |
| WIND   | WIND VELOCITY CATEGORIES   |
| SUN    | FRACTION OF SHIFT WITH SUNSHINE  |
| FOG    | FRACTION OF SHIFT WITH FOG   |
| PREC   | PRECIPITATION CATEGORIES   |
| RH     | RELATIVE HUMIDITY CATEGORIES   |
| PT     | CORRECTION OF EFFECTIVE TEMPERATURE FOR PAINTERS   |
| EPROD  | AVERAGE ANNUAL PRODUCTIVITY FOR EFFECTIVE TEMPERATURE CATEGORIES   |
| APROD  | AVERAGE ANNUAL PRODUCTIVITY FOR DRY BULB TEMPERATURE CATEGORIES  |
| WPROD  | AVERAGE ANNUAL PRODUCTIVITY FOR WIND CONDITIONS  |
| PRPROD | AVERAGE ANNUAL PRODUCTIVITY FOR PRECIPITATION (RELATIVE HUMIDITY   |
|        | FOR PAINTERS) CONDITIONS   |
| FOGPR  | AVERAGE ANNUAL PRODUCTIVITY FOR FOG CONDITIONS   |
| SUNPR  | AVERAGE ANNUAL PRODUCTIVITY FOR SUN CONDITIONS   |
| GW     | IDEAL WEATHER OUTSIDE  |
| AGW    | IDEAL WEATHER IN-SHIP  |
| BGW    | EXCESS IDEAL WEATHER IN-SHIP OVER OUTSIDE  |
| TPROD  | TOTAL ANNUAL PRODUCTIVITY FOR EACH TEMPERATURE CATEGORY  |
| PCT    | DISTRIBUTION OF WORKMEN BETWEEN SHIFTS   |
| ICRAFT | NUMBER OF WORKMEN OF EACH CRAFT AT EACH LOCATION   |
| JCRAFT | NUMBER OF WORKMEN OF EACH CRAFT AT EACH LOCATION ON EACH SHIFT   |
| LURAFT | FRACTION OF TOTAL WORKMEN ON EACH SHIFT AND LOCATION   |
| ADDER  | INCREASE IN PRODUCTIVITY ACHIEVABLE THROUGH TRANSFER OF CRAFTSMEN TO OUTSIDE WORK DURING IDEAL WEATHER                                       |
| SADDER | INCREASE IN PRODUCTIVITY ACHIEVABLE THROUGH TRANSFER OF SHOP CRAFTSMEN TO IN-SHIP WORK DURING IN-SHIP IDEAL WEATHER (SEE DEFINITION FOR BGW) |
| SPRD   | AVERAGE SHIFT PRODUCTIVITY   |
| 31 1/0 | AVENAGE SHILL PRODUCTIVITY   |

AVERAGE CRAFT PRODUCTIVITY

#### APPENDIX L (contd)

YARD
YARDT
AVERAGE PRODUCTIVITY AT EACH WORK LOCATION
AVERAGE ANNUAL SHIPYARD PRODUCTIVITY

TOPAY
ZPAY
TTPAY
YDPAY

AVERAGE PRODUCTIVITY
AT EACH WORK LOCATION
AVERAGE PRODUCTIVITY

VARIABLES ORIGINALLY USED FOR ANNUAL WAGE PAYMENT CALCULATIONS
RELATED TO TRANSFER AND PASS OUT CONDITIONS. THIS PART OF THE
PROGRAM WAS DISCARDED WHEN THE VARIATION IN WAGE PAYMENTS WAS
FOUND TO BE INSIGNIFICANT

## LISTING OF THE COMPUTER PROGRAM FOR THE SHIPYARD PRODUCTIVITY MODEL

```
*IT FR5 SHIPS.SHIPS
      DIMENSION PRODET(5.8).PRODAT(5.8).RTTIO(5.3).
     1PRODWS(2.5.2).PRODPR(2.5.4).FGP(5).
     2PPODSH(2) - RAINPP(4) - NAM(8) - DT(3 - 8) - ET(3 - 8) - WIND(3 - 3) - SUN(3) -
     3PRFC(3,4),RH(3,2),PT(3,4),EPROD(5,3,8),APROD(5,3,8),WPROD(2,5,3),
     4PRPROD(2.5.3).FOGPR(5).SUNPR(2.3).GW(3.5).AGW(3.5).BGW(3.5).
     5TPROD(3,5,3,8),PCT(3),ICRAFT(5,3),JCRAFT(5,3,3),DCRAFT(5,3,3),
     6ADDER(3,5),SADDER(3,5),SPRD(3,5,3),TPRD(3,5),YARD(3),TOPAY(3,5,3)
     7, ZPAY(4,5), TTPAY(3,5), YDPAY(3)
      SUN(3)=0.0
      DATA((PRODET(I.J).J=1.8) .I=1.5) / .3..56..75..92.1...84..48..15..
     175,.51,.7,.92.1...79..48..15..25..56..75..92.1...84..53..20..25..5
     31 . . 70 . . 92 . 1 . . . 84 . . 53 . . 2 . . 3 . . 55 . . 75 . . 92 . 1 . . . 84 . . 53 . . 2/
      DATA((PRODAT(I.J).J=1.8).I=1.5) /3*0...7.1...79...48..15..3..56...75
     1,2*1.,.74,.43,.1,.3,.56,.75,.9,1.,.79,.48,.15,.3,.56,.75,.92,1.,.7
     39,.48,.15,.3,.56,.75,.92,1.0.79,.48,.15/
      NATA PRODWS /10*1...7.1...8.1...9.1...9.1...95.1...95.1...0....8..1..8..15.
     1.4.2.8.4.4.8/
      DATA PRODPR /10*1.,2*0.,.8,1.,.95,1.,.95,1.,.95,1.,.3*0.,.95,.85,.9
     15,.85,.95,.95,.95,3*0,.8,.4,.8,.4,.8,.5,.8/
      DATA (FGP(J),J=1,5) /2*1.,2*.5,1./
      DATA (PRODSH(L)+L=1+2) /+7++95/
      DATA(RAINPR(I) . I = 1 . 4) / 1 . 0 . 1 . 0 . . 875 . . 875 /
 205 FORMAT (16F5.0)
206 FORMAT (12F17.3)
  200 FORMAT (8A6,32X)
    3 READ 200+(NAM(I)+I=1+8)
      PRINT 200+ (NAM(I)+I=1+8)
      IL=-1
      DO 20 [=1.3
      READ 205+(DT([,J),J=1.8)
      IF (DT (1.5) .LT ..001) GO TO 999
PRINT 206.(DT(1.J).J=1.8)
      READ 205+(ET(I+J)+J=1+8)
      PRINT 206+(ET(I+J)+J=1+8)
            205. ((WIND(I.J).J=1.3).(PREC(I.J).J=1.4).(RH(I.J).J=1.2))
      READ
      PRINT 206, ((WIND(I,J),J=1,3),(PREC(I,J),J=1,4),(RH(I,J),J=1,2))
      RFAD 205, (PT(I+J), J=1+4)
      PRINT 206. (PT(I.J), J=1.4)
      IF (I.GT.1) GO TO 20
      READ 205, SUN(1), SUN(2), FOG
      PRINT 206. SUN(1).SUN(2).FOG
   20 CONTINUE
   21 CONTINUE
      IF(IL.GE.O) PRINT 847
 847 FORMAT (* THIS MODEL DOES NOT PERMIT TRANSFER BETWEEN LOCATIONS*)
      TEMPERATURE PRODUCTIVITY CALCULATIONS
      DO 52 L=1+2
      DO 50 J=1.5
```

```
00 40 K=1.3
WPROD(L.J.K)=0.
      PRPROD(L.J.K)=A.
      CHECK=RH(K.1)+RH(K.2)
      IF (CHECK.GT.1.01.0R.CHECK.LT..99)PRINT 803.K.K.K
      CHECK=0.
      CHECL=0.
      DO 30 I=1,8
      PC =0.
      CHECK=CHECK+ET(K+I)
      CHECL=CHECL+DT(K+1)
      IF(J.EQ.1.AND.I.LE.4)PC=PT(K.I)
      FPROD(J.K.I)=PRODET(J.I)*(ET(K.I)-PC)
      APROD(J+K+I)=PRCDAT(J+I)*DT(K+I)
   30 CONTINUE
  210 FORMAT (315.2F10.3)
      IF (CHECK.GT.1.01.OR.CHECK.LT..99)PRINT 803.L.J.K
      IF (CHECL.GT.1.01.OR.CHECL.LT..99)PRINT 803.L.J.K
  803 FORMAT (* ERROR IN SUM CHECK! 315)
      CHECK=0.
      CHECL=0.
      WIND PRODUCTIVITY CALCULATIONS
C
      90 35 I=1.3
      CHFCK=CHECK+WIND(K+I)
   35 WPROD(L.J.K)=WPROD(L.J.K)+(PRODWS(L.J.I)*WIND(K.I))
      IF (CHECK.GT.1.01.OR.CHECK.LT..99)PRINT 803.L.J.K
      PRECIPITATION AND HUMIDITY PRODUCTIVITY CALCULATIONS
      IF (J.EQ.1) GO TO.41
      DO 36 I=1.4
      CHECL=CHECL+PREC(K+I)
      IF (PRODPR(L.J.I).EQ..O) GO TO 37
      PRPROD(L+J+K)=PRPROD(L+J+K)+PREC(K+I)*PRODPR(L+J+I)*RAINPR(I)
      GO TO 39
   37 PRPROD(L.J.K)=PRPROD(L.J.K)+PREC(K.I)+.075
   39 CONTINUE
   36 CONTINUE
      IF (CHECL.GT.1.01.OR.CHECL.LT..99)PRINT 803.L.J.K
      GU TO 42
   41 PRPROD(L.J.K)=PRPROD(L.J.K)+(1.4RH(K.1)+RH(K.2)*.075)
   42 CONTINUE
      IDEAL WEATHER OUTSIDE
      GW(K+J)=ET(K+5)*WIND(K+1)*PREC(K+1)
      IF (J.EQ.1)GW(K.J)=GW(K.J)*RH(K.1)/PREC(K.1)
      IF (J.EQ.3.OR.J.EO.4) GW(K.J)=GW(K.J)*(1-FOG)
C
      FOG AND SHADE EFFECTS
      SUMPR(L.K)=1.00*(1-SUN(K))+PRODSH(L)*SUN(K)
      IDEAL WEATHER IN SHIP
C
      AGW(K+J|=DT(K+5)*(WIND(K+1)+WIND(K+2))*(PREC(K+1)+PREC(K+2))
      IF (J.EO.1) AGW(K.J) = AGW(K.J) = RH(K.1)/(PREC(K.1) + PREC(K.2))
      IF (J.EQ.3.OR.J.EQ.4) AGW(K.J)=AGW(K.J)+(1-FOG)
```

```
- mon(K+1)=AGM(K+1)-GM(K+1)
   40 CONTINUE
      FOGPR(J)=1.00*(1-FOG)+FGP(J)*FOG
   50 CONTINUE
   52 CONTINUE
      TOTAL PRODUCTIVITY CALCULATIONS
C
      DATA (PCT (K) . K = 1,3) / . 65. . 30. . 05/
      KTOTAL = 2138
      DATA ((ICRAFT (J.L), J = 1.5), L = 1.3) / 60, 227,
    161. 237. 57. 39. 272. 58. 229. 308. 7. 156.
     243 - 204 - 807
      00 90 L = 1.3
      00 99 J = 1.5
      ZPAY(L.J)=).
      TPRD(L.J)=0.
     DO 90 K = 1.3
90 89 I=1.8
      SC=1.
      IF (I.GE.6) SC=SUNPR(L.K)
         (L.EQ.2) 50 TO 80
      1F (L.EQ.3) GO TO 82
     OUTSIDE PRODUCTIVITY
     TPROD (L+J+K+I) = FPROD (J+K+I ) # WPROD (L+J+K) # PRPROD (L+J+K)
    1#FOGPR(J)#SC
     GO TO 88
     INSIDE PRODUCTIVITY
  80 CONTINUE
     TPROD (L*J*K*) = APROD (J*K*I) * WPROD (L*J*K) * PRPROD (L*J*K) *
    1FOGPR(J)*SC
     GO TO 88
  #2 TPROD (L.J.K.I)=1.#DT(K.I)
  88 CONTINUE
     CTOT=CTOT+TPROD(L,J,K,I)
  89 CONTINUE
     PRINT 12.CTOT.L.J.K
     CTOT=0.
  12 FORMAT (* TOTAL PRODUCTIVITY IS*F7.3. AT LOCATION*13. FOR CRAFT*
    113+ AND SHIFT 13)
     DISTRIBUTION OF WORKERS
     JCRAFT (J.L.K) = ICRAFT (J.L) # PCT (K) + .5
DCRAFT (J.L.K) =FLOAT( JCRAFT (J.L.K))/ FLOAT(KTOTAL)
 90 CONTINUE
     IDEAL WEATHER ADDER
    DO 111 J = 1.5
    RTTIO (J.2) =FLOAT(ICRAFT(J.3))/FLOAT(ICRAFT(J.2) )
111 RTTIO (J+1) =FLOAT(I CRAFT (J+ 2) + I CRAFT (J+3))/ FLOAT(ICRAFT (
    YARDT=0.
    DO 188 LY= 1.3
    L=LY
```

```
YARD(L)=0.
YDPAY(L)=0.
    DO 187 J = 1.5
    TTPAY(L.J)=0.
    DO 186 K = 1.3
    SPRD(L.J.K)=0.
    IF (L.GE.2) GO TO 183
  THIS STATEMENT PROHIBITS TRANSFERS BETWEEN LOCATIONS
    IF(IL.GE.O) GO TO 183
    00 128 I=1.8
IF (J.GT.1) GO TO 127
    PAINT = RH (K+2) *(*(***(**ICRAFT(J+1))*(**ICRAFT(J+2))))/ICRAFT(J+3)
    TPROD (3*1*K*I) = TPROD (3*1*K*I)*(1+ PAINT)
127 CONTINUE
    IF (J.NE.2) GO TO 128
    WELD = (PREC(K_{•}3) + PREC(K_{•}4))*(.7*ICRAFT(J_{•}1))/ICRAFT(J_{•}2)
    TPROD (2+2+K+1) = TPROD (2+2+K+1)*(1+WELD)
128 CONTINUE
    ADDER (K \cdot J) = GW (K \cdot J) * (RTTIO (J \cdot I))
    TPROD (1.J.K.5) = TPROD (1.J.K.5)
                                             +ADDER (K.J)
    TPROD (2*J*K*5) = TPROD (2*J*K*5)-GW(K*J)
    TPROD (3*J*K*5) = TPROD (3*J*K*5)-GW(K*J)
    IN SHIP ADDER
    SADDER (K.J) = BGW (K.J) * ( RTTIO (J.2))
    TPROD (2+J+K+5) = TPROD (2+J+K+5) + SADDER (K+J)
    TPROD (3+J+K+5) = TPROD (3+J+K+5) - BGW (K+J)
183 CONTINUE
    DO 185 I = 1.8
185 SPRD (L_{\bullet}J_{\bullet}K) = SPRD (L_{\bullet}J_{\bullet}K) + TPROD (L_{\bullet}J_{\bullet}K_{\bullet}I)
PRINT 313, L. J. K. SPRD (L.J.K)
313 FORMAT ( * TOTAL SHIFT PRODUCTIVITY* 315. F 10.3)
186 TPRD (L.J) = TPRD (L.J) + SPRD (L.J.K)*PCT(K)
    # (TPRD(L.J).GT.1) GO TO 273
    GO TO 274
273 XY=TPRD(L.J)-1.
    ZPAY(L,J)=ZPAY(L,J)-XY
    LL=L+1
    IF (LL.EQ.4) LL=1
IF (TPRD(LL.J).EQ.1.) LL=LL+1
    PY=(XY*ICRAFT(J,L))/ICRAFT(J,LL)
    ZPAY(LL,J)=ZPAY(LL,J)+PY
    TPRD(L,J)=1.
    TPRO(LL,J)=TPRO(LL,J)+PY
    PRINT 917.XY,L,LL,PY
917 FORMAT (F7.3. EXCESS PRODUCTIVITY TRANSFERRED FROM LOCATION 13.
   1FQUIVALENT PRODUCTIVITY GAIN AT'13. 15'F7.3)
    IF (TPRD(LL+J)+LE+1+) GO TO 274
    XY=TPRD(LL+J)-1.
    ZPAY(LL,J)=ZPAY(LL,J)-XY
```

```
TPRD(LL+J)=1.
LQ=LL+1
    IF (LQ.E0.4) LQ=1
    PY=(XY*[CRAFT(J+LL)]/ICRAFT(J+LQ)
    TPRD(LC+J)=TPRD(LC+J)+PY
    ZPAY(LQ.J)=ZPAY(LQ.J)+PY
    PRINT 917.XY.LL.LQ.PY
274 CONTINUE
PRINT 314. L. J. TPRD (L.J)
314 FORMAT (* CRAFT PRODUCTIVITY* 215 . F10.3)
187 YARD (L) = YARD (L) +(TPRD (L.J) *ICRAFT(J.L))/KTOTAL
PRINT 315. L. YARD (L)
315 FORMAT (/ LOCATION: 15. F10.3)
188 VARDT = YARCT + YARD (L)
PRINT 316. YARDT. (NAM (I). I = 1.8)
316 FORMAT (/ YARD PRODUCTIVITY: F 10.3. 5X. 8A6)
    RX=1.-YARDT
    CX=BX/YARDT
    DX= . 374 *CX
    PRINT 319+DX
319 FORMAT ( EXCESS STRAIGHT TIME LABOR COST .F6.3)
     IL=IL+1
     IF (IL.GE.7) GO TO 599
     IF(IL.EQ.0) GO TO 21
    GO TO (591,593,594,592,601,611).IL
591 PRODSH(1)=1.
     PRODSH(2)=1.
     PRINT 595
595 FORMAT (* PRODUCTIVITY WITH SHADE PROVIDED*)
     GO TO 21
592 DO 757 L=1.2
     nn 757 J=1,5
     DO 757 K=1.3
     PRODWS(L.J.K)=1.
757 CONTINUE
     PRODET(1.1)=0.
     PRODET(1.2)=0.
     PRODET(1+3)=0.
     PRODET(1:4)=.7
     DO 609 K=1+3
     DO 609 [=1.8
IF (I.LE.4) PT(K.I)=0.
609 FT(K+1)=DT(K+1)
PRINT 596
596 FORMAT (1
                PRODUCTIVITY WITH WIND PROTECTION*)
     GO TO 21
593 DO 758 L=1.2
     DO 758 J=1.5
     DO 758 K=1.4
```

```
PRODPR(L.J.K)=1.
 758 CONTINUE
     RAINPR(3)=1.
     DAINPR(4)=1.
     PRINT 597
 597 FORMAT (* PRODUCTIVITY WITH RAIN PROTECTION*)
     GO TO 21
 594 CONTINUE
     DO 602 K=1.3
     RH(K,1)=1.
 602 PH(K,2)=0.
 PRINT 598
598 FORMAT (* PRODUCTIVITY WITH DEHUMIDIFIERS*)
     GO TO 21
 601 00 604 J=1.5
00 604 I=6.8
     PRODET(J.I)=1.
 604 PRODAT (J. 1)=1.
     PRINT 606
                 PRODUCTIVITY WITH COOLING PROVIDED*)
 606 FORMAT (
     GO TO 21
 611 DO 613 J=1.5
     DO 613 I=1.4
     PRODET(J.I)=1.
     PRCDAT(Jel)=1.
 613 CONTINUE
      PRINT 615
                 PRODUCTIVITY WITH HEATING PROVIDED*)
 615 FORMAT (*
     GO TO 21
 599 CONTINUE
      GO TO 3
 999 CONTINUE
      STOP
      END
. XQT SHIPS
      SAN DIEGO
        •0
             .0 .001 .963 .033 .003
                                        •0
   .0
.0 .0 .0 .018 .946 .033 .003 .0
.8638.1350.0025 .983 .006 .007 .004.9862.0138
            •0
   .0
        •0
                   • 0
.6265.2750
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                   .0 .986 .n13
  •0
       •0
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   .0
        .0
              .0 .016 .971 .013
.9638.0350.0n13 .981 .006 .010 .003.9512.0488
            •0
   .0
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                   •0
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   .0
                   .0 .991 .008
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        •0
              •0
        .0 .001 .018 .973 .008
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   •0
.9800.0200.0013 .975 .009 .013 .003.8275.1725
   .0
        •0
              •0
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